Laboratory Power

When building any electronic equipment, some form of power supply is required for testing and experimental purposes, even though the equipment power supply, in its final form, may be batteries or even a

purpose-built mains powered unit.

The ability to vary the supply voltage, to simulate the effect of a failing battery for example, is a desirable feature when testing certain equipment. Many circuits require bipolar supplies (dual rail) while a fixed +5V for TTL is a definite asset. To anyone who has struggled to test a new circuit with partly discharged batteries or some hairy hook-up to give 5 volts for the logic, this Lab Power Supply will certainly take some of the exasperation out of experimentation.

Description

The Lab Power Supply provides three individual power supplies: +5V 0-400mA for TTL, 0 to +15V 0-100mA, 0 to -15V 0-100mA for op. amps and general transistor circuitry.

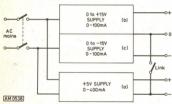


Fig. 1: Block diagram.

The +5V is fully floating while the bipolar supply has a common zero volt connection as shown in Fig. 1. This arrangement provides a fixed supply for TTI. and a fully variable supply which may provide up to 30V at 100mA, with the supplies in series, or 0 to +15V and 0 to -15V with a common 0V connection.

In conventional usage, the 0V output of the 5V TTL supply and the centre 0V of the dual supply would be joined together. To do this, a link switch is provided to join or 'common' the 0V connections. This switch may be set to the un-linked position when full isolation of the supplies is required.

Circuit

The full circuit diagram is shown in Fig. 2. The 5V supply is shown in the lower part of Fig. 2 and comprises a mains transformer T2, full-wave bridge rectifier BR2, smoothing capacitor C5 and integrated circuit regulator IC3. Current and voltage metering is provided by R19-22 and R23 respectively. These are



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connected to the meter by S3. The rather unusual resistor arrangement for monitoring current avoids the difficulty of making up a low resistance shunt for the meter. The recommended resistors for R19-21 are 2% thick film types and for R22, 2% metal oxide, giving a worst case error of about 7%.





For voltage monitoring, the meter is switched in series with R23, giving 20V full scale deflection.

In the variable supplies, the mains transformer T1, bridge rectifier BR1, and smoothing capacitors C1 and C2 generate a dual 20V supply line. From these rails, regulated lines of +10V, +5V, -5V and -10V are provided by corresponding Zener diodes D1, D2, D3 and D4. These voltages are fed to various parts of the circuit.

Variable regulator circuit

The basic regulator circuit is shown in Fig. 3. It consists of a 741 operational amplifier used as a summing amplifier and a power transistor, Tr1, connected as an emitter follower. The output from the emitter follower is fed back to the inverting input of the 741 and so provides negative feedback. This causes the output of the emitter follower to maintain the voltage at the inverting input equal to the non-inverting input, i.e. at zero volts.

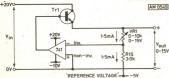


Fig. 3: The basic schematic of the variable voltage section. Fig. 2, the complete circuit diagram, is shown on page 589.

A negative current of 1.5mA is set up through R15 by connecting the bottom end to -5V. An equal but opposite polarity current comes from TR1 emitter (the output terminal) through VR1 to cancel out this

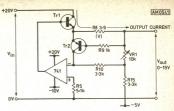


Fig. 4: The current limiting circuitry.

negative current thus maintaining the 'summing junction' at 0V. With VR1 set at zero resistance, +1·5mA will be provided with the output terminal virtually at 0V; with VR1 set to maximum (10kO), Tr1 emitter and the output will now move to +15V to maintain +1·5mA through VR1. Therefore, at any setting of VR1 the output voltage will be equal to the voltage drop across VR1 produced by 1·5mA through

* components

components	
Resistors	
R1 680Ω ‡W	R13 330Ω 2%
R2 680Ω ‡W	R14 3-9Ω 2% +W thick film
R3 330Ω	R15 3-3kΩ
R4 680Ω	R16 3-3kΩ
R5 5-1kΩ	R17 20kΩ 2%
R6 5·1kΩ	R18 20kΩ 2%
R7 330Ω 2%	R19 3-9Ω 2% ±W thick film
R8 3-9Ω 2% &W thick film	R20 3-9Ω 2% ‡W thick film
R9 1kΩ	R21 3.9Ω 2% ±W thick film
R10 3·3kΩ	R22 1-2kΩ 2%
R11 3-3kΩ	R23 20kΩ 2%
R12 1kΩ	
All 1W 5% carbon film, exc	cept where stated.
VR1 10kΩ 1W wire wound	VR2 10kΩ 1W wire wound
Capacitors	
C1 2200 µF 25V	
C2 2200 µF 25 V	
C3 10µF 25V C4 10µF 25V	
C5 2200μF 25V C6 220nF	
C7 470nF	
Semiconductors	
Tr1 TIP31	IC1 741
Tr2 BC214	IC2 741
Tr3 BC184	IC3 7805
Tr4 TIP39	BR1 1A type

S1 DPDT S2 SPST S3 2 pole 6 way

Switches

T1 Primary 240V, secondary two windings each of 15V 0-2A
T2 Primary 240V, secondary two windings each of 4-5V 0-6A

BR2 1A type

Missellansous

PC (from Readers PCB service, if required), Meter 0-1 mA, terminals, knobs, mains lead, hardware, cabinet (21 × 8 × 14cms).

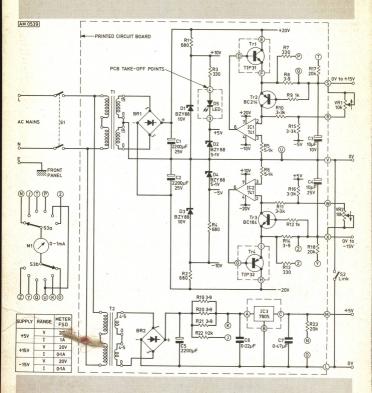


Fig. 2: The complete schematic. The mains transformer primaries are not connected to the printed circuit board. As such, they are not indicated by reference letters which correspond with Fig. 6, the PCB overlay.

Rotation of VR1 produces a linearly variable output voltage of 0-15V.

When a current is drawn from the output terminal, this tends to reduce the output voltages slightly and this negative change is at once apparent at the 'summing junction' and so produces a positive change at the output and restores the output voltage to the correct value again, or almost so. This amplified correction gives the characteristically low output impedance that can be obtained from electronic voltage regulator circuits.

Regulator with current limiting

The circuit with the additional components is shown in Fig. 4. A current sampling resistor, RB, monitors the load current. This resistor is between the emitter and base of Tr2 and when the load current produces a sufficient voltage drop across RB, Tr2 turns on causing positive current to flow from the collector of Tr2 to the 'summing junction'. This results in a negative polarity change in the output, ensuring that the output current does not rise to a dangerously high value. Tr2 will turn on when the emitter-base voltage (V) reaches about 0.55V.

$$I_{max} = \frac{0.55V}{3.9\Omega} = 140 \text{mA approx.}$$

The resistor R8 performs a dual purpose in that with R7 (see Fig. 2) it provides a meter shunt for monitoring output current, giving a full scale deflec-

tion of the panel meter for 100mA. The shunting arrangement is similar to the +5V supply circuit previously described.

R9 is included in the base circuit of Tr2 to limit the base current to a safe value and R5 is included in the hon-inverting input of the 741 to balance the small voltage off-sets produced by the input currents of the device. C3 is fitted across the output terminals to provide a low output impedance at medium and high frequencies. The negative supply is a mirror image of the positive supply.

The panel meter has a basic sensitivity of 1mA full scale deflection and is switched to various parts of the circuit for output voltage and current measurements.

Construction

The prototype was housed in a Verobox. The printed circuit board carrying all the components was fixed to tapped pillars provided in the base of the Verobox. The front and rear panels fit into slots in the base and cover.

The printed circuit board layout is given in Fig. 5. The overlay, Fig. 6, shows numbered interconnection points where the wiring from the front and rear panels is connected. These points are also identified on the circuit diagram shown in Fig. 2. The only connections not identified in this way, are those to the mains transformer primaries, as they do not connect with the PCB. The primaries of the transformers are fed from S1. the double-pool on/off switch.

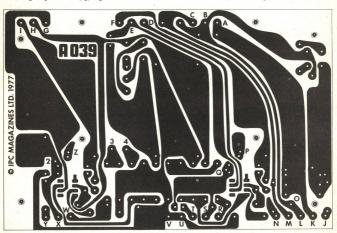


Fig. 5: The PCB shown copper side. The scale factor is one; ready made boards may be obtained from the PW Readers' PCB service. Details page 593. Fig. 6: Component overlay. This drawing is shown on page 591 (overleaf). The reference letters refer to the circuit diagram.

