

Scope Sweep Generator

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Construction details on an inexpensive time-mark generator for calibrating the horizontal sweep of an oscilloscope.

MEASURING time or frequency accurately with an oscilloscope is impossible if the scope's horizontal sweep (trace) is uncalibrated. The horizontal sweep can be calibrated by a time-mark generator. Although a professional time-mark generator costs about \$300, the simple time-mark generator covered in this article can be built for substantially less than this amount.

This time-mark generator has outputs at known frequencies and when the frequency is accurately known, the period in microseconds along the scope trace can be calculated. Table 1 indicates the relationship between frequency and time for this generator.

A scope's horizontal sweep can be calibrated in one of three ways. The first and most useful is in microseconds-per-centimeter. Other, less-common markings, are microseconds-per-inch, or frequency, which is uncalibrated. With a known frequency signal any scope's horizontal sweep can be calibrated with great accuracy by merely adjusting the variable sweep speed until a known number of timing intervals occupies a specific distance on the screen. Any scope sweep non-linearity will also be displayed.

In this time-mark calibrator, thirteen transistors are used to provide accurate calibration points of 1, 5, 10, 100, 1000, and 10,000 microseconds duration.

As shown in Fig. 1, a 1-MHz crystal oscillator (Q1) furnishes an accurate 1-microsecond timing output *via* Q2 to point "A". A one-shot multivibrator (Q3-Q4), adjusted for a division of five, furnishes an accurate 5- μ sec output at point "B". Division-by-two is accomplished in flip-flop Q5-Q6 to produce a 10- μ sec output at point "C". Division-by-ten can now be accomplished with unijunction transistor stage Q7 to produce a 100- μ sec output at point "D". Two more divide-by-ten circuits, Q8 and Q9, have outputs of 1000 μ secs at point "E" and 10,000 μ secs at point "F", respectively.

Accuracy is inherent in this design. The crystal provides the primary accuracy and any error is too small to be observed on a scope. All of the other outputs are obtained by division from this stable source. A word of caution—division in the last three stages will be correct only if the loading of the unijunction emitters remains constant. For this reason, an emitter follower, Q12 and Q13, has been added.

If your scope does not have a 10-megohm vertical amplifier input impedance, then the emitter follower should be used as part of the testing procedure. The emitter follower is a Darlington configuration with a calculated input impedance of about 14 megohms. It exhibits no measurable loading to any of the circuits.

Parts required to build this generator are standard but a high-*beta*, high-*f*, transistor should be used for the higher frequency circuits. Placement of the parts is not critical although short leads should be used.

The addition of regulator R8 and Q10 and Q11 will result in greater stability. The emitter-base junctions of the 2N3638's are used as a low-cost zener diode. If a regulated supply or a mercury battery is used, the regulator would not be required, and could be omitted.

Waveforms

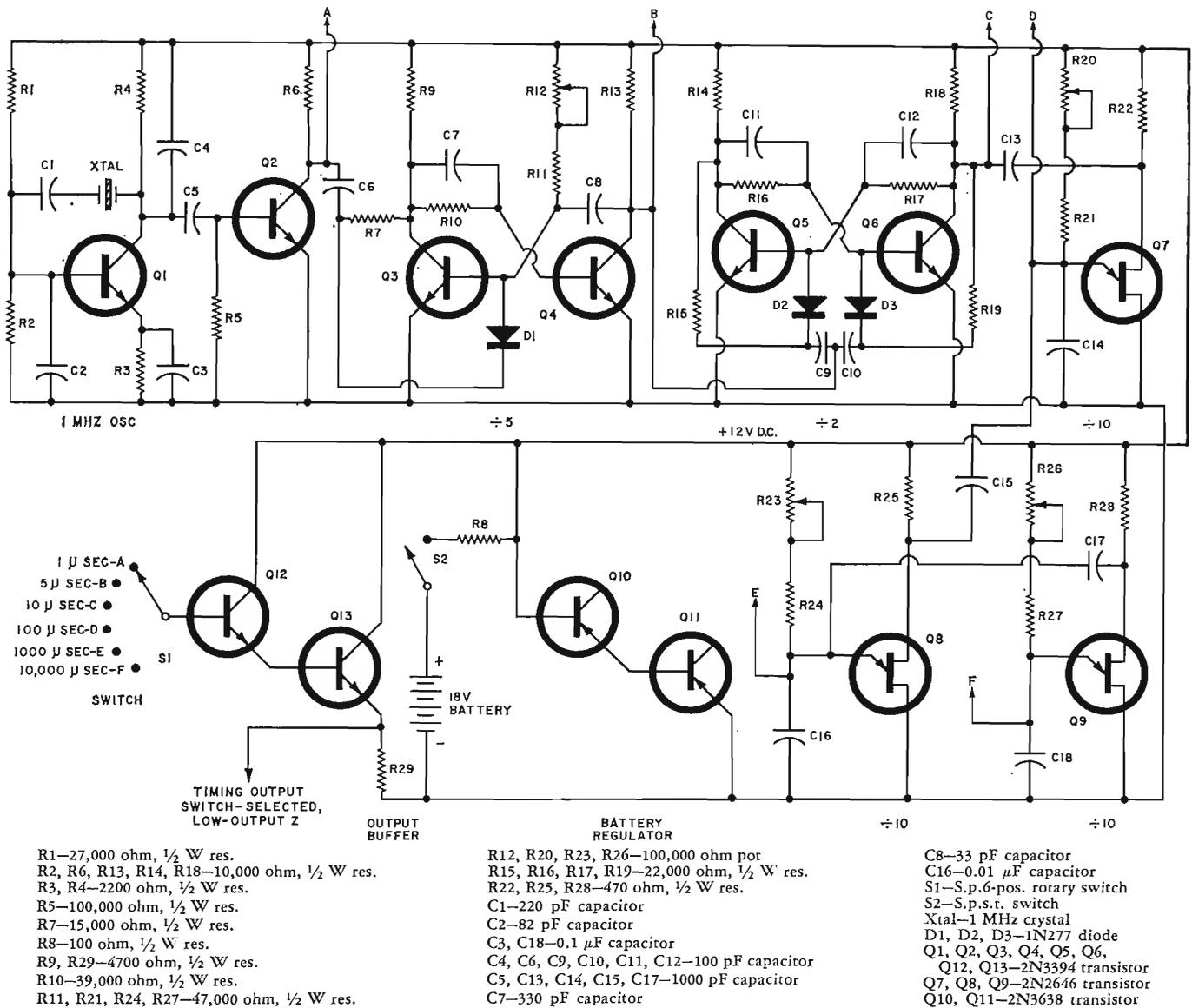
When power is applied, the waveform of Fig. 2A will be present at the collector of Q1. The purpose of buffer Q2 is to provide a sharp falling edge for triggering the following divide-by-five counter. The waveform of Fig. 2B will be present at the collector of Q2 and point "A". The trailing edges of this waveform are 1 μ sec apart. Transistors Q3 and Q4 make up a one-shot, divide-by-five circuit. Q3 is normally "on" ("on" is defined as the transistor in conduction while "off" is when it is not). A negative pulse coupled through C6 and D1 turns Q3 "off" causing Q4 to go "on". Since the voltage across capacitor C8 cannot change instantaneously, the base of Q3 is forced approximately 10 volts below the emitter. Capacitor C8 is charged by R11 and R12 in series and, when approximately +0.6 volt is reached, Q3 turns "on" removing the base drive from Q4. Control R12 is adjusted so that the time required for this complete cycle is five pulses of the input. Fig. 2C shows the collector waveform of Q4 at point "B", while Fig. 2D shows the waveform at the base of Q3. The waveform at the collector of Q4 is 5 μ sec per cycle.

Division-by-two is most easily accomplished with a flip-flop. Transistors Q5 and Q6 make a simple flip-flop, with D2 and D3, the triggering diodes. Since R16 and R17 form direct paths from opposite collectors to opposite bases, the flip-flop will remain stable until a change is triggered by the falling edge of the Q4 output waveform. The waveforms of this flip-flop will be affected by subsequent loading, so C13 and R22 should be connected before testing. Fig. 2E shows the waveform present at the Q6 collector and point "C". This waveform is 10 μ sec per cycle, or 100 kHz.

Division-by-ten can be accomplished at lower frequencies using a unijunction transistor. Capacitor C13 couples the pulses from Q6 into base-2 of Q7. The combination of C14 and R20 and R21 form a time constant equivalent to a fre-

Table 1. The relationship between frequency and time for the various output waveforms of the simple scope sweep calibrator.

TEST POINT	FREQUENCY	TIME
"A"	1 MHz	1 μ sec
"B"	200 kHz	5 μ secs
"C"	100 kHz	10 μ secs
"D"	10 kHz	100 μ secs
"E"	1 kHz	1000 μ secs
"F"	100 Hz	10,000 μ secs



- R1—27,000 ohm, 1/2 W res.
- R2, R6, R13, R14, R18—10,000 ohm, 1/2 W res.
- R3, R4—2200 ohm, 1/2 W res.
- R5—100,000 ohm, 1/2 W res.
- R7—15,000 ohm, 1/2 W res.
- R8—100 ohm, 1/2 W res.
- R9, R29—4700 ohm, 1/2 W res.
- R10—39,000 ohm, 1/2 W res.
- R11, R21, R24, R27—47,000 ohm, 1/2 W res.

- R12, R20, R23, R26—100,000 ohm pot
- R15, R16, R17, R19—22,000 ohm, 1/2 W res.
- R22, R25, R28—470 ohm, 1/2 W res.
- C1—220 pF capacitor
- C2—82 pF capacitor
- C3, C18—0.1 μF capacitor
- C4, C6, C9, C10, C11, C12—100 pF capacitor
- C5, C13, C14, C15, C17—1000 pF capacitor
- C7—330 pF capacitor

- C8—33 pF capacitor
- C16—0.01 μF capacitor
- S1—S.p.s.r. rotary switch
- S2—S.p.s.r. switch
- Xtal—1 MHz crystal
- D1, D2, D3—1N277 diode
- Q1, Q2, Q3, Q4, Q5, Q6, Q12, Q13—2N3394 transistor
- Q7, Q8, Q9—2N2646 transistor
- Q10, Q11—2N3638 transistor

Fig. 1. Schematic and parts list for scope sweep calibrator. Regulator transistors Q10 and Q11 can be omitted if a regulated power supply or mercury battery is used. Each lettered output is connected to the appropriate terminal of switch S1.

quency of 10 kHz. Both C15 and R25 should be connected since they present a load to Q7. Potentiometer R20 is adjusted until 10 pulses at the Q6 collector result in one sawtooth at the emitter of Q7, as shown in Fig. 2F. This sawtooth is 100 μsec per cycle or 10 kHz.

Division-by-ten is accomplished twice more in exactly the same way by unijunction oscillators Q8 and Q9. Outputs are 1000 μsecs per cycle (1 kHz) and 10,000 μsecs per cycle (100 Hz), respectively. The waveform is identical to Fig. 2F except the μsec/cm scale becomes 100 and 1000 respectively. Fig. 2G shows the waveform at base-2 of each unijunction transistor.

How to Use

The generator output is connected to the scope vertical input and the scope is set to trigger on negative peaks. If the scope has provisions for external triggering, then the generator output can also be connected (in parallel) to this terminal and the sweep set for negative triggering.

The scope graticule should be calibrated in centimeters along the horizontal axis (one centimeter equals 0.3937 inch).

Assume that it is desired to calibrate the scope to 1 μsec/cm. Set the generator S1 to position "A", and adjust the scope sweep until one complete waveform (Fig. 2B) occupies one centimeter division. This distance, and all equivalent marked distances along the sweep, are now calibrated at 1 μsec per centimeter. The same centimeter divisions can be used to set the sweep to any desired value as selected by S1, and the corresponding waveforms of Fig. 2.

Fig. 2. Waveforms present in the generator. See text for explanation.

