

# design ideas

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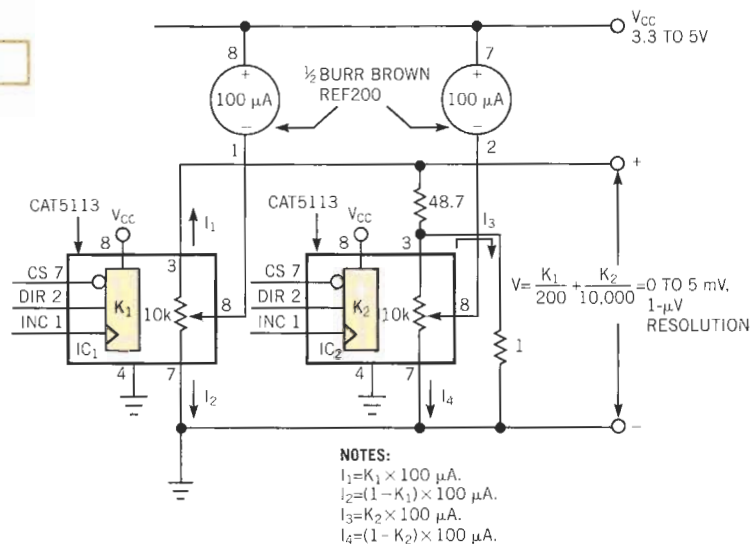
## DPPs make nonvolatile microvolt DAC

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**T**HE AVAILABILITY of a seemingly limitless variety of monolithic DAC chips makes it easy to implement most digital-to-analog-conversion applications with a single off-the-shelf device. Sometimes, an unusual set of requirements necessitates a multichip approach, however. One example of such a requirement is the need for nonvolatility of the DAC's setting in power-up and -down cycles. Another example is the need for output resolution and stability at less than 1  $\mu\text{V}$ . The circuit in **Figure 1** combines inexpensive DPPs (digitally programmed potentiometers) from Catalyst Semiconductor ([www.catsemi.com](http://www.catsemi.com)) with precision current references from Burr-Brown ([www.ti.com](http://www.ti.com)) to achieve both nonvolatility and less-than-1- $\mu\text{V}$  performance. Accurate simulation of the signals from high-temperature platinum-rhodium-based thermocouples requires less-than-1- $\mu\text{V}$  performance. These temperature sensors have Seebeck coefficients of only 6  $\mu\text{V}/^\circ\text{C}$ . Therefore, only voltage sources with 1- $\mu\text{V}$ -level stability and precision can simulate such sensors.

To achieve such low output drift would

**Figure 1**



**Digitally programmed potentiometers combine to form a novel, microvolt-level DAC.**

normally require the use of active circuit elements, such as chopper-stabilized amplifiers, with offset temperature coefficients not much higher than 1 nV/ $^\circ\text{C}$ . The circuit in **Figure 1** takes a different approach by using current division and a passive and, therefore, inherently drift-free output that needs no amplifiers. Each half of the REF200 sources a 100- $\mu\text{A}$  reference current. The twin currents each connect to the wiper of DPPs, IC<sub>1</sub> and IC<sub>2</sub>. There, they split into two currents (for example, I<sub>1</sub> and I<sub>2</sub>) in a wiper-to-total ratio, K<sub>1</sub>, which the programmed setting of the DPP determines. I<sub>1</sub> = K<sub>1</sub> × 100  $\mu\text{A}$ , and I<sub>2</sub> = (1 - K<sub>1</sub>) × 100  $\mu\text{A}$ . I<sub>1</sub> passes through the series combination of the 48.7 $\Omega$  resistor and the 1 $\Omega$  output resistor and thereby generates the output voltage: V = K<sub>1</sub>(50 $\Omega$  × 100  $\mu\text{A}$ ) = 0 to 5 mV as K<sub>1</sub> varies from 0 to 1. The operation is straightforward and drift-free. Unfortunately, the resolution with a single po-

tentiometer is inadequate for many precision applications.

IC<sub>2</sub>, a CAT5113, like other DPPs, offers the versatility of an uncommitted resistance element and nonvolatility of the setting. Its resolution, however, is only 100 steps, which is slightly worse than 7 bits and equivalent to 50  $\mu\text{V}$  in this circuit. You therefore incorporate a second DPP, IC<sub>2</sub>, in the converter. IC<sub>2</sub>'s output current acts into the 1 $\Omega$  load for a 50-to-1 resolution enhancement over IC<sub>1</sub> alone. IC<sub>2</sub> thus adds a 0- to 100- $\mu\text{V}$  contribution to V. Hence, the composite output is V = K<sub>1</sub>/200 + K<sub>2</sub>/10,000 with a 5-mV span and 1- $\mu\text{V}$  resolution. The circuit is an ideal approach for such applications as the simulation of thermocouple signals in precision temperature-measurement and -control systems.

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