

Various Schematics and Diagrams

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Chapter 1) About the Author & Copyright

Various Schematics and Diagrams

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Chapter 2) Introduction

This is a collection of various useful and interesting schematics. Some of these are also referenced by or included in other documents at this site.

What isn't here (this may not be everything):

- * Extremely important safety information. See the document: "[Safety Guidelines for circuits involved high voltage and/or direct line-connected high power systems](#)". Getting electrocuted could ruin your whole day. For really high voltage equipment, also see: [Tesla Coils Safety Information](#).
- * Laser power supplies and other laser related schematics will be found in the document: "Lasers: Safety, Diode Lasers, Helium Neon Lasers, Drive, Info, Links, Parts".
- * Additional electronic flash and other strobe related schematics will be found in the document: "[Notes on the Troubleshooting and Repair of Electronic Flas](#)".
- * Isolation and variable transformers (Variacs), homemade degaussing coils,

series light bulb adapter, and other Incredibly Handy Widgets(tm) for your test bench will be found in the document: "Troubleshooting and Repair of Consumer Electronic Equipment" and possibly in the specific document for each type of equipment.

- * General nifty gadget and other pack rat stuff can be found in the document: "[Salvaging Interesting Gadgets, Components, and Subsystems](#)" which identifies useful components which may be removed from common consumer electronics and appliances as well as unconventional uses for their subsystems, modules, or replacement parts.
- * Schematics associated with the testing of capacitors, transistors and other semiconductor devices (includes simple curve tracer design), flyback transformers, etc., will be found in the document dealing with each of these type of devices.

Chapter 3) Simple High Voltage Generator

This basic circuit is capable of supplying up to 30 kilovolts or more from a low voltage DC source using a flyback (LOPT) transformer salvaged from a TV or computer monitor. Typical output with a 12 VDC 2 A power supply or battery will be around 12,000 V. Current at full voltage is typically around 1 to 2 mA. Higher currents are available but the output voltage will drop. At 2 KV, more than 10 mA may be possible depending on your particular flyback transformer.

This is an ASCII file: [F_hvinvert.html](#)

Chapter 4) Adjustable High Voltage Power Supply

This circuit uses a pair of 555 timers to provide variable frequency variable pulse width drive to an inverter using a flyback transformer salvaged from a black and white or color TV or computer monitor.

The input voltage can range from about 5 to 24 V. Using a flyback from a MAC Plus computer which had its bad primary winding excised, an output of more than 20 KV is possible (though risky since the flyback is probably not rated for more than about 12 KV) from a 24 VDC, 2 A power supply. By adjusting the drive frequency and duty cycle, a wide range of output voltages and currents may be obtained depending on your load.

With the addition of a high voltage filter capacitor (.08 uF, 12 KV), this becomes a nice little helium neon laser power supply which operates on 8 to 15 VDC depending on required tube current and ballast resistor. See the document: "Lasers: Safety, Drive, Info, Parts; Diode, HeNe, Ar/Kr Ion Lasers" for details.

The drive transformer is from a B/W computer monitor (actually a video display terminal) and has a turns ratio of 4:1 wound on a 5/16" square by 3/8" long

nylon bobbin on a gapped ferrite double E core. The primary has 80 turns and the secondary has 20 turns, both of #30 wire. Make sure you get the polarity correct: The base of the switching transistor should be driven when the driver turns on.

Where the flyback includes an internal rectifier and/or you are attempting to obtain the maximum output voltage of a specific polarity, the direction of drive matters as the largest pulse amplitude is generated when the switching transistor turns off. Since flyback transformers are not marked, you will have to try both possible connections to the drive coil. Use the one that produces the higher output voltage for a given set of input conditions (drive and pulse rate/width).

Many variations on this basic circuit are certainly possible. However, one nice thing about running it at 24 VDC or less is that it is much more difficult to let the smoke out of the circuit! The 5 A power supply I was using shut down on several occasions due to overcurrent but the only time I blew the chopper transistor was by accidentally shorting the base to collector.

These schematics are available in both PDF and GIF format.

Get HVGEN32-SCH: [hvgen32.pdf](#) or [hvgen32.gif](#)

Chapter 5) Panasonic VCR Switching Power Supply (PV48XX and Clones)

This circuit was reverse engineered from the switching power supply from a Panasonic VCR. It is typical of the small switchers used in the Panasonic PV28XX, PV48XX, and many other models, their Magnavox clones, as well as other Matsushita manufactured VCRs. Many VCRs of other brands use similar designs.

Errors in transcription are possible. Some models use additional outputs each fed from a single rectifier diode and filter capacitor (not shown). Some part numbers and the connector pinout may not be the same for your particular VCR.

A totally dead supply with a blown fuse usually means a shorted switchmode power transistor, Q1. Check all other components before applying power after replacement as other parts may be bad as well.

The most common problems resulting in low or incorrect outputs are dried up or leaky electrolytic capacitors - C4, C16, C17, C21.

See the document: "[Notes on the Troubleshooting and Repair of Small Switchmode Power](#)

These schematics are available in both PDF and GIF format:

Get VCRPS-SCH: [vcrps.pdf](#) or [vcrps.gif](#)

Chapter 6) Variable Intensity Variable

Frequency Stroboscope

The circuit referenced in the document: "Notes on the Troubleshooting and Repair of Electronic Flash Units and Strobe Lights and Design Guidelines, Useful Circuits, and Schematics" is designed to provide a variety of options in terms of repetition rate, flash intensity, and various repeat and triggering modes.

The design includes:

- * Line operated voltage doubler power supply.
- * Power transformer operated low voltage logic supply.
- * Variable frequency repeat mode controlled by 555 timer.
- * Optoisolated external trigger input.
- * Selectable flash intensities of .2, 2, and 20 W-s.
- * Autorepeat speeds from .05 to 100 Hz (though obviously, the flashlamp will not operate at all intensities for these entire ranges.)

Parts of this circuit have been built and tested but the entire unit is not complete. Maybe someday....

These schematics are available in both PDF and GIF format.

Get STROBEX-SCH: [strobex.pdf](#) or [strobex.gif](#)

Chapter 7) Jacobs Ladders

The climbing arcs of old bad sci-fi movies are always a popular item. Just make sure you understand the safety implications before constructing one of these. See the document: "[Safety Guidelines for High Voltage and/or Line Powered Eq](#)

This is an ASCII file: [F_jacobs.html](#)

Chapter 8) Inverter Circuits

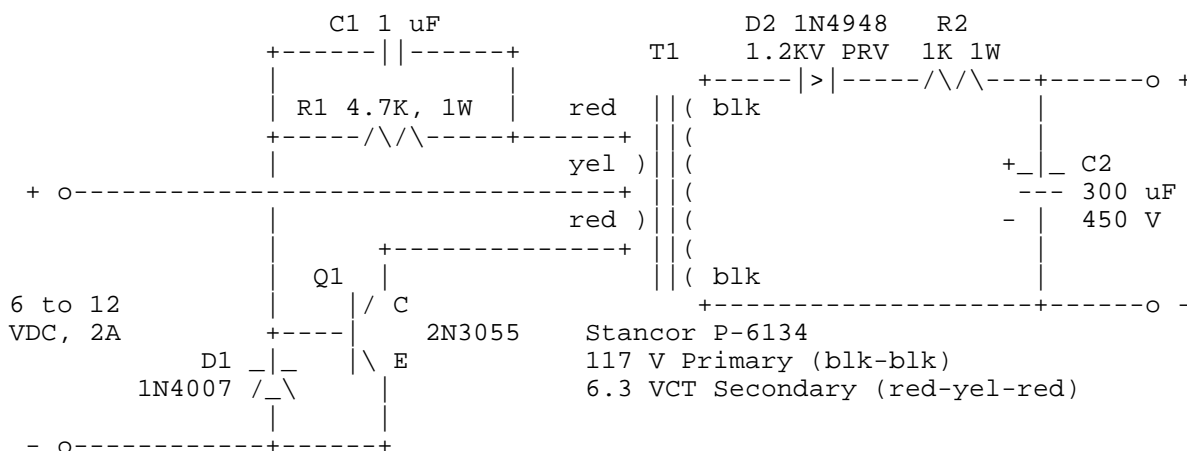
Except for the "[Super simple inverter](#)", these circuits were all reversed engineered from commercial products. The good news is that this means they probably all work somewhat reliably. The bad news is that a custom wound transformer (you can build in most cases) will be needed and there may be errors in the number of turns and wire sizes listed since these were all determined without totally dismembering the unit in question.

8.1) Super simple inverter

This circuit can be used to power a small strobe or fluorescent lamp. It will generate over 400 VDC from a 12 VDC, 2.5 A power supply or an auto or marine battery. While size, weight, and efficiency are nothing to write home about - in fact, they are quite pitiful - all components are readily available (even from Radio Shack) and construction is very straightforward. No custom coils or transformers are required. If wired correctly, it will work.

Output depends on input voltage. Adjust for your application. With the component values given, it will generate over 400 V from a 12 V supply and charge a 200 uF capacitor to 300 V in under 5 seconds.

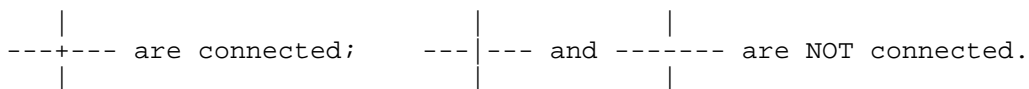
For your less intense applications, a fluorescent lamp can be powered directly from the secondary (without any other components). This works reasonably well with a F13-T5 or F15-T12 bulb (but don't expect super brightness). Q1 does get quite hot so use a good heat sink.



8.2) Notes on super simple inverter

1. Construction can take any convenient form - perf board, minibox, etc. Make sure the output connections are well insulated.
2. C1 must be nonpolarized type - not an electrolytic.
3. D1 provides a return path for the base drive and prevents significant reverse voltage on the B-E junction. Any 1 A or greater silicon diode should be fine.
4. C2 is shown as typical energy storage capacitor for strobe applications. Remove D2 and C2 for use with a fluorescent lamps.
5. D2 should be a high speed (fast recovery) rectifier. However, for testing, a 1N4007 should work well enough. R2 limits surge current through D2.
6. The polarity of the input with respect to the output leads is important. Select for maximum voltage by interchanging the black output wires.

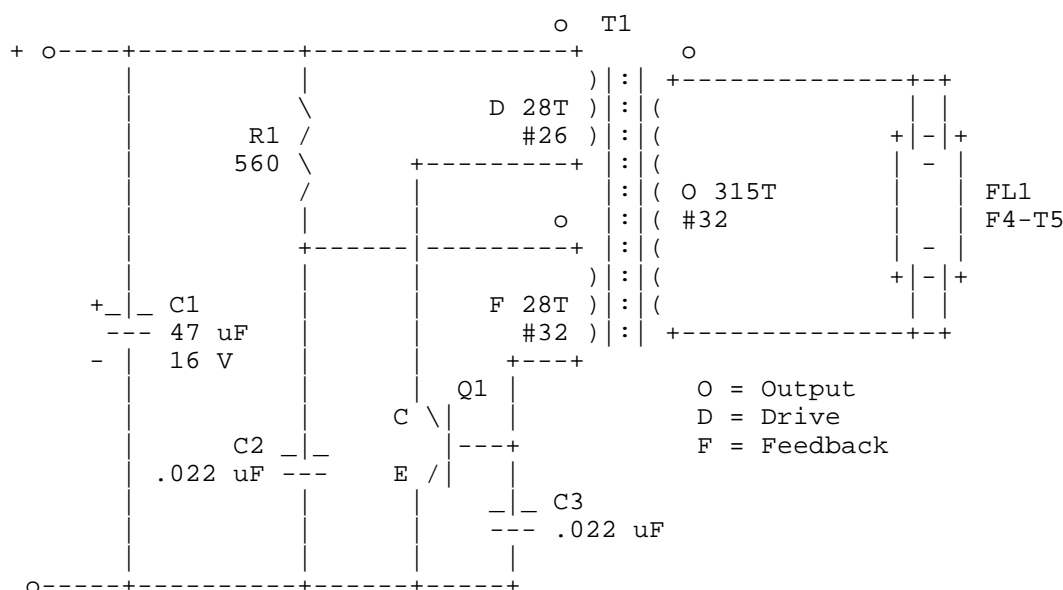
7. Mount Q1 (2N3055) on a heat sink if continuous operation is desired. It will get warm. Other NPN power transistors with $V_{ce0} > 80\text{ V}$, $I_c > 2\text{ A}$, and $H_{fe} > 15$ should work. For a PNP type, reverse the the polarities of the power supply and D1, and interchange one set of leads (where a diode is used for DC output).
8. Some experimentation with component values may improve performance for your application.
9. When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by R1 and C1 (and the gain of your particular transistor).
10. WARNING: Output is high voltage and dangerous even without large energy storage capacitor. With one, it can be lethal. Take appropriate precautions.
- 11.



8.3) Archer mini flashlight fluorescent lamp inverter

The circuit below was reverse engineered from the Archer model number 61-3724 mini fluorescent/incandescent flashlight combo (no longer in the Radio Shack catalog). The entire inverter fits in a space of 1-1/8" x 1" x 3/4". It is powered by 3 C size Alkaline cells and drives a F4-T5 tube.

This design can easily be modified for many other uses at lower or higher power.



8.4) Notes on Archer mini flashlight fluorescent lamp inverter

1. T1 is an E-core ferrite transformer. The core is 5/8" x 3/4" x 3/16" overall. The outer legs of the core are 1/8" thick. The central leg is 3/16" square. The square nylon bobbin has a diameter of 5/16". There is a .020" gap (spacer) in between the two halves of the E-core.

The 315T O (Output) is wound first followed by the 28T D (Drive) and 28T F (Feedback) windings. There should be a strip of mylar insulating tape between each of the windings.

The number of turns were estimated without disassembly as follows:

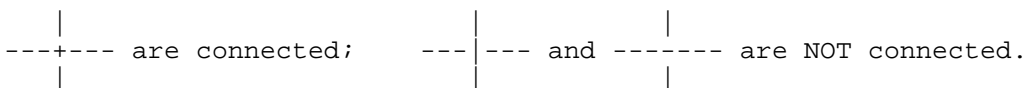
- * The wire sizes were determined by matching the diameters of the visible ends of the wire for each winding to magnet wire of known AWG.
- * The number of turns in the Output winding was determined based on its measured resistance, core diameter, and the wire gauge tables.
- * A 50 KHz .1 V p-p signal was then injected into the Feedback winding. The amplitudes of the resulting outputs from the Drive and Output windings were then measured. From these, the ratios of the number of turns were calculated.

2. The transistor was totally unmarked. A general purpose NPN medium power transistor like a 2N3053 or ECG24 should work. For PNP types, reverse the polarities of the power supply and C1.

Since it is very low power, no heat sink is used in the Archer flashlight. However, for other applications, one may be needed.

3. Some experimentation with component values may improve performance for your application.
4. When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by C2 and C3, the number of turns on each of the windings of T1, and the gain of your particular transistor.
5. WARNING: Output is high voltage and dangerous. Take appropriate precautions.

6.

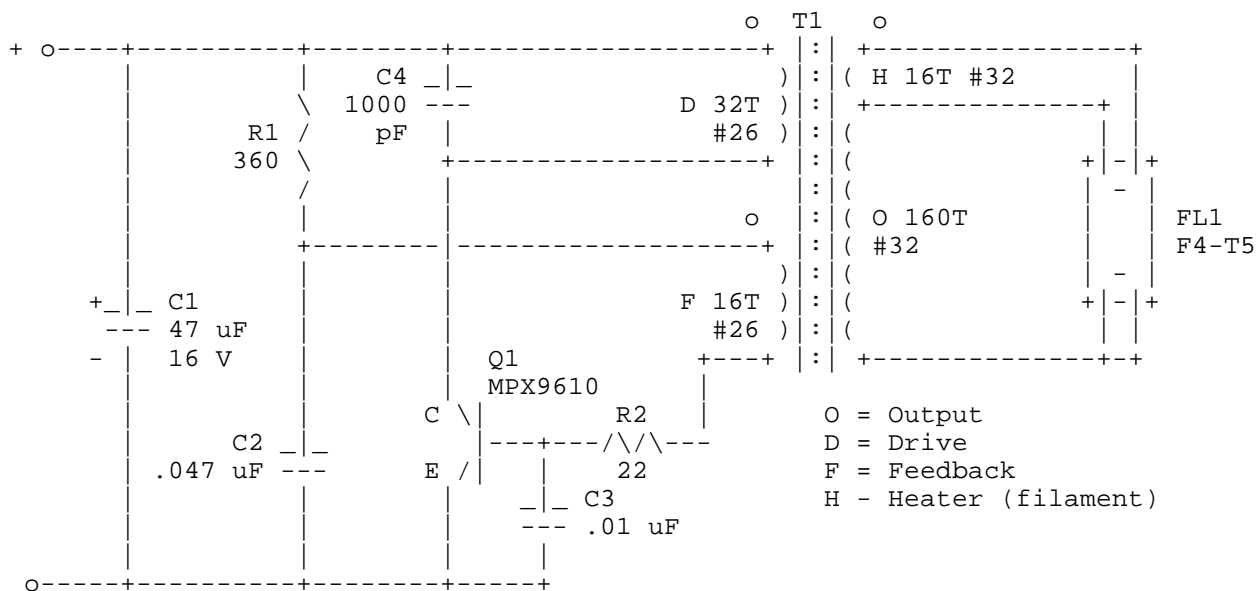

 ---+--- are connected; ---|--- and ---|--- are NOT connected.

8.5) Energizer mini flashlight fluorescent lamp inverter

The circuit below was reverse engineered from the Energizer model number unknown (worn off) mini fluorescent/incandescent flashlight combo. The entire

inverter fits in a space of 1-1/8" x 1-1/8" x 3/4". It is powered by 4 AA size Alkaline cells and drives a F4-T5 tube.

This design is very similar to the Archer model (see the section: "[Archer mini flash](#)" actually heating one of the filaments of the T5 lamp. Thus, a lower voltage transformer can be used.



8.6) Notes on Energizer mini flashlight fluorescent lamp inverter

1. T1 is an E-core ferrite transformer. The core is 1/2" x 5/8" x 3/16" overall. The outer legs of the core are 3/32" thick. The central leg is 3/16" square. The square nylon bobbin has a diameter of 5/16". There is a .010" (estimate) gap (spacer) in between the two halves of the E-core.

The 160T O (Output) is wound first followed by the 16T H (Heater), 32T D (Drive), and 16 T F (Feedback) windings. There should be a strip of mylar insulating tape between each of the windings.

The number of turns were estimated after unsoldering the transformer from the circuit board as follows:

- * The wire sizes were determined by matching the diameters of the visible ends of the wire for each winding to magnet wire of known AWG.
- * The number of turns in the Output winding was determined based on its measured resistance, core diameter, and the wire gauge tables.
- * A 100 KHz .1 V p-p signal was then injected into the Drive winding. The amplitudes and phases relationship of the resulting outputs from the Feedback, Heater, and Output windings were then measured. From these, the ratios of the number of turns and winding start/end were determined.

2. The transistor was an MPX9610. I was not able to locate specs for this part number but a transistor like a 2N3053 or ECG24 should work. For PNP

types, reverse the polarities of the power supply and C1.

Since it is very low power, no heat sink is used in the Energizer flashlight. However, for other applications, one may be needed.

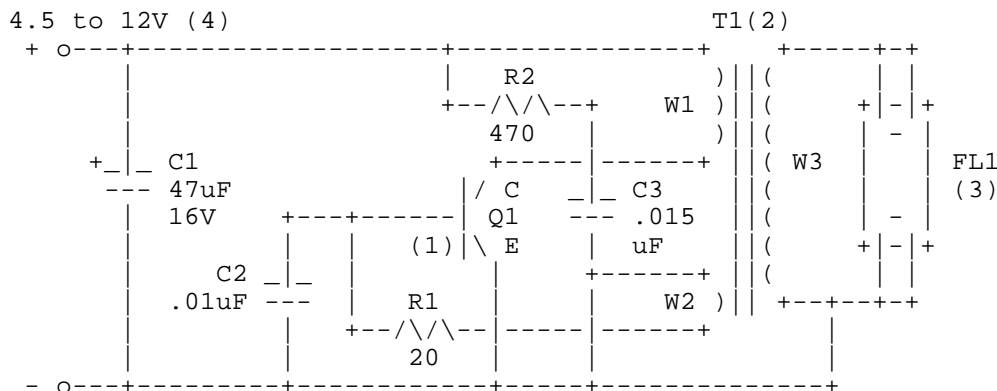
3. Some experimentation with component values may improve performance for your application.
4. When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by C2 and C3, the number of turns on each of the windings of T1, and the gain of your particular transistor.
5. WARNING: Output is high voltage and dangerous. Take appropriate precautions.
- 6.

---+--- are connected; ---|--- and ---|--- are NOT connected.

8.7) Pocket fluorescent blacklight inverter GH-RV-B1

(Schematic from: Axel Kanne (axel.k@swipnet.se)).

This was reverse engineered from a toy pocket blacklight, made in China. It has been tested with tubes up to 6 W.



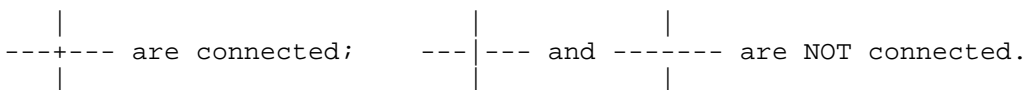
8.8) Notes on Pocket blacklight inverter

1. The original transistor is marked 8050 C0ZC. A 2N3055 works better than the original, the tube starts faster and the transistor runs much cooler.
2. T1 is a ferrite E-core transformer measuring 17mm x 15mm x 15mm. The core seems to be 5 mm thick. The turns ratio has not been determined. Winding W1 is made of ~0.2 mm wire, the resistance is below 1 ohm. The data for winding W2 is the same as winding W1. Winding W3 is made of ~0.5 mm wire

and its resistance is 5 ohms.

3. The original tube is an F4T5BLB blacklight tube, but the inverter has been tested with an ordinary F4T5 tube as well as a Philips 6W tube. The 6W tube causes the original transistor to run quite hot, so using a 2N3055 or similar power NPN is recommended.
4. 4.5V seems to be the absolute minimal voltage required to start an F4T5 tube. 5V will start the 6W tube when a 2N3055 transistor is used. Voltage can probably be cranked up above 12V, but that was the highest I tried (Didn't want to test when the tube blows).
5. CAUTION: The inverter can give a nice(?) shock when run with the original transistor on 5V. With a 2N3055 and higher supply voltage, it can be nasty. Avoid touching the tube terminals. The bottom of the PCB can also give quite suprise, as I discovered :-(.

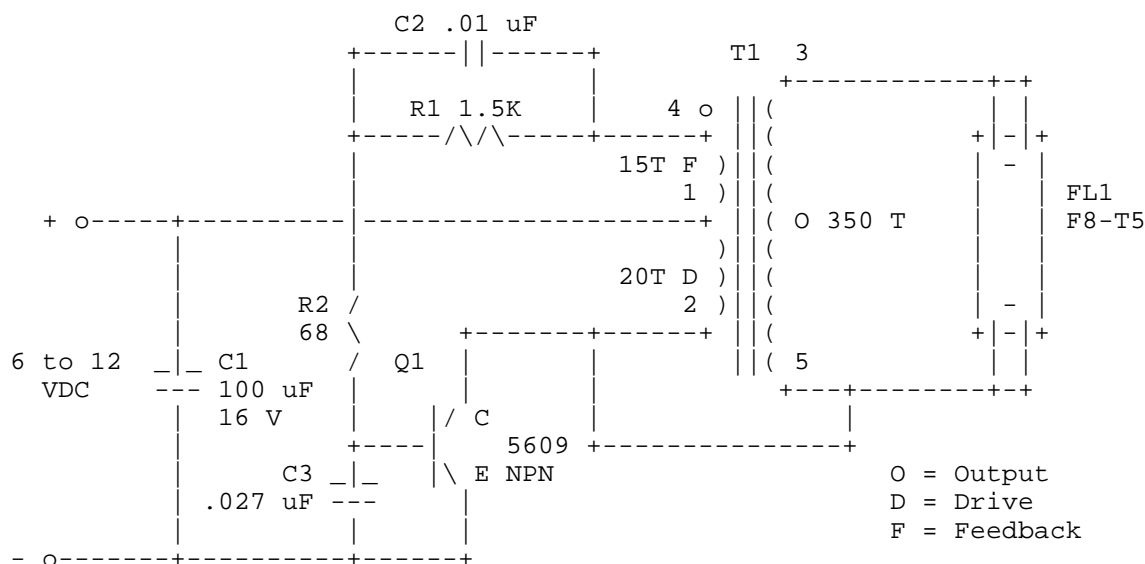
6.



8.9) Low power fluorescent lamp inverter 1

The circuit below was reverse engineered from a model number FL-12 'Made in Hong Kong' battery (8 AA cells) or 12 V wall adapter powered portable fluorescent lamp. The bulb is an F8-T5.

This design can easily be modified for many other uses at lower or higher power. Note that its topology is similar to that of the circuit described in the section: "[Super simple inverter](#)".



8.10) Notes on low power fluorescent lamp inverter 1

1. T1 is an E-core ferrite transformer. The core is 5/8" x 3/4" x 3/16" overall. The outer legs of the core are 3/32" thick. The central leg is 3/16" square. The square nylon bobbin has a diameter of 5/16". There is no visible spacer between the cores but I did not disassemble to confirm.

The 350T O (Output) is wound first followed by the 25T D (Drive) and 18T F (Feedback) windings. There should be a strip of mylar insulating tape between each of the windings.

The number of turns were estimated without disassembly as follows:

- * The resistances of each of the windings was measured to determine the arrangement of the transformer.
- * The inverter was run at just enough input voltage for it to oscillate (so the load of the fluorescent tube would not affect the readings) and the voltages on all 3 windings were measured on an oscilloscope. From this, the ratios for the windings were determined.
- * An estimate was made of the number of turns likely to be on the Drive winding based on other similar designs. The number of turns on the other windings were calculated based on the turns ratios. Wire size is probably #36 AWG.

2. The transistor was marked 5609 which I could not cross to anything. I would guess that a general purpose medium NPN power transistor like a 2N3053 or ECG24 should work. For a PNP type, reverse the polarities of the power supply and C1.

Since it is very low power, no heat sink is used in this lamp. However, for other applications, one may be needed.

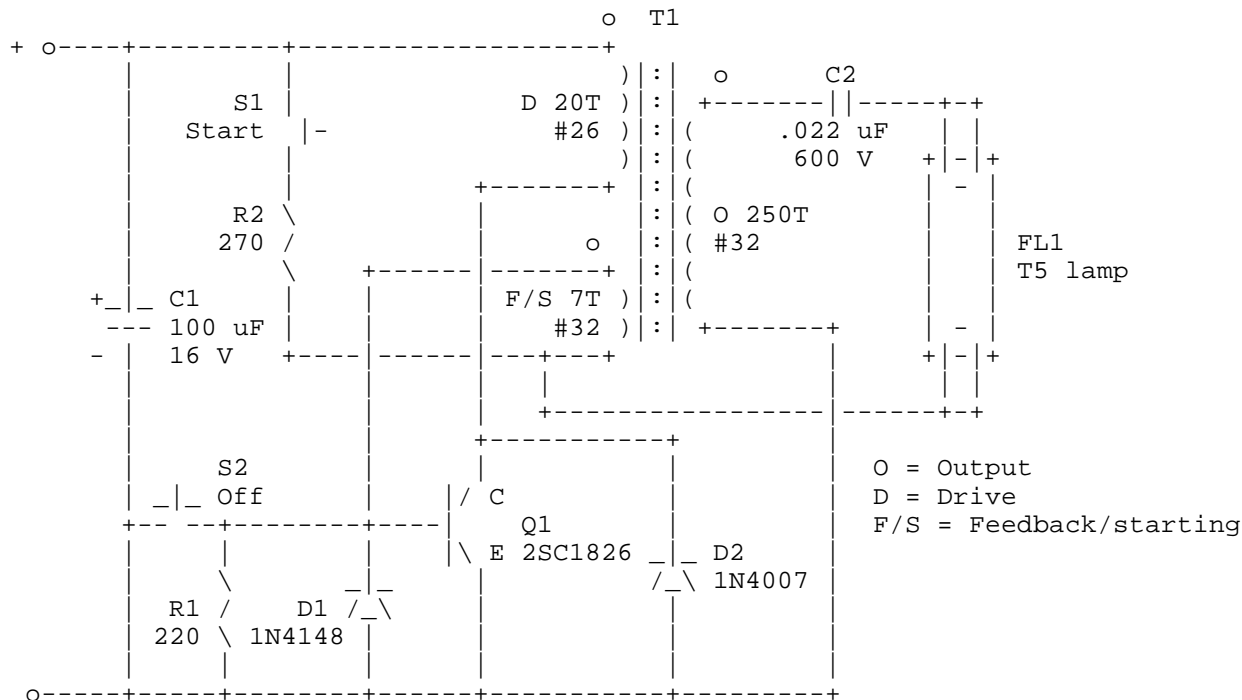
3. Some experimentation with component values may improve performance for your application.
4. When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by C2, C3, R1, R2, the number of turns on each of the windings of T1, and the gain of your particular transistor.
5. WARNING: Output is high voltage and dangerous. Take appropriate precautions.
- 6.

---+--- are connected; ---|--- and ---|--- are NOT connected.

8.11) Low power fluorescent lamp inverter 2

The circuit below is the type used in inexpensive fluorescent camping lanterns. In this particular model, an F6-T5 lamp was used. It will drive F4-T5 to F13-T5 tubes depending on input voltage. The power source can be a 4 to 9 V, 2 A power supply (depending on the size of your lamp) or a suitable battery pack. This design was reverse engineered from a random commercial unit of

unknown manufacture using a lead-acid battery battery that expired long ago.



The approximate measured operating parameters are shown in the chart below. The two values of input current are for starting/running (starting is with the Start button, S1, depressed).

Lamp type ---->	F4-T5	F6-T5	F13-T5
V(in)	I(in)	I(in)	I(in)
3 V	.9/.6 A	-	-
4 V	1.1/.7 A	1.1/.8 A	-
5 V	1.3/.8 A	1.2/.9 A	-
6 V	-	1.4/1.0 A	1.6/.95 A
7 V	-	-	1.7/1.0 A
8 V	-	-	1.8/1.2 A
9 V	-	-	2.1/1.3 A
10 V	-	-	2.2/1.4 A

8.12) Notes on low power fluorescent lamp inverter 2

- Construction can take any convenient form - perf board, minibox, etc. Make sure the output connections are well insulated.
- T1 is assembled on a square nylon bobbin, 3/8" cubed. Wind the 250T O (Output) first, insulate with mylar tape, 20T D (Drive) next, and 7T F/S (Feedback/Starting) last. Observe directions of windings as indicated by the dots (o). The number of turns for the O winding was estimated based on measured winding resistance, wire size, and the dimensions of the bobbin.

The core is just a straight piece of ferrite 1/4" x 1/4" x 1-3/8" It is fully open - there is no gap.

- Any general purpose NPN power transistor with $V_{ceo} > 80 \text{ V}$, $I_c > 2 \text{ A}$, and $H_{fe} > 15$ should work. For a PNP type, reverse the polarities of the power supply, C1, D1, and D2.

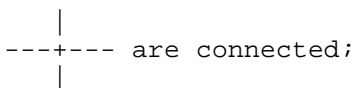
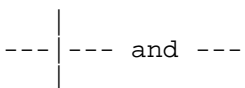
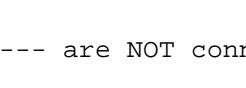
Use a good heat sink for continuous operation at higher power levels (6 V input or above). The type used (2SC1826) was a replacement after I fried the unidentified transistor originally installed (103-SV2P001).

- Pushbutton switches are used to control operation. S1 (Start) provides initial base drive to the transistor via the Feedback/Starting winding of T1 until the tube arc is established. At that point, feedback is sustained via current flowing through the tube. S2 (Off) shorts the base of the transistor to ground to stop the oscillator.

Like a regular manual start preheat fluorescent fixture, the start switch, must be depressed until the lamp comes on at full brightness indicating that the filaments are adequately heated.

- Some experimentation with component values may improve performance for your application.
- When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by R1 and R2 (during starting in particular), the number of turns on each of the windings of T1, and the gain of your particular transistor.
- WARNING:** Output is high voltage and dangerous. Take appropriate precautions.

8.


 are connected;
 
 and
 
 are NOT connected.

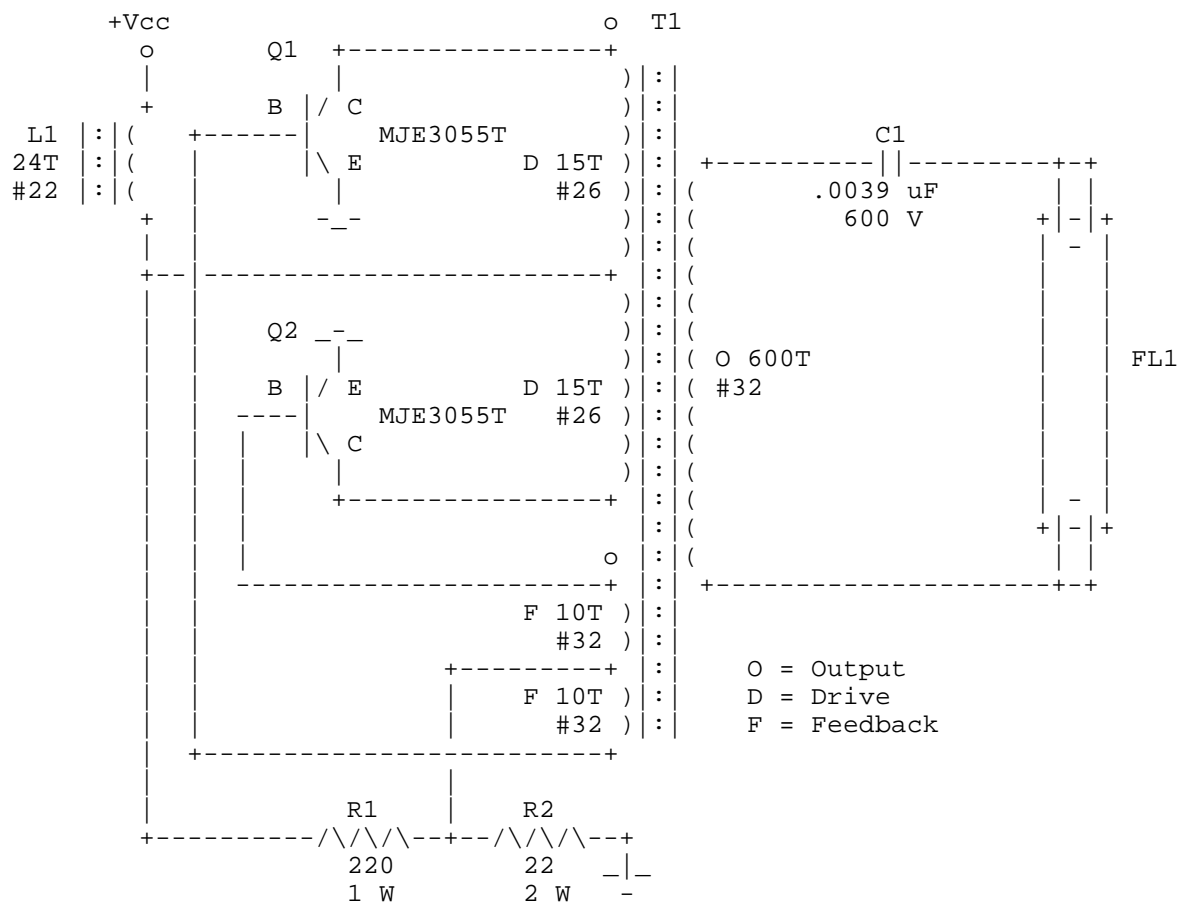
8.13) Medium power fluorescent lamp inverter

This circuit is capable of driving a variety of fluorescent lamps from a 4 to 12 V, 2 to 2.5 A DC power supply, rechargeable battery pack, or auto or marine battery. With appropriate modifications (if needed) it may be used for other applications like powering an electronic flash or HeNe laser tube. The transformer will need to be custom wound (by you) but this is not really difficult - just slightly time consuming for the 600 turn 0 (Output) winding if you don't have a coil winding machine.

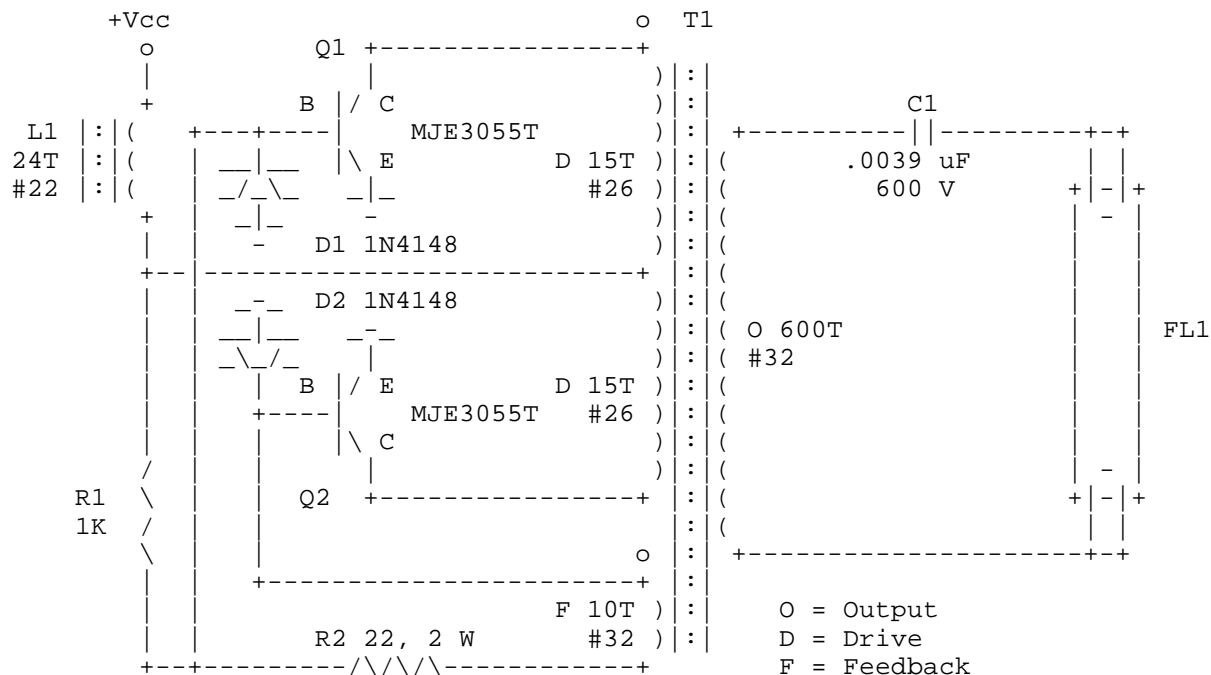
I have used it with fluorescent tubes of many sizes: F6-T5, F13-T5, F15-T12, and F20-T12. The arc will be sustained with the filaments hot on an input as low as about 3.5 to 4 V (with a new tube) but during starting, an input voltage of about 5 or 6 V may be needed until the filaments are hot enough to sustain the arc at the lower voltage.

Two nearly identical circuits are shown.

- * This design saves a couple of diodes but requires a centertapped feedback winding on the transformer. The input voltage must exceed about 4 V for oscillation to commence:



* The following slightly modified design starts oscillating at a very low input voltage (under 2 V). This may be beneficial when driving small lamps. The circuit behaves quite similarly in all other respects.



The switching frequency is about 21 KHz and varies less than 5 percent over

the range of input voltage for which the bulb remains lit (it is significantly higher with no load - about 140 KHz). An input voltage of about 4 V is needed to start oscillation (reducing R1 or increasing R2 would lower this at the expense of efficiency at higher voltages) but it will continue well below 3 V.

The measured input current at various input voltages for two lamp types are shown in the chart below. SV (Starting Voltage) is the minimum input voltage required to preheat the filaments before the lamp will turn on (current is lower until filaments are hot). FB (Full Brightness) is the point at which the lamp appears to be operating at the same intensity as if it were installed in a normal 115 VAC fixture.

Lamp type --->	F13-T5	F20-T12
V(in)	I(in)	I(in)
3 V	-	1.37 A
4 V	1.76 A	1.52 A (SV)
5 V	1.80 A (SV)	1.60 A
6 V	1.90 A	1.65 A
7 V	1.96 A (FB)	1.70 A
8 V	2.02 A	1.80 A
9 V	2.16 A	1.90 A
10 V	2.33 A	2.05 A
11 V	-	2.30 A (FB)
12 V	-	2.60 A

8.14) Notes on medium power fluorescent lamp inverter

1. T1 is an E-core ferrite transformer. Once complete, the cores are installed on the bobbin with a 2 mm gap. Some experimentation with the core gap may be needed to optimize performance for a given lamp type and input voltage.

Each E core is 1" x 1/2" x 1/4" overall. The outer legs of the core are 1/8" thick. The central leg is 1/4" square. The square nylon bobbin has a diameter of 5/16" and length of 3/8".

The 600T O (Output) is wound first followed by the 15T D (Drive) and 10T F (Feedback) windings. For convenience, wind the D and F windings bifiler style (the two wires together). Determine the appropriate connections with an ohmmeter (or label the ends). The centertaps are brought out to terminals. Try to distribute the O winding uniformly across the entire bobbin area by winding it in multiple layers. This will assure that no wires with a significant voltage difference are adjacent. There should be a strip of insulating tape between the O and the other windings.

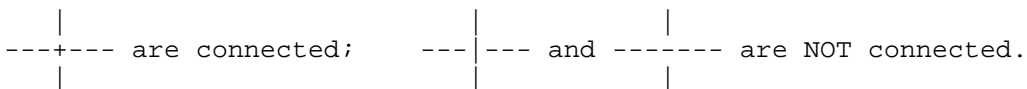
2. L1 isolates the power supply. It is 24 turns of #22 wire wound on a 1/4" ferrite core. The inverter works fine without L1 but seems to have a tad more strength at low voltage with it.
3. The transistors are MJE3055T (2N3055 in a TO220 package) types but are not critical. However, I expect that some faster switching transistors would run cooler. Any fast switching NPN power transistor with $V_{ceo} > 80$ V, $I_c > 3$ A, and $H_{fe} > 15$ should work. For PNP types, reverse the polarity of the power supply.

For operation above about 6 V, a pair of good heat sinks will be required. However, power dissipation in the transistors does not seem to increase as much as expected - the base drive is probably more optimal at higher

input voltage.

4. Some experimentation with component values may improve performance for your application.
5. When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by C1, the number of turns on each of the windings of T1, the gap of the core of T1, and the gain of your particular transistor. If the circuit does not start oscillating, interchange the F winding connections to Q1 and Q2.
6. WARNING: Output is high voltage and dangerous. Take appropriate precautions.

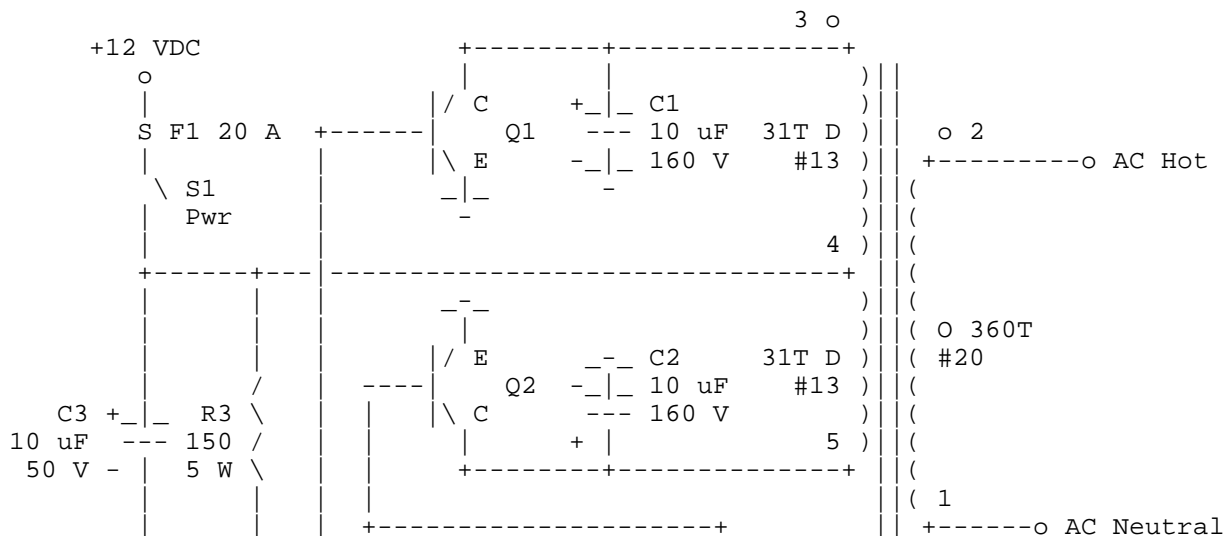
7.

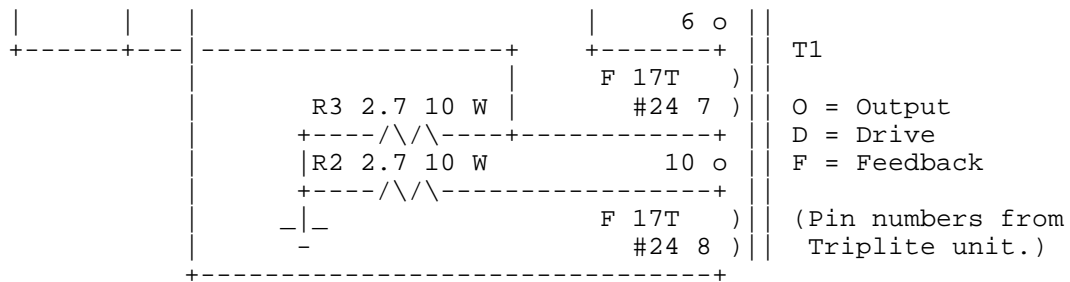


8.15) Basic 200 W power inverter

This circuit was reverse engineered from a Tripp-Lite "Power-Verter" Model PV200 DC to AC Inverter - typical of those used for camping or boating applications where the only source of power is an auto or marine battery. This particular model is rated 200 W continuous. The output is a 60 Hz squarewave and there is no regulation or precise frequency control. (Unlike the other circuits in this collection, it is NOT a high frequency inverter.)

Modifications for higher or lower output voltage are easily achieved. For example, a fast cycle strobe requiring 330 VDC, would only require using three times the number of turns on the Output winding and the addition of a bridge rectifier to charge the energy storage capacitor(s). Alternatively, the inverter could be used as-is with the addition of a voltage tripler. A tripler rather than doubler is needed because of the squarewave output. (The RMS and peak voltages are the same so you don't get the boost of 1.414 as you do with the sinusoidal waveform from the power company.)





8.16) Notes on basic power inverter

1. Construction was all done point-to-point - there is no circuit board. Layout appears not to be critical.
2. T1 is a relatively large heavy laminated E-I core transformer. The E and I sheets alternate direction to assure a low reluctance magnetic circuit.

The core dimensions are 3-3/4" x 3-1/8" x 1-1/8" overall. The outer legs of the core are 5/8" thick. The central leg is 1" wide. The square bobbin has a diameter of 1-3/8".

The 360T O (Output) secondary is wound first as 4 or 5 insulated layers followed by the 31T D (Drive) and 17T F (Feedback) windings. There are insulating layers between each of the windings.

The number of turns were estimated without disassembly as follows:

- * The wire sizes were determined by matching the diameters of the visible ends of the wire for each winding to magnet wire of known AWG and/or measuring with a micrometer where possible. (The Drive windings are actually wound using square cross-section magnet wire for maximum packing density. This was estimated to be equivalent to #13 AWG round wire.)
- * The number of turns in the Output winding was determined based on its measured resistance, core diameter, and the wire gauge tables.
- * The inverter was run and the amplitudes of the signals on each winding were measured. From these ratios, the number of turns were calculated.

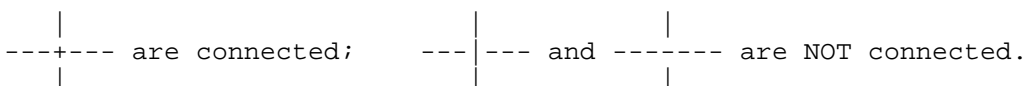
2. The transistor were marked 69-206. ECG29 is a close match - high power amplifier switch - 80 V, 50 A, 300 W, Hfe 20 min. 2SD797 is another readily available power transistor that should work. For PNP types, reverse the polarities of the power supply, C1, C2, and C3.

The transistors are mounted on heat sinks which form the sides of the case.

3. C3 and R3 are required for starting. Since there is no source of current for the bases of the transistors other than the Feedback windings, this provides a starting pulse to Q2 when the unit is switched on. Ramping the input voltage slowly rather than using the power switch would likely result in the inverter behaving like an inanimate object.
4. Measured frequency of operation was about 56 Hz. This is likely affected by nearly everything - input voltage, capacitance, core saturation, phase of the moon, etc. Therefore, don't expect to drive a clock mechanism from this thing with any accuracy!

5. Some experimentation with component values may improve performance for your application.
6. When testing, use a variable power supply so you get a feel for how much output voltage is produced for each input voltage. Component values are not critical but behavior under varying input/output voltage and load conditions will be affected by C2 and C3, the number of turns on each of the windings of T1, and the gain of your particular transistors. However, See note (3) about starting.
7. WARNING: Output is high voltage and dangerous - even more so if you increase its output for true HV applications. Over 200 W is available continuously. Take appropriate precautions.

8.


 are connected; ---|--- and ---|--- are NOT connected.

Chapter 9) Kevin's Strobe Schematics

9.1) High power inverter and trigger circuits

(From: Kevin Horton (khorton@tech.iupui.edu)).

I'm building a super strobe bar! It has 8 strobe tubes under computer control. (Actually a PIC processor, but hey, computer is a computer.) I have all the stuff done except the control section, and I only have 2 of the 8 strobe units done due to the fact that I haven't found any more cheap cameras at the thrift store! (One Saturday morning's worth of garage sales and flea markets would remedy that! --- sam).

It runs on 12 V, at up to 6 A, and can fire the tubes at a rate of about 8-10 times per second. The storage cap is a 210 uf, 330 V model; it gets to about 250 V to 300 V before firing; depending on how long it has had to charge. Because of this high speed, the tubes get shall we say, a little warm. (Well, maybe a lot warm --- sam). I have it set up at the moment driving two alternating 5 W-s tubes. I'm pumping them quite a bit too hard, as the electrodes start to glow after oh, about 5 seconds or so of continuous use. I know, a high class problem, indeed! My final assembly will have 8 tubes spaced about 8 inches apart on a 2x4, with a Plexiglass U-shaped enclosure with a nice 12 V fan blowing air through one end of the channel to cool the inverter and the tubes. Stay tuned.

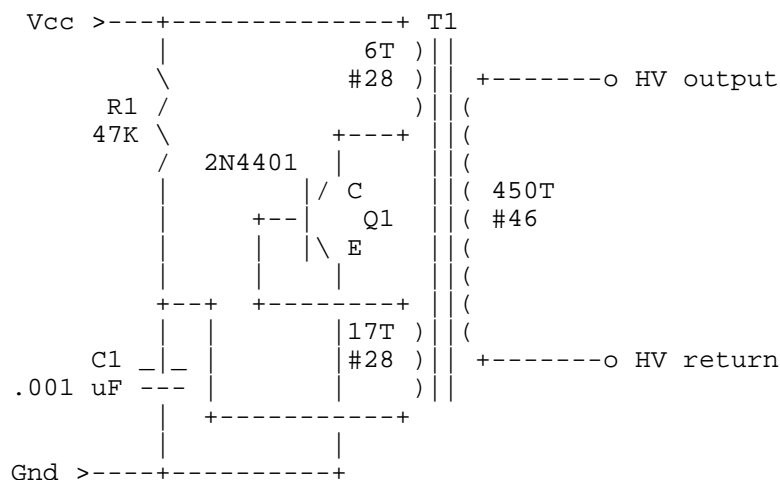
Inverter - High power 12 V to 300 V inverter for high repeat rate medium power strobes. Schematic in GIF format: [inverter.gif](#)

Trigger - Opto-isolated logic level trigger for general strobe applications. Schematic in GIF format: [trigger.gif](#)

9.2) Tiny tiny inverter design

I have developed a cool little transformer circuit that seems to be very efficient. I built this inverter as tiny as I could make it. It runs off of 3V, and charges up a little 1 uf 250V cap all the way up in about 30 seconds; drawing about 5 to 8 mA in the process. The numbers by the windings tell the number of turns. The primary and feedback windings are #28, while the secondary is #46. Yes, #46! I could hardly tell what gauge it was, as it was almost too small to measure with my micrometer! It may be #44 or #45, but at these sizes, who knows? I used a trigger transformer for the wire. I used all the wire on it, to be exact; it all **JUST** fit on the little bobbin. The primary went on the core first, then the secondary, and finally the feedback winding. This order is very important. I used a ferrite bobbin and corresponding ferrite 'ring' that fit on it. The whole shebang was less than 1 cm in diameter, and about 3-5 mm high! I gave it a coat of wax to seal things up, and made the inverter circuit with surface-mount parts, which I then waxed onto the top. There are two wires in, and two wires out. It's enough to run a neon fairly brightly at 1.2 V, with a 3 ma current draw.

Schematic in GIF format: [teeny.gif](#)



Chapter 10) IR Detector/Tester Circuits

Two approaches are shown below.

- * The first uses a bare photodiode as the sensor. It is simpler, lower power, and shouldn't care what, if any, modulation is used by the IR source.
- * An IR detector module salvaged from a TV or VCR, or purchased from Radio Shack or elsewhere may be used instead of a photodiode. This will have a much greater dynamic range (response to both weak and powerful signals) than a simple photodiode. However, some of these assume a particular modulation frequency and will be blind to anything else. Power requirements may also be more restrictive - it may insist on regulated 12 V).

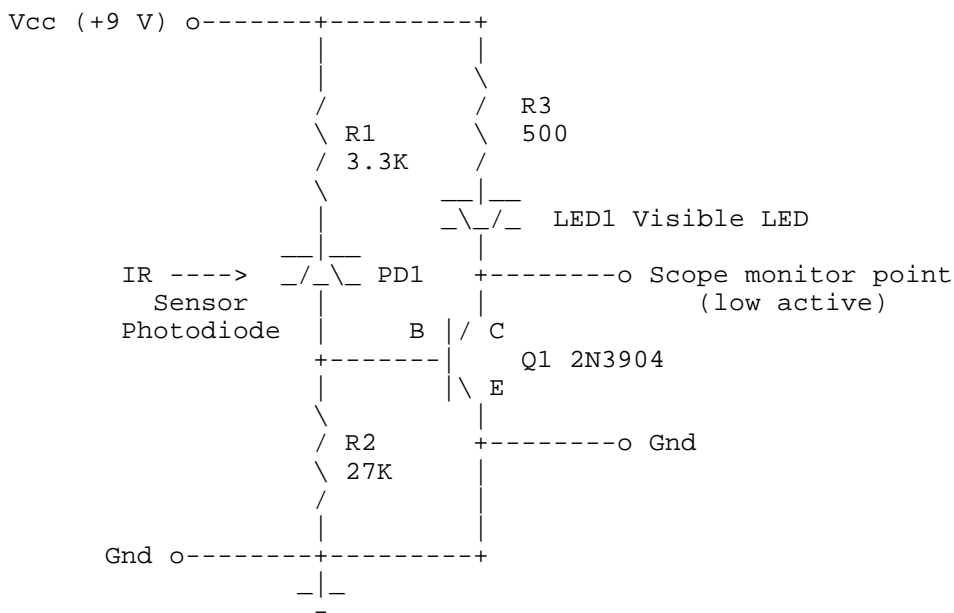
10.1) IR detector circuit using bare photodiode

This IR Detector may be used for testing of IR remote controls, CD player laser diodes, and other low level near IR emitters. It will not have the sensitivity or dynamic range of the approach described in the section: "[IR detector of IR falling within the wavelength range of the photodiode used since there is not demodulation or coupling circuitry to get in the way.](#)

IR radiation falling on the photodiode causes current to flow through R1 to the base of Q1 switching it and LED1 on.

Component values are not critical. Purchase photodiode sensitive to near IR - 750-900 um or salvage from optocoupler or photosensor. Dead computer mice, not the furry kind, usually contain IR sensitive photodiodes. For convenience, use a 9V battery for power. Even a weak one will work fine. Construct the circuit so that the LED does not illuminate the photodiode!

The detected signal may be monitored across the transistor with an oscilloscope.

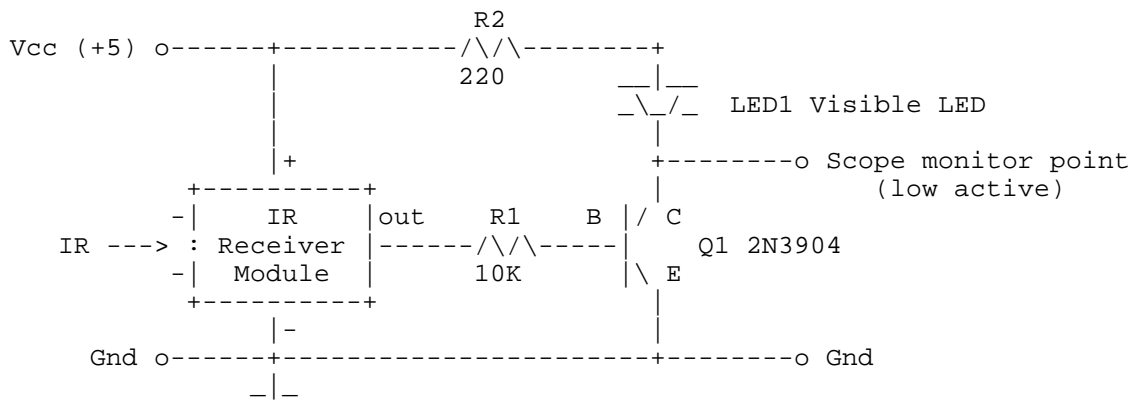


10.2) IR detector circuit using IR receiver module

This one uses an entire IR receiver module as the IR sensor. Its sensitivity and dynamic range will be much better than the circuit described in the section: "[IR detector circuit using bare photodiode](#)" since these modules have automatic gain control circuitry built in. However, some modules are tuned to a particular modulation frequency and/or are AC coupled and will not respond to all remotes or other pulsed or continuous IR sources.

The IR receiver module from a TV, VCR, or purchased from Radio Shack or elsewhere, drives the base of Q1 through R1. It may even be possible to eliminate the transistor circuit entirely and connect the LED directly to the module's output (in series with a current limiting resistor to Vcc or Gnd) but that depends on the drive capabilities of the module. You can use whatever Vcc is required for the IR receiver module for the LED circuit as well but may need to change the value of R2 to limit the current to the LED to less than its maximum rating.

The specific case where Vcc is +5 V is shown.



Chapter 11) Basic Incandescent Light Dimmer Circuits

These are the type of common light dimmers (e.g., replacements for standard wall switches) widely available at hardware stores and home centers.

CAUTION: However, note that a dimmer should not be wired to control an outlet since it would be possible to plug a device into the outlet which might be incompatible with the dimmer resulting in a safety or fire hazard.

While designed for incandescent or heating loads only, these will generally work to some extent with universal motors as well as fluorescent lamps down to about 30 to 50 percent brightness. Long term reliability is unknown for these non-supported applications.

11.1) Simplest dimmer schematic

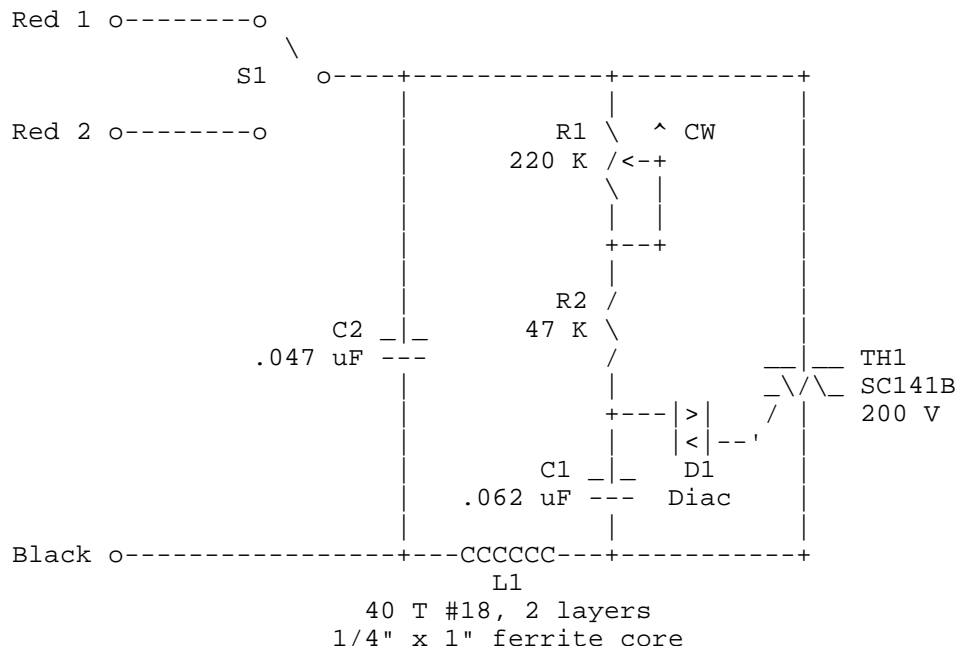
The first schematic is of a normal (2-way) inexpensive dimmer - in fact this contains just about the minimal number of components to work at all!

S1 is part of the control assembly which includes R1.

The rheostat, R1, varies the amount of resistance in the RC trigger circuit.

dimmer also includes a choke (L1) and capacitor (C2) to suppress Radio Frequency Interference (RFI). Operation is otherwise identical to that of the simpler circuit.

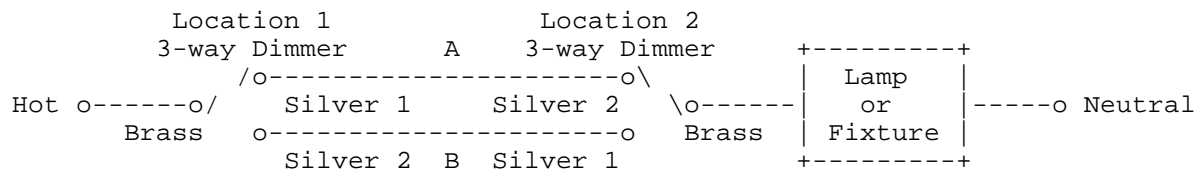
This type of 3-way dimmer can be used at only one end of a multiple switch circuit. All the other switches should be conventional 3-way or 4-way types. Thus, control of brightness is possible only from one location.



11.4) Simple 3-way dimmer schematic 2

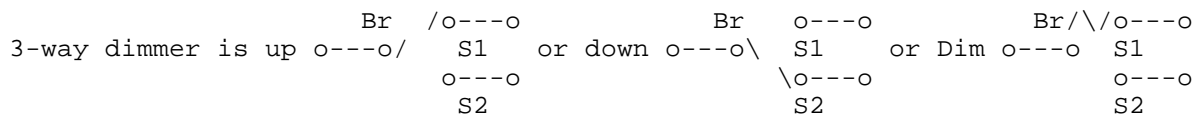
The schematic below is of a 3-way dimmer with a slightly more complex switching arrangement such that when the local dimmer is set to full on or full off, it is bypassed. (If you ignore the intermediate dimming range of the control, it behaves just like a normal 3-way switch.) With this scheme, it is possible to have dimmers at both locations without the dimmer circuitry ever being in series and resulting in peculiar behavior.

Whether this is really useful or not is another story. The wiring would be as follows:



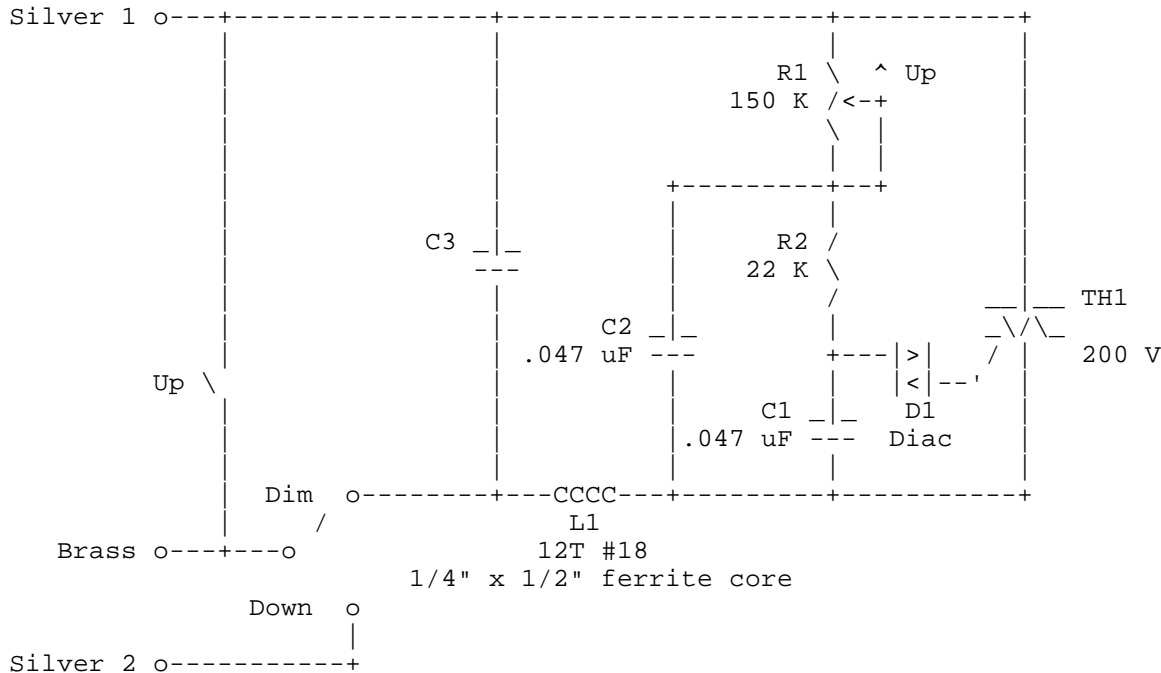
(If dimming interacts, interchange the A and B wires to the silver screws at one dimmer).

This one uses a toggle style potentiometer where the up and down positions operate the switches. Therefore, it has 3 states: Brass to Silver 1 (fully up), dim between Brass and Silver 1 (intermediate positions), and Brass to Silver 2 (fully down).



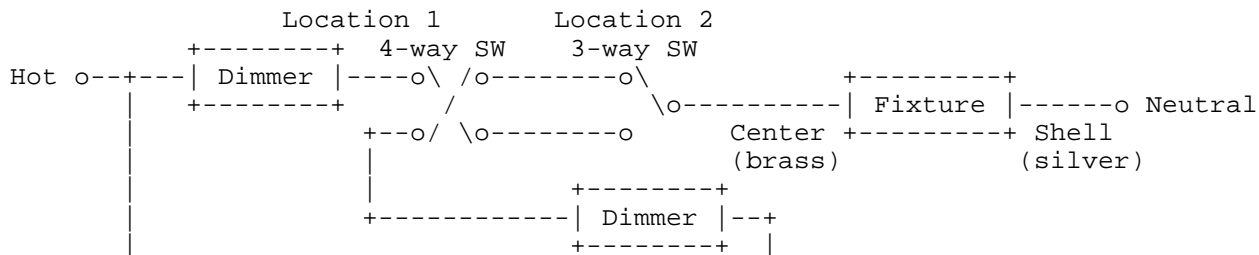
However, it is still not possible to have totally independent control - local behavior differs based on the setting of the remote dimmer (details left as an exercise for the reader).

Like the previous circuit, this dimmer also includes a choke (L1) and capacitor (C3) to suppress Radio Frequency Interference (RFI). It is just a coincidence (or a matter of cost) that the 3-way dimmers have RFI filters and the 2-way type shown above does not.



11.5) Independent dimming from two locations - kludge #3251

Here is a scheme which will permit dimming with independent control from two locations. Each location will have a normal switch and a dimmer knob. The toggle essentially selects local or remote but like normal 3-way switches, the actual position depends on the corresponding setting of the other switch:



+-----+

As usual, the brass screw on the fixture or outlet should be connected to the Hot side of the wiring and the silver screw to the Neutral side.

The dimmers can be any normal knob or slide type with an off position.

Note that as drawn, you need 4 wires between switch/dimmer locations. 4-way switches are basically interchange devices - the connections are either an X as shown or straight across. While not as common as 3-way switches, they are available in your favorite decorator colors.

If using Romex type cable in between the two locations, make sure to tape or paint the ends of the white wires black to indicate that they may be Hot as required by Code.

And, yes, such a scheme will meet Code if constructed using proper wiring techniques.

No, I will not extend this to more than 2 locations!

CAUTION: However, note that a dimmer should not be wired to control an outlet since it would be possible to plug a device into the outlet which might be incompatible with the dimmer resulting in a safety or fire hazard.

Chapter 12) Simple Power Supplies

This is a (currently somewhat meager) collection of basic power supply circuits that will hopefully grow as time passes.

12.1) Converting an AC output wall adapter to DC

Where a modest source of DC is required for an appliance or other device, it may be possible to add a rectifier and filter capacitor (and possibly a regulator as well) to a wall adapter with an AC output. While many wall adapter output DC, some - modems and some phone answering machines, for example - are just transformers and output low voltage AC.

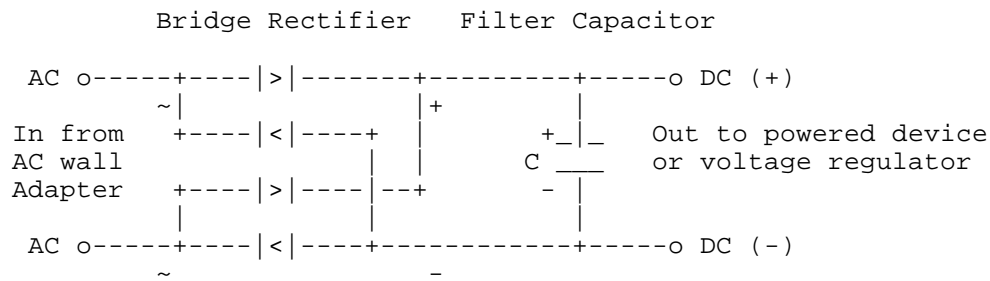
This is also the simplest and safest way to construct a small DC power supply as you do not need to deal with the 110 VAC at all.

To convert such an adapter to DC requires the use of:

- * Bridge rectifier - turns AC into pulsating DC.
- * Filter capacitor - smooths the output reducing its ripple.
- * Regulator - produces a nearly constant output voltage.

Depending on your needs, you may find a suitable wall adapter in your junk box (maybe from that 2400 baud modem that was all the rage a couple of years ago!).

The basic circuit is shown below:



Considerations:

- * An AC input of V_{in} VRMS will result in a peak output of approximately $1.4 V_{in} - 1.4 V$. The first factor of 1.4 results from the fact that the peak value of a sinusoid (the power line waveform) is $1.414 (\sqrt{2})$ times the RMS value. The second factor of 1.4 is due to the two diodes that are in series as part of the bridge rectifier. The fact that they are both about 1.4 is a total coincidence.

Therefore, you will need to find an AC wall adapter that produces an output voltage which will result in something close to what you need. However, this may be a bit more difficult than it sounds since the nameplate rating of many wall adapters is not an accurate indication of what they actually produce especially when lightly loaded. Measuring the output is best.

- * Select the filter capacitor to be at least 10,000 μF per 1000 mA of output current with a voltage rating of at least $2 \times V_{in}$. This rule of thumb will result in a ripple of less than 1 V p-p which will be acceptable for many devices or where a voltage regulator is used (but may be inadequate for some audio devices resulting in some 120 Hz hum. Use a larger or additional capacitor or a regulator in such a case.
- * Suitable components can be purchased at any electronics distributor as well as Radio Shack. The bridge rectifier comes as a single unit or you can put one together from 1N400x diodes (the x can be anything from 1 to 7 for these low voltage applications). Observe the polarity for the filter capacitor!

The following examples illustrate some of the possibilities.

- * Example 1: A typical modem power pack is rated at 12 VAC but actually produces around 14 VAC at modest load (say half the nameplate current rating). This will result in about 17 to 18 VDC at the output of the rectifier and filter capacitor.
- * Example 2: A cordless VAC battery charger adapter might produce 6 VAC. This would result in 6 to 7 VDC at the output of the rectifier and filter capacitor.

Adding an IC regulator to either of these would permit an output of up to about 2.5 V less than the filtered DC voltage.

12.2) Adding an IC regulator to a wall adapter or battery

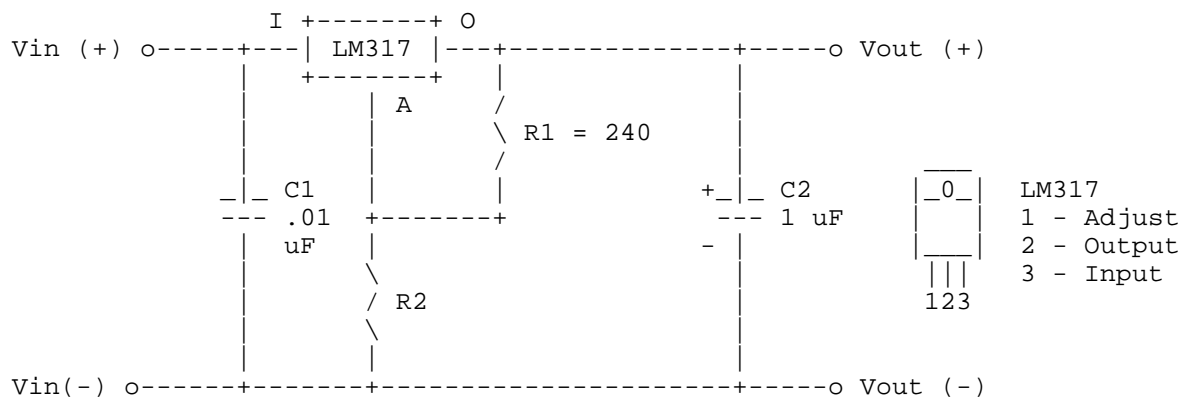
For many applications, it is desirable to have a well regulated source of DC power. This may be the case when running equipment from batteries as well as from a wall adapter that outputs a DC voltage or the enhanced adapter

described in the section: "[Converting an AC output wall adapter to DC](#)".

The following is a very basic introduction to the construction of a circuit with appropriate modifications will work for outputs in the range of about 1.25 to 35 V and currents up 1 A. This can also be used as the basis for a small general purpose power supply for use with electronics experiments.

What you want is an IC called an 'adjustable voltage regulator'. LM317 is one example - Radio Shack should have it along with a schematic. The LM317 looks like a power transistor but is a complete regulator on a chip.

Here is a sample circuit:



Note: Not all voltage regulator ICs use this pinout. If you are not using an LM317, double check its pinout - as well as all the other specifications.

For the LM317:

1. $R2 = (192 \times V_{out}) - 240$, where R2 in ohms, Vout is in volts and must be at between 1.2 V and 35 V.
2. Vin should be at least 2.5V greater than Vout. Select a wall adapter with a voltage at least 2.5 V greater than your regulated output at full load.

However, note that a typical adapter's voltage may vary quite a bit depending on manufacturer and load. You will have to select one that isn't too much greater than what you really want since this will add unnecessary wasted power in the device and additional heat dissipation.

3. Maximum output current is 1 A. Your adapter must be capable of supplying the maximum current safely and without its voltage drooping below the requirement in (2) above.
4. Additional filter capacitance (across C1) on the adapter's output may help (or be required) to reduce its ripple and thus the swing of its input. This may allow you to use an adapter with a lower output voltage and reduce the power dissipation in the regulator as well.

Using 10,000 uF per *amp* of output current will result in less than 1 V p-p ripple on the input to the regulator. As long as the input is always greater than your desired output voltage plus 2.5 V, the regulator will totally remove this ripple resulting in a constant DC output independent of line voltage and load current fluctuations. (For you purists, the regulator isn't quite perfect but is good enough for most applications.)

Make sure you select a capacitor with a voltage rating at least 25% greater than the adapter's *unloaded* peak output voltage and observe the polarity!

Note: wall adapters designed as battery chargers may not have any filter



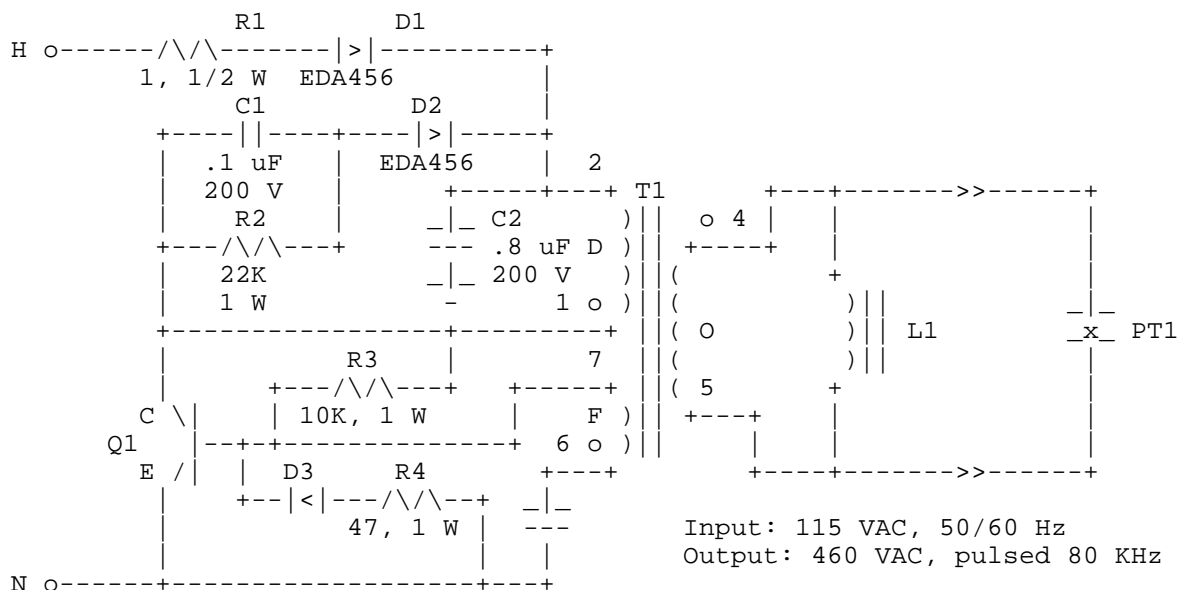
Question for the student: What happens if one or both Cs are replaced by resistors?

Chapter 14) Ultrasonic cleaner schematic

Ultrasonic cleaning is a means of removing dirt and surface contamination from intricate and/or delicate parts using powerful high frequency sound waves in a liquid (water/detergent/solvent) bath.

An ultrasonic cleaner contains a power oscillator driving a large piezoelectric transducer under the cleaning tank. Depending on capacity, these can be quite massive.

A typical circuit is shown below. This is from a Branson Model 41-4000 which is typical of a small consumer grade unit.



The power transistor (Q1) and its associated components form an self excited driver for the piezo-transducer (PT1). I do not have specs on Q1 but based on the circuit, it probably has a Vceo rating of at least 500 V and power rating of at least 50 W.

Two windings on the transformer (T1, which is wound on a toroidal ferrite core) provide drive (D) and feedback (F) respectively. L1 along with the inherent capacitance of PT1 tunes the output circuit for maximum amplitude.

The output of this (and similar units) are bursts of high frequency (10s to 100s of KHz) acoustic waves at a 60 Hz repetition rate. The characteristic sound these ultrasonic cleaners make during operation is due to the effects of the bursts occurring at 60 Hz since you cannot actually hear the ultrasonic frequencies they use.

The frequency of the ultrasound is approximately 80 KHz for this unit with a

maximum amplitude of about 460 VAC RMS (1,300 V p-p) for a 115 VAC input.

WARNING: Do not run the device with an empty tank since it expects to have a proper load. Do not touch the bottom of the tank and avoid putting your paws into the cleaning solution while the power is on. I don't know what, if any, long term effects there may be but it isn't worth taking chances. The effects definitely feel strange.

Where the device doesn't oscillate (it appears as dead as a door-nail), first check for obvious failures such as bad connections and cracked, scorched, or obliterated parts.

To get inside probably requires removing the bottom cover (after pulling the plug and disposing of the cleaning solution!).

CAUTION: Confirm that all large capacitors are discharged before touching anything inside!

The semiconductors (Q1, D1, D2, D3) can be tested for shorts with a multimeter (see the document: "[Basic Testing of Semiconductor Devices](#)").

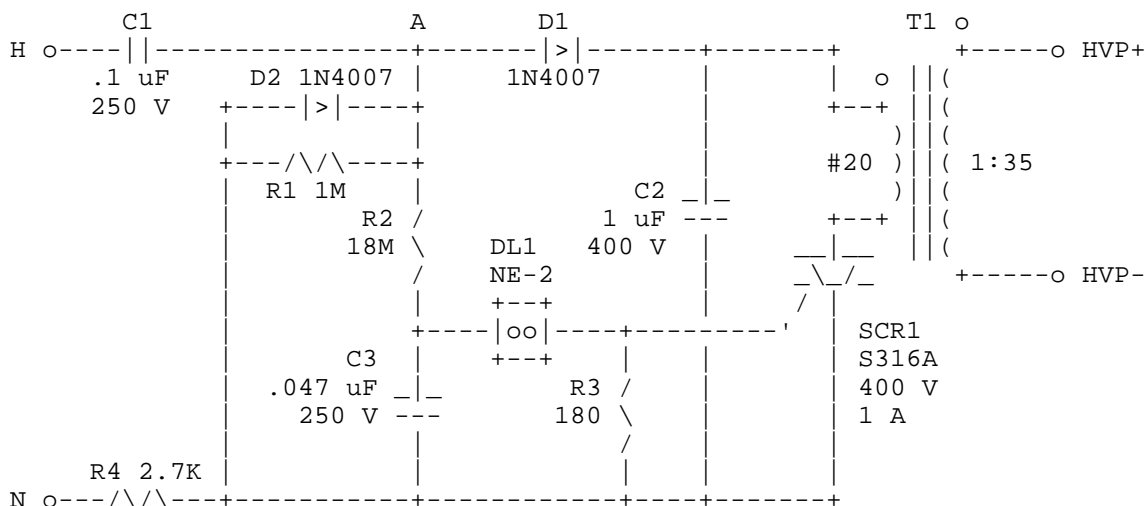
The transformer (T1) or inductor (L1) could have internal short circuits preventing proper operation and/or blowing other parts due to excessive load but this isn't kind of failure likely as you might think. However, where all the other parts test good but the cleaning action appears weak without any overheating, a L1 could be defective (open or other bad connections) detuning the output circuit.

Chapter 15) Range, oven, and furnace electronic ignition Schematic

Many modern gas stoves, ovens, furnaces, and other similar appliances use an electronic ignition rather than a continuously burning pilot flame to ignite the fuel. These are actually simple high voltage pulse generators.

- * Where starting is manual (there is a 'start' position on the control(s), a set of switch contacts on the control(s) provides power to the ignition module.
 - A problem of no spark with only one control indicates that the fault is with it or its wiring.
 - A problem with continuous sparking even with all the controls off or in their normal positions indicates a short - either due to a defective switch in one of the controls or contamination bypassing the switch contacts.
- * Where starting is automatic, an electronic sensor, thermocouple, or bimetal switch provides power to the ignition module as needed.

The Harper-Wyman Model 6520 Kool Lite(tm) module is typical of those found in Jenne-Aire and similar cook-tops. Input is 115 VAC, 4 mA, 50/60 Hz AC. C1 and D1 form a half wave doubler resulting in 60 Hz pulses with a peak of about 300 V and at point A and charges C2 to about 300 V through D2. R2, C3, and DL1 form a relaxation oscillator triggering SCR1 to dump the charge built up on C2 into T1 with a repetition rate of about 2 Hz.



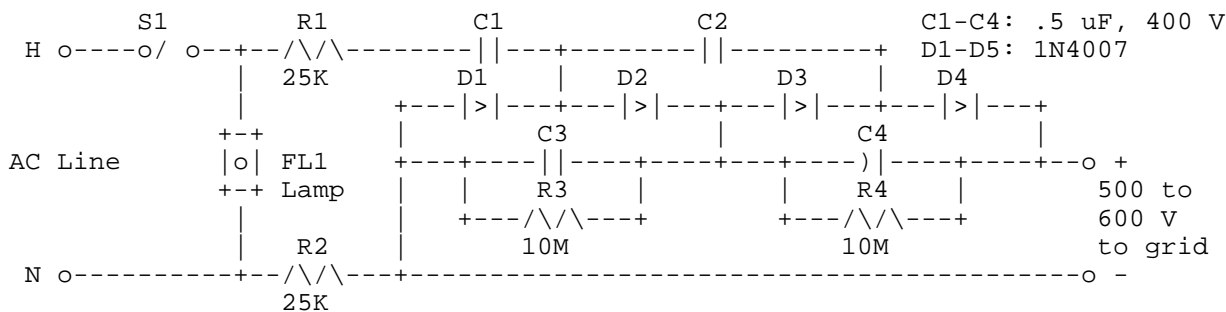
Chapter 16) Bug Zapper

You know the type - a purplish light with an occasional (or constant) Zap! Zap! Zap! If you listen real closely, you may be able to hear the screams of the unfortunate insects as well :-).

The high-tech versions consist of a high voltage low current power supply and fluorescent (usually) lamp selected to attract undesirable flying creatures. (Boring low-tech devices may just use a fan to direct the insects to a tray of water from which they are too stupid to be able to escape!)

However, these devices are not selective and will obliterate friendly and useful bugs as well as unwanted pests.

Here is a typical circuit:

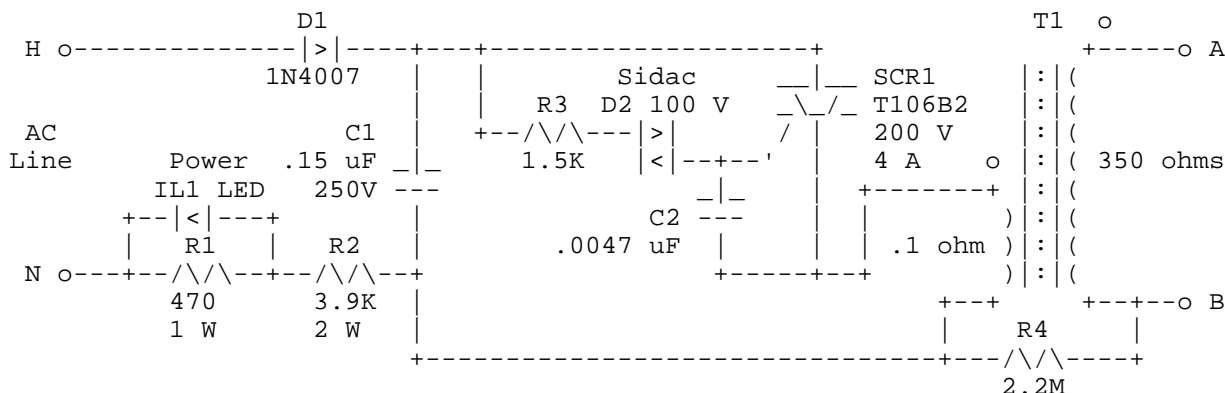


This is just a line powered voltage quadrupler. R1 and R2 provide current limiting when the strike occurs (and should someone come in contact with the grid). The lamp, FL1, includes the fluorescent bulb, ballast, and starter (if required). Devices designed for jumbo size bugs (or small rodents) may use slightly larger capacitors!

Chapter 17) Electronic Air Cleaner HV Generator

At least I assume this cute little circuit board is for an electronic air cleaner or something similar (dust precipitator, positive/negative ion generator, etc.)! I received the unit (no markings) by mistake in the mail. However, I did check to make sure it wasn't a bomb before applying power. :-)

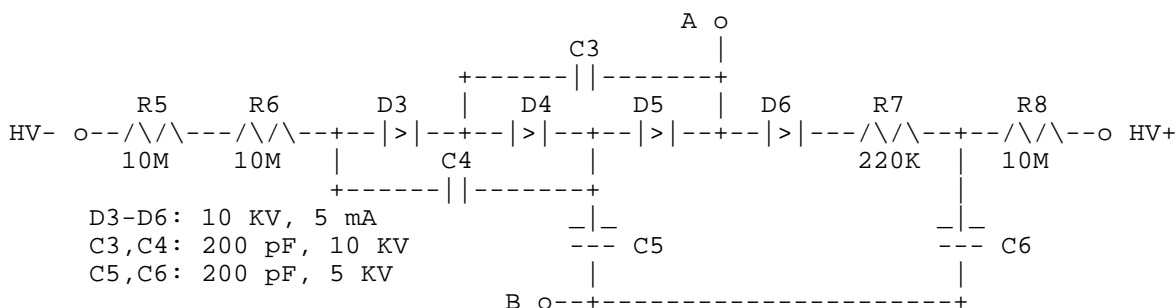
This module produces both positive and negative outputs when connected to 115 VAC, 60 Hz line voltage. Each is about 5 KV at up to around 5 uA.



The AC input is rectified by D1 and as it builds up past the threshold of the sidac (D2, 100 V), SCR1 is triggered dumping a small energy storage capacitor (C1) through the primary of the HV transformer, T1. This generates a HV pulse in the secondary. In about .5 ms, the current drops low enough such that the SCR turns off. As long as the instantaneous input voltage remains above about 100 V, this sequence of events repeats producing a burst of 5 or 6 discharges per cycle of the 60 Hz AC input separated by approximately 13 ms of dead time.

The LED (IL1) is a power-on indicator. :-)

The transformer was totally potted so I could not easily determine anything about its construction other than its winding resistances and turns ratio (about 1:100).



The secondary side consists of a voltage tripler for the negative output (HV-) and a simple rectifier for the positive output (HV+). This asymmetry is due to the nature of the unidirectional drive to the transformer primary.

From my measurements, this circuit produces a total of around 10 KV between HV+ and HV-, at up to 5 uA. The output voltages are roughly equal plus and minus when referenced to point B.

I assume the module would also operate on DC (say, 110 to 150 V) with the discharges repeating continuously at about 2 KHz. Output current capability would be about 5 times greater but at the same maximum (no load) voltage. (However, with DC, if the SCR ever got stuck in an 'on' state, it would be stuck there since there would be no AC zero crossings to force it off. This wouldn't be good!)

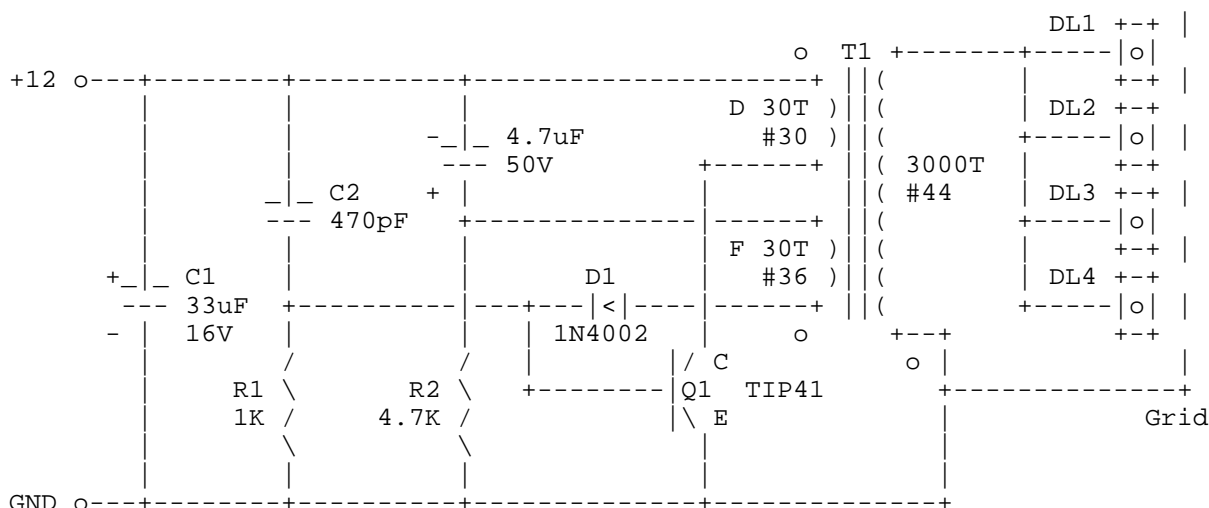
The secondary side circuitry can be easily modified or redesigned to provide a single positive or negative output or for higher or lower total voltage. Simply removing R4 will isolate it from the input and earth ground (assuming T1's insulation is adequate).

Where there is no high voltage from such a device, check the following:

- * Make sure power is actually getting to the high voltage portion of the unit. Test the wall socket and/or AC adapter or other power supply for proper voltage with a multimeter.
- * Excessive dirt/dust/muck/moisture or physical damage or a misplaced paper clip may be shorting it out or resulting in arcing or corona (a strong aroma of ozone would be an indication of this). With such a small available current (only uA) it doesn't take much for contamination to be a problem. Thoroughly clean and dry the unit and check for shorts (with a multimeter between the HV electrodes and case) and then test it again. Your problems may be gone!
- * If this doesn't help and the unit is not fully potted (in which case, replacement is the only option), check for shorted or open components, especially the power semiconductors.

Chapter 18) Auto Air Purifier HV Generator

Well, maybe :-). This thing is about the size of a hot-dog and plugs into the cigarette lighter socket. It produces a bit of ozone and who knows what else. Whether there is any effect on air quality (beneficial or otherwise) or any other effects is questionable but it does contain a nice little high voltage circuit.



T1 is constructed on a 1/4" diameter ferrite core. The D (Drive) and F

(Feedback) windings are wound bifilar style (interleaved) directly on the core. The O (Output) winding is wound on a nylon sleeve which slips over the core and is split into 10 sections with an equal number of turns (100 each) with insulation in between them.

DL1 to DL4 look like neon light bulbs with a single electrode. They glow like neon light bulbs when the circuit is powered and seem to capacitively couple the HV pulses to the grounded grid in such a way to generate ozone. I don't know if they are filled with special gas or are just weird neon light bulbs.

Chapter 19) Typical Rechargeable Flashlight Schematics

Here are circuit diagrams from several inexpensive rechargeable flashlights. These all use very 'low-tech' chargers so battery life may not be as long as possible and energy is used at all times when plugged into an AC outlet.

19.1) First Alert Series 50 rechargeable flashlight schematic

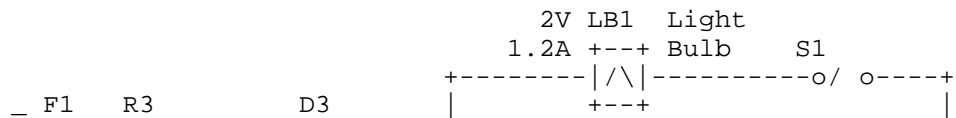
This one is typical of combined all-in-one units using a lead-acid battery that extends a pair of prongs to directly plug into the wall socket for charging.

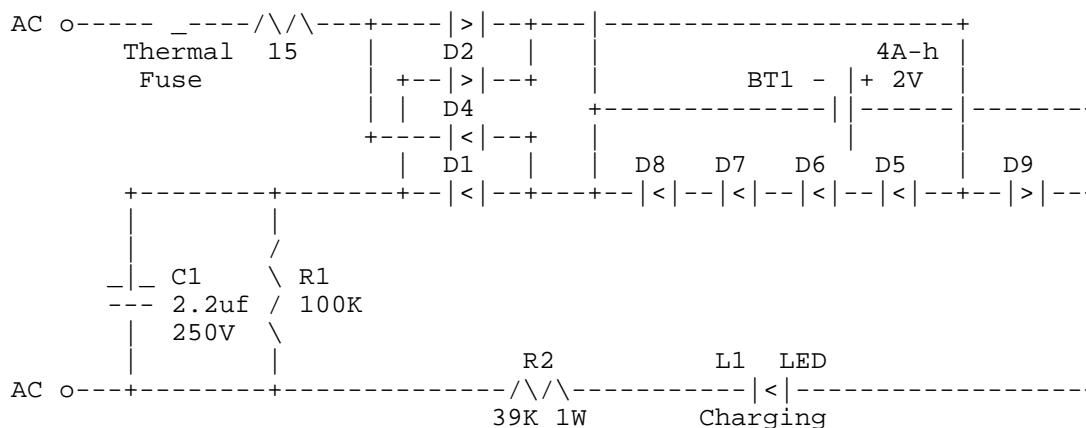
It is a really simple, basic charger. However, after first tracing out the circuit, I figured only the engineers at First Alert knew what all the diodes were for - or maybe not :-). But after some reflection and rearrangement of diodes, it all makes much more sense: C1 limits the current from the AC line to the bridge rectifier formed by D1 to D4. The diode string, D5 to D8 (in conjunction with D9) form a poor-man's zener to limit voltage across BT1 to just over 2 V.

The Series 50 uses a sealed lead-acid battery that looks like a multi-cell pack but probably is just a funny shaped single cell since its terminal voltage is only 2 V.

Another model from First Alert, the Series 15 uses a very similar charging circuit with a Gates Cyclon sealed lead-acid single cell battery, 2 V, 2.5 A-h, about the size of a normal Alkaline D-cell.

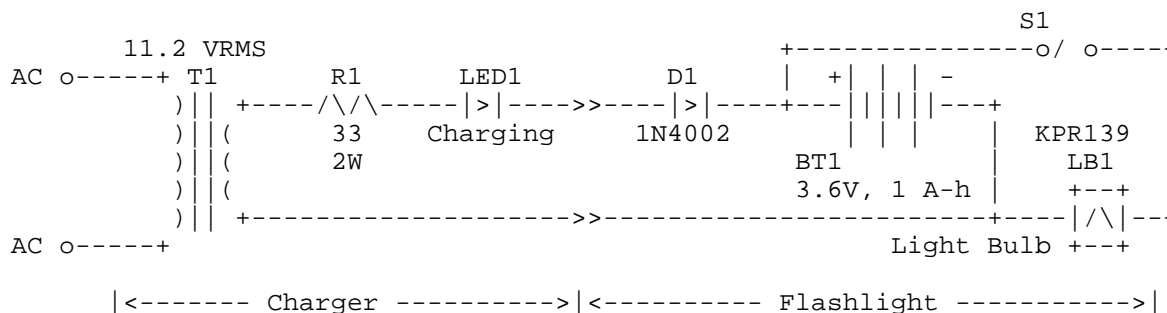
WARNING: Like many of these inexpensive rechargeable devices with built-in charging circuitry, there is NO line isolation. Therefore, all current carrying parts of the circuit must be insulated from the user - don't go opening up the case while it is plugged in!





19.2) Black & Decker Spotlighter Type 2 rechargeable flashlight

This uses a 3 cell (3.6 V) NiCd pack (about 1 A-h). The charging circuit is about as simple as it gets!



I could not open the transformer without dynamite but I made measurements of open circuit voltage and short circuit current to determine the value of R1. I assume that R1 is actually at least in part the effective series resistance of the transformer itself.

Similar circuits are found in all sorts of inexpensive rechargeable devices. These have no brains so they trickle charge continuously. Aside from wasting energy, this may not be good for the longevity of some types of batteries (but that is another can of worms).

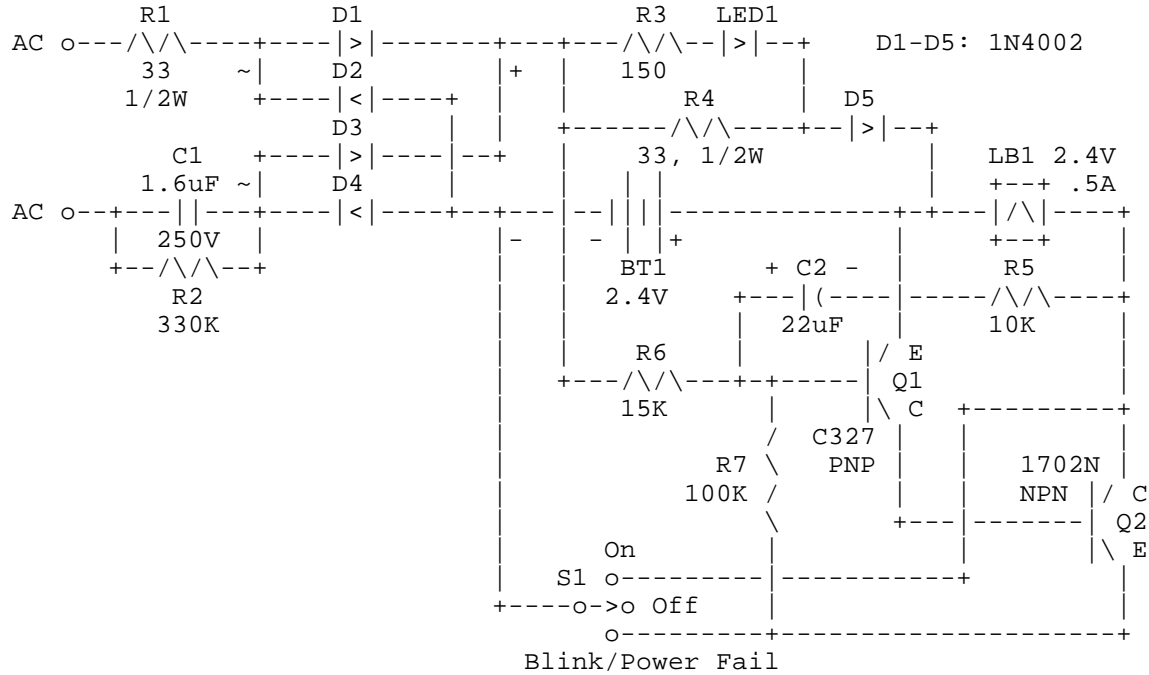
19.3) Brand Unknown (Made in China) rechargeable flashlight schematic

This is another flashlight that uses NiCd batteries. The charger is very simple - a series capacitor to limit current followed by a bridge rectifier.

There is an added wrinkle which provides a blinking light option in addition

to the usual steady beam. This will also activate automatically should there be a power failure while the unit is charging if the switch is in the 'blink' position.

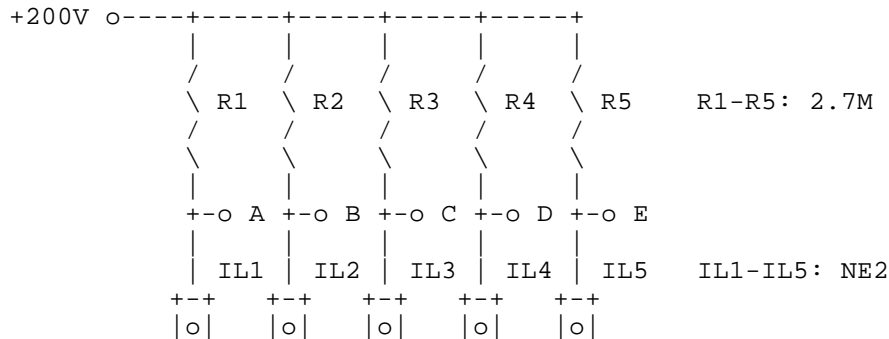
With Sa in the blink position, a simple transistor oscillator pulses the light with the blink rate of about 1 Hz determined by C2 and R5. Current through R6 keeps the light off if the unit is plugged into a live outlet. (Q1 and Q2 are equivalent to ECG159 and ECG123AP respectively.)

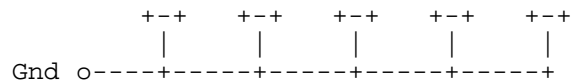


Chapter 20) Interesting Sequential Neon Flasher

This is a sort of brain teaser since it certainly isn't intuitively obvious how this circuit works (if it works at all). It may be instructive to start with the degenerate case of 2 resistors, 2 neon lamps, and a single capacitor. What happens with that configuration?

(From: Steve Roberts (osteven@akrobiz.com)).





Connect a .22 uF, 200 V capacitor between each of the following pairs of points: A to C, A to D, B to D, B to E, C to E.

Neons will flash in sequence ABCDE if fed off DC. Momentarily removing the DC will cause them to flash EDCBA.

From an ancient Radio Shack "Pbox" kit - the first kit I ever built!

Written by Samuel M. Goldwasser. [\[Feedback Form\]](#) | [\[mailto\]](#). The most recent version is available on the WWW server <http://www.repairfaq.org/> [\[Copyright\]](#) [\[Disclaimer\]](#)