

## Up-down ramp quickens servo system response

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Servo systems often require a ramp waveform to control both the acceleration and deceleration rates of heavy loads, but all too often system complexity and reaction time are increased because only a positive-going, fixed-slope ramp is available for performing the dual function. Using a dual-polarity ramp generator that allows individual selection of both the up- and down-ramp rates, such as that shown in the figure, ensures optimum servo system response at low cost.

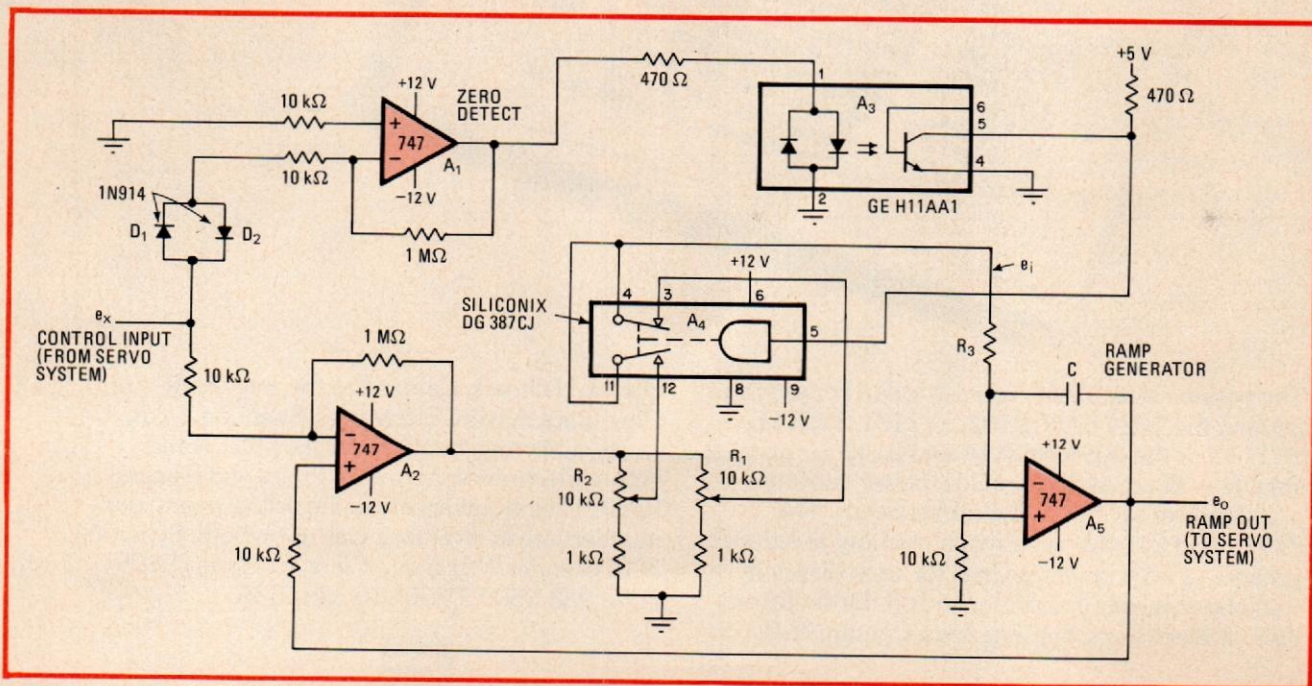
Command-input voltage derived from the servo system's joy-stick (control) position is applied to operational amplifiers  $A_1$  and  $A_2$ , as shown. Diodes  $D_1$  and  $D_2$  provide a 0.7-volt drop of the input signal before it is introduced to  $A_1$ .

When the control-input voltage is above or below zero by more than 0.7 v, the system load must be accelerated

to a position corresponding to that control voltage.  $A_1$  detects that the input voltage is other than zero and switches phototransistor  $A_3$  on, which in turn switches  $A_4$ . Meanwhile,  $A_2$  will switch from a positive voltage to  $-12$  v if the control voltage is equal to or greater than the ramp's output voltage.  $A_3$  provides a high-impedance input for  $A_1$  and an output signal suitable for driving transistor-transistor or similar logic.  $A_4$  is a solid-state, single-pole, double-throw relay that initiates an up-ramp waveform whose slope is partially controlled by the value of  $R_1$ .

The positive-going ramp emanating from  $A_5$  will move the system load toward its desired position, and as that occurs, the servo system's feedback voltage will act to reduce the control-input voltage. When the input voltage moves within 0.7 v of ground,  $A_1$  moves low and  $A_3$  turns off.  $A_4$  now initiates a down-ramp waveform to decelerate the system to a stop at a rate determined partially by  $R_2$ .

The ramp generator,  $A_5$ , is an op-amp integrator that produces waveforms whose rate is proportional to the input voltage,  $e_i$ . This voltage, in turn, is set by  $R_1$  or  $R_2$ . The time-dependent voltage output from the ramp generator is approximately equal to the voltage across  $C$ .  $C$  is charged by a steady current  $I = e_i/R_3$ , so that:



**Placement.** Up-down ramp generator with selectable-slope capability can efficiently position heavy servo-system loads. Key to operation is solid-state relay  $A_4$ , which switches from up ramp to down ramp to decelerate load when it zeros in on terminating position.

$$e_o = e_i t/R_3C \quad (1)$$

because  $e_o = e_c = It/C$ .

Equation 1 is useful for setting the values of  $R_3$  and  $C$  needed for a given ramp slope. For example, assume that the maximum positive-going or negative-going ramp rate must be 20 v/second and that  $e_i$  is 12 v maximum. Then,  $1 \cdot 20 = 12/R_3C$  and therefore  $R_3C = 0.6$ .

Assuming a nominal value of 0.33 microfarad for  $C$ ,  $R_3$  is then equal to 1.81 megohms.

Using the component values shown in the circuit allows a linear ramp to be generated over a 10:1 frequency range. Note that once the component values for the maximum ramp rate are determined, the actual ramp rate may be selected by setting  $R_1$  and  $R_2$  for the corresponding value of  $e_i$ .  $\square$