## Dual transistor improves current-sense circuit

Robert Zawislak, PE, Consultant, Palatine, IL



In multiple-output power supplies in which a single supply

powers circuitry of vastly different current draws, two perplexing steps are

sensing the current that each output draws and deactivating the power supply in the event of an overload on that output. These issues are especially important in protecting the fragile PCB (printed-circuit-board) traces in low-level circuits. A typical circuit would use the base-emitter threshold volt-

## designideas

age of approximately 0.6V of a bipolar transistor to trigger the power-supplyprotection circuits. Although economical, the transistor's threshold varies excessively over temperature; hence, the protection level is unstable.

The circuit in Figure 1 essentially eliminates the base-emitter-voltage temperature-variation problem as the derivation of the output voltage and as a function of the load current. By using dual bipolar devices in one case, the manufacturer nearly perfectly matches the two devices. Although this Design Idea describes a positive power supply, you can realize a similar negative-output-supply current-sense circuit using a dual NPN transistor in place of the

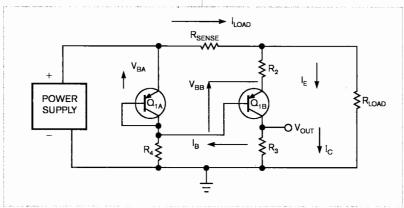


Figure 1 This simple two-transistor circuit provides a voltage output proportional to the current through sense resistor R<sub>SENSE</sub>.

dual PNP that the figure shows.

The following equations show the derivation of the output voltage as a function of the load current (referring to Figure 1):

$$\begin{split} &V_{BA} + (I_{LOAD} \times R_{SENSE}) + (I_{E} \times R_{2}) - V_{BB} = 0. \\ &[(V_{BA} - V_{BB}) + (I_{LOAD} \times R_{SENSE})] - I_{E}R_{2} = 0. \\ &I_{C} + I_{B} = I_{E}. \\ &(V_{BA} - V_{BB}) + (I_{LOAD} \times R_{SENSE}) - (I_{C} + I_{B})R_{2} = 0. \\ &I_{B} = I_{C}/\beta. \\ &V_{BA} - V_{BB} + I_{LOAD} \times R_{SENSE} - (I_{C} + I_{C}/\beta)R_{2} = 0. \\ &V_{BA} - V_{BB} + I_{LOAD} \times R_{SENSE} - (I_{C} + I_{C}/\beta)R_{2} = 0. \\ &V_{DUT} = I_{C}R_{3}. \\ &I_{C} = V_{OUT}/R_{3}. \\ &V_{BA} - V_{BB} + I_{LOAD} \times R_{SENSE} - (V_{OUT}/R_{3})(\beta + 1/\beta)R_{2} = 0. \\ &V_{DUT} = I_{C}R_{3}. \\ &I_{C} = V_{OUT}/R_{3}. \\ &V_{BA} - V_{BB} + I_{LOAD} \times R_{SENSE} - (V_{OUT}/R_{3})(\beta + 1/\beta)R_{2} = 0. \\ &If V_{BA} = V_{BB}, then V_{BA} - V_{BB} = 0, and \\ &I_{LOAD} \times R_{SENSE} - (V_{OUT}/R_{3})(\beta + 1/\beta)R_{2} = 0. \\ &V_{OUT} = I_{LOAD} \times R_{SENSE}[R_{3}/(\beta + 1)](\beta/R_{2}). \\ &If \beta \text{ is high, then } \beta/(\beta + 1)\beta) \approx 1, and \\ &V_{OUT} = (I_{LOAD} \times R_{SENSE} \times R_{3})/R_{2}. \text{EDN} \end{split}$$