Shunt regulator serves as inexpensive op amp in power supplies

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Developed as a three-terminal shunt regulator, the popular and multiple-sourced TL431 IC offers designers many intriguing possibilities beyond its intended application. Internally, the TL431 comprises a precision voltage reference, an operational amplifier, and a shunt transistor (**Figure 1a**). In a typical voltage-regulator application, adding two external resistors, R_A and R_B , sets the shunt-regulated output voltage at the lower end of load resistor R_s (**Figure 1b**).

In today's power-supply market, cost reduction drives most designs, as evidenced by Asian manufacturers that have resorted to shaving pennies off their power-supply products by using single-sided pc boards. This Design Idea shows how a three-terminal shunt regulator can replace a more expensive conventional operational amplifier in a power-converter design.

A switched-mode power supply uses a galvanically isolated feedback portion of a PWM circuit (Figure 2). In designs that omit a voltage amplifier, a shunt regulator can serve as an inexpensive op amp. Resistors R_1 and R set the power supply's dc output voltage, and optocoupler IC, provides galvanic isolation. Resistor R_1 provides bias for the optocoupler and the TL431, IC₁. Resistor R_3 and zener diode D_1 establish a fixed bias voltage to ensure that bias resistor R1 does not form a feedback path. Resistors R₁ and R₂ control the gain across the optocoupler. In most designs, the ratio of R_2 to R_1 is roughly 10-to-1.

Components C_p , C_z , and R_z provide frequency compensation for the control loop. The optocoupler includes a highfrequency pole, f_p , in its frequency response, an item that most optocouplers' data sheets omit. You can use a network analyzer to determine the location of the high-frequency pole or estimate that the pole occurs at approximately 10 kHz. The following **equation** describes the compensation network's small-signal transfer function:

$$\begin{split} \mathbf{G}_{\mathbf{C}}(\mathbf{s}) &= \frac{\Delta V_{\text{ERR}}}{\Delta V_{\text{OUT}}} = \\ & \frac{(\mathbf{s} \times \mathbf{R}_{Z} \times \mathbf{C}_{Z} + \mathbf{l})}{(\mathbf{s} \times \mathbf{R}_{I} (\mathbf{C}_{Z} + \mathbf{C}_{P}) \left(\frac{\mathbf{s} \times \mathbf{R}_{Z} \times \mathbf{C}_{P} \times \mathbf{C}_{Z}}{\mathbf{C}_{P} + \mathbf{C}_{Z}} + 1\right)} \times \\ & \frac{\mathbf{R}_{2}}{\mathbf{R}_{1}} \times \left(\frac{1}{\left(\frac{\mathbf{s}}{2 \times \pi \times \mathbf{f}_{P}} + 1\right)}\right). \end{split}$$

Note that, under some circumstances, adding a bypass capacitor across diode D_1 may be necessary for output-noise reduction.**EDN**





