## Dual-Frequency Oscillator Design

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Oscillators capable of oscillating at two different frequencies simultaneously provide outputs that are a linear addition of two sine waves. Frequency ratios of $20: 1$ have been obtained, and the two output frequencies need not be harmonically related.

## Theory

Qualitative operation of the oscillators is relatively simple to understand, but quantitatively they are quite difficult. Synthesis of the circuit is much simpler than analysis.
The generalized dual-frequency oscillator configuration is shown in Fig. 1A. Neglecting effects of the active element, oscillator frequency is $Z_{1}+Z_{2}+Z_{3}=0$. The circuits in Fig. 1B and 1C are simultaneous dual-frequency oscillators.

The circuit shown in Fig. 2A is a conventional Hartley oscillator and that in Fig. 2B is a Colpitts oscillator. If capacitors and inductors were interchanged, the Hartley oscillator would become a Colpitts oscillator and the Colpitts oscillator would become a Hartley oscillator. Two networks capable of appearing capacitive at one fre-

$P=P L A T E, C=$ COLLECTOR G=GRID, B= 8ASE $K=$ CATHODE,$E=$ EMITTER (A)

(B)

(C)

FIG. 1-Generolized dual-frequency oscillator is shown of (A). Lower of two frequencies is produced by Hortley oscillator of (B) and by Colpitts oscillotor of (C)
quency and inductive at another are shown in Fig. 3.

## Design

Assume two properly designed single-frequency oscillators, a Hartley and a Colpitts. Angular velocity $\omega_{1}$ of the Hartley oscillator is less than angular velocity $\omega_{2}$ of the Colpitts oscillator. A network configuration is required that appears as a Hartley oscillator at $\omega_{1}$ and as a Colpitts oscillator at $\omega_{2}$. These conditions are satisfied in Fig. 1B.

At $\omega_{1}$, network $L_{A} C_{A}$ appears as

## Electrostatically Focused TWT



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FIG. 2-Hartley oscillator (A) and Colpitts (B)
$L_{1}$; and at $\omega_{2}$, it appears as $C_{2}$. Network $L_{B} C_{n}$ appears as $C_{1}$ at $\omega_{1}$ and $L_{3}$ at $\omega_{2}$. Network $L_{c} C_{c}$ appears as $L_{2}$ at $\omega_{1}$ and as $C_{3}$ at $\omega_{2}$.

The equations for circuit values are:
$\left(-1 / \omega_{1} L_{A}\right)+\omega_{1} C_{A}=-1 / \omega_{1} L_{1}$ and $\left(-1 / \omega_{2} L_{4}\right)+\omega_{2} C_{4}=\omega_{2} C_{2} ;$ $\omega_{1} L_{B}-\left(1 / \omega_{1} C_{B}\right)=-1 / \omega_{1} C_{1}$ and $\omega_{2} L_{B}-\left(1 / \omega_{2} C_{B}\right)=\omega_{2} L_{3} ;$
$\left(-1 / \omega_{1} L_{c}\right)+\omega_{1} C_{C}=-1 / \omega_{1} L_{2}$ and $\left(-1 / \omega_{2} L_{C}\right)+\omega_{2} L_{C}=\omega_{2} C_{3}$.
The dual-frequency oscillator in Fig. 1C is for $\omega_{1}$ greater than $\omega_{\%}$. The equations are:

$$
\begin{aligned}
& \omega_{1} L_{D}-\left(1 / \omega_{1} C_{D}\right)=\omega_{1} L_{1} \text { and } \\
& \omega_{2} L_{D}-\left(1 / \omega_{2} C_{D}\right)=-1 / \omega_{2} C_{2} ; \\
& \left(-1 / \omega_{1} L_{E}\right)+\omega_{1} C_{E}=\omega_{1} C_{1} \text { and } \\
& \left(-1 / \omega_{2} L_{B}\right)+\omega_{2} C_{E}=-1 / \omega_{2} L_{n} ; \\
& \omega_{1} L_{F}-\left(1 / \omega_{1} C_{F}\right)=\omega_{1} L_{2} \text { and } \\
& \omega_{2} L_{F}-\left(1 / \omega_{2} C_{F}\right)=-1 / \omega_{2} C_{3} .
\end{aligned}
$$

The number of frequencies at which an oscillator can oscillate


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simultaneously is not limited to two. Three single-frequency oscillators could also be combined to form a triple-frequency oscillator. It would combine a Hartley oscillator at $\omega_{1}$, a Colpitts at $\omega_{2}$ and a Hartley at $\omega_{3}$. Three-element networks would appear as $C_{11}$ at $\omega_{1}$,



FIG. 3-Networks appear capacitive at one frequency and inductive at the other
$L_{11}$ at $\omega_{2}$ and $C_{m}$ at $\omega_{3}$; or $L_{m}$ at $\omega_{1}, C_{\mathrm{z}}$ at $\omega_{2}$ and $L_{\mathrm{s}}$ at $\omega_{3}$.

In the dual-frequency oscillator, adjustment or control of either of its operating frequency is difficult because the value of each component in the circuit is a function of the two frequencies.

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