LM628 Programming Guide

National Semiconductor
Application Note 693
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INTRODUCTION

The LM628/LM629 are dedicated motion control processors. Both devices control DC and brushless DC servo motors, as well as, other servomechanisms that provide a quadrature incremental feedback signal. Block diagrams of typical LM628/LM629-based motor control systems are shown in *Figures 1* and *2*.

As indicated in the figures, the LM628/LM629 are bus peripherals; both devices must be programmed by a host processor. This application note is intended to present a concrete starting point for programmers of these precision motion controllers. It focuses on the development of short programs that test overall system functionality and lay the groundwork for more complex programs. It also presents a method for tuning the loop-compensation PID filter.†

REFERENCE SYSTEM

Figure 18 is a detailed schematic of a closed-loop motor control system. All programs presented in this paper were developed using this system. For application of the programs in other LM628-based systems, changes in basic programming structure are not required, but modification of filter coefficients and trajectory parameters may be required.

I. PROGRAM MODULES

Breaking programs for the LM628 into sets of functional blocks simplifies the programming process; each block executes a specific task. This section contains examples of the principal building blocks (modules) of programs for the LM628.

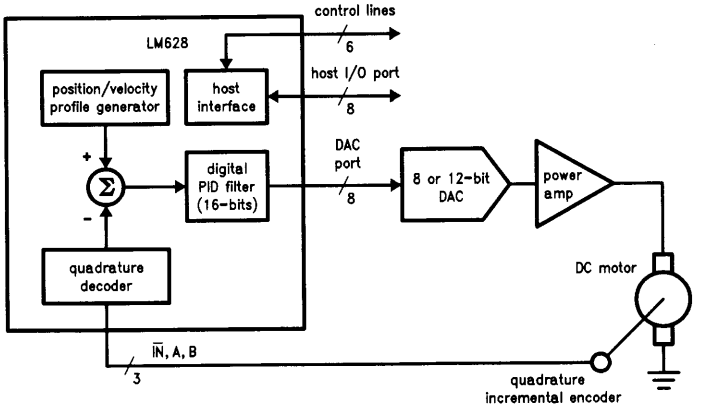


FIGURE 1. LM628-Based Motor Control System

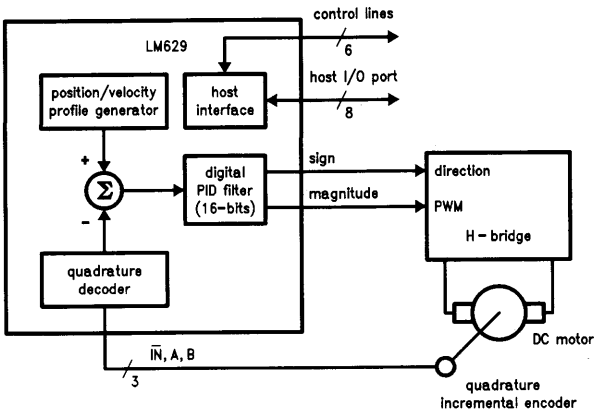


FIGURE 2. LM629-Based Motor Control System

†**Note:** For the remainder of this paper, all statements about the LM628 also apply to the LM629 unless otherwise noted.

BUSY-BIT CHECK MODULE

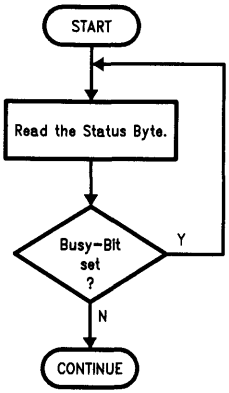
The first module required for successful programming of the LM628 is a busy-bit check module.

The busy-bit, bit zero of the status byte, is set immediately after the host writes a command byte, or reads or writes the second byte of a data word. See *Table I*. While the busy-bit is set, the LM628 will ignore any commands or attempts to transfer data.

A busy-bit check module that polls the Status Byte and waits until the busy-bit is reset will ensure successful host/LM628 communications. ***It must be inserted after a command write, or a read or write of the second byte of a data word.*** *Flow diagram 1* represents such a busy-bit check module. This module will be used throughout subsequent modules and programs.

Reading the Status Byte is accomplished by executing a RDSTAT command. RDSTAT is directly supported by LM628 hardware and is executed by pulling $\overline{CS}$, $\overline{PS}$, and $\overline{RD}$ logic low.

Flow Diagram 1. Busy-bit Check Module



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INITIALIZATION MODULE

In general, an initialization module contains a reset command and other initialization, interrupt control, and data reporting commands.

The example initialization module, detailed in *Figure 3*, contains a hardware reset block and a PORT 12 command.

Hardware Reset Block

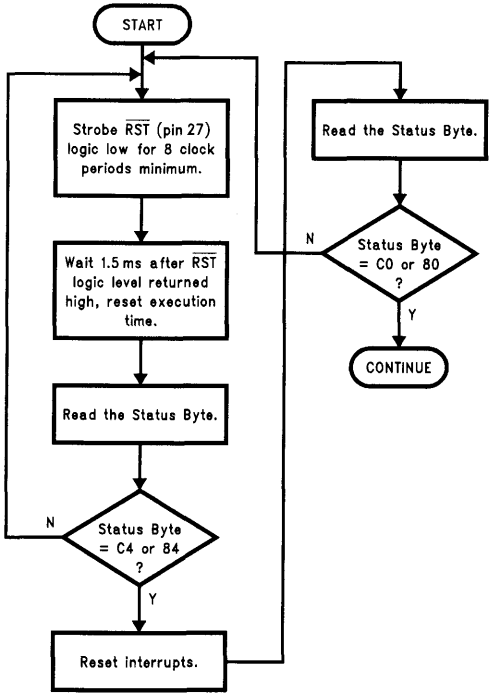
Immediately following power-up, a hardware reset ***must be*** executed. Hardware reset is initiated by strobing $\overline{RST}$ (pin 27) logic low for ***a minimum of eight LM628 clock periods.*** The reset routine begins after $\overline{RST}$ is returned to logic high. During the reset execution time, **1.5 ms** maximum, the LM628 will ignore any commands or attempts to transfer data.

A hardware reset forces the LM628 into the state described in what follows.

1. The derivative sampling coefficient, d_S, is set to one, and all other filter coefficients and filter coefficient input buffers are set to zero. With d_S set to one, the derivative sampling interval is set to $2048/f_{CLK}$.
2. All trajectory parameters and trajectory parameters input buffers are set to zero.
3. The current absolute position of the shaft is set to zero ("home").
4. The breakpoint interrupt is masked (disabled), and the remaining five interrupts are unmasked (enabled).
5. The position error threshold is set to its maximum value, 7FFF hex.
6. The DAC output port is set for an 8-bit DAC interface.

Flow diagram 2 illustrates a hardware reset block that includes an LM628 functionality test. This test *should be* completed immediately following all hardware resets.

Flow Diagram 2. Hardware Reset Block



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Reset Interrupts

An RSTI command sequence allows the user to reset the interrupt flag bits, bits one through six of the status byte. See *Table I*. It contains an RSTI command and one data word.

The RSTI command initiates resetting the interrupt flag bits. Command RSTI also resets the host interrupt output pin (pin 17).

Port	Bytes	Command	Comments
	(Note 4)	hardware reset	Strobe $\overline{RST}$, pin 27, logic low for eight clock periods minimum.
		wait	The maximum time to complete hardware reset tasks is 1.5 ms. During this reset execution time, the LM628 will ignore any commands or attempts to transfer data.
c (Note 1)	xx (Note 2)	RDSTAT	This command reads the status byte. It is directly supported by LM628 hardware and can be executed at any time by pulling $\overline{CS}$, $\overline{PS}$, and $\overline{RD}$ logic low. Status information remains valid as long as $\overline{RD}$ is logic low.
		decision	If the status byte is C4 hex or 84 hex, continue. Otherwise loop back to hardware reset.
c	1D	RSTI	This command resets *only* the interrupts indicated by zeros in bits one through six of the next data word. It also resets bit fifteen of the Signals Register and the host interrupt output pin (pin 17).
		Busy-bit Check Module	
d	xx	HB (Note 3)	don't care
d	00	LB	Zeros in bits one through six indicate *all* interrupts will be reset.
		Busy-bit Check Module	
c	xx	RDSTAT	This command reads the status byte.
		decision	If the status byte is C0 hex or 80 hex, continue. Otherwise loop back to hardware reset.
c	06	PORT12	The reset default size of the DAC port is eight bits. This command initializes the DAC port for a 12-bit DAC. It should not be issued in systems with an 8-bit DAC.
		Busy-bit Check Module	

FIGURE 3. Initialization Module (with Hardware Reset)

Note 1: The 8-bit host I/O port is a dual-mode port; it operates in command or data mode. The logic level at $\overline{PS}$ (pin 16) selects the mode. Port c represents the LM628 command port-commands are written to the command port and the Status Byte is read from the command port. A logic level of "0" at $\overline{PS}$ selects the command port. Port d represents the LM628 data port—data is both written to and read from the data port. A logic level of "1" at $\overline{PS}$ selects the data port.

Note 2: x - don't care

Note 3: HB - high byte, LB - low byte

Note 4: All values represented in hex.

Immediately following the RSTI command, a single data word is written. The first byte is not used. Logical zeros in bits one through six of the second byte reset the corresponding interrupts. See *Table II*. Any combination of the interrupt flag bits can be reset within a single RSTI command sequence. This feature allows interrupts to be serviced according to a user-programmed priority.

In the case of the example module, the second byte of the RSTI data word, 00 hex, resets *all* interrupt flag bits. See *Figure 3*.

TABLE I. Status Byte Bit Allocation

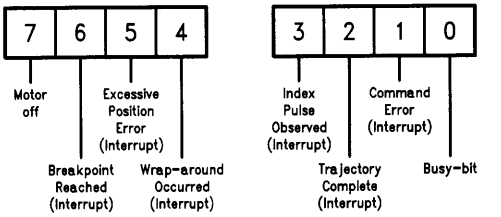

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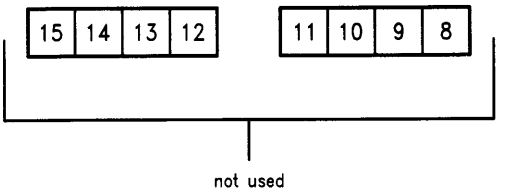
TABLE II. Interrupt Mask/Reset Bit Allocations

high byte



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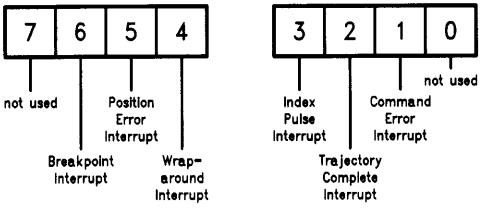
low byte



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DAC Port Size

During both hardware and software resets, the DAC output port defaults to 8-bit mode. If an LM628 control loop utilizes a 12-bit DAC, command PORT12 should be issued immediately following the hardware reset block and all subsequent resets. Failure to issue command PORT12 will result in erratic, unpredictable motor behavior.

If the control loop utilizes an 8-bit DAC, command PORT12 must not be executed; this too will result in erratic, unpredictable motor behavior.

An LM629 will ignore command PORT8 (as it provides an 8-bit sign/magnitude PWM output). Command PORT12 *should not* be issued in LM629-based systems.

Software Reset Considerations

After the initial hardware reset, resets can be accomplished with either a hardware reset or command RESET (software reset). Software and hardware resets execute the same tasks† and require the same execution time, 1.5 ms maximum. During software reset execution, the LM628 will ignore any commands or attempts to transfer data.

The hardware reset module includes an LM628 functionality test. This test is ***not*** required after a software reset.

Figure 4 details an initialization module that uses a software reset.

†In the case of a software reset, the position error threshold remains at its pre-reset value.

Port	Bytes	Command	Comments
c	00	RESET	See Initialization Module text.
		wait	The maximum time to complete RESET tasks is 1.5 ms.
c	06	PORT12	The RESET default size of the DAC port is eight bits. This command initializes the DAC port for a 12-bit DAC. It should not be issued in a system with an 8-bit DAC.
		Busy-bit Check Module	
c	1D	RSTI	This command resets *only* the interrupts indicated by zeros in bits one through six of the next data word. It also resets bit fifteen of the Signals Register and (pin 17) the host interrupt output pin.
		Busy-bit Check Module	
d	xx	HB	Don't care
d	00	LB	Zeros in bits one through six indicate *all* interrupts will be reset.
		Busy-bit Check Module	

FIGURE 4. Initialization Module (with Software Reset)

Comments

Figure 5 illustrates, in simplified block diagram form, the LM628. The profile generator provides the control loop input, desired shaft position. The quadrature decoder provides the control loop feedback signal, actual shaft position. At the first summing junction, actual position is subtracted from desired position to generate the control loop error signal, position error. This error signal is filtered by the PID filter to provide the motor drive signal.

After executing the example initialization module, the following observations are made. With the integration limit term (i_L) and the filter gain coefficients (k_p, k_i, and k_d) initialized to zero, the filter gain is zero. Moreover, after a reset, desired shaft position tracks actual shaft position. Under these conditions, the motor drive signal is zero. The control system can not affect shaft position. The shaft should be stationary and "free wheeling". If there is significant drive amplifier offset, the shaft may rotate slowly, but with minimal torque capability.

Note: Regardless of the free wheeling state of the shaft, the LM628 continuously tracks shaft absolute position.

FILTER PROGRAMMING MODULE

The example filter programming module is shown in *Figure 6*.

Load Filter Parameters (Coefficients)

An LFIL (Load FILter) command sequence includes command LFIL, a filter control word, and a variable number of data words.

The LFIL command initiates loading filter coefficients into input buffers.

The two data bytes, written immediately after LFIL, comprise the filter control word. The first byte programs the derivative sampling coefficient, d_s (i.e. selects the derivative sampling interval). The second byte indicates, with logical ones in respective bit positions, which of the remaining four filter coefficients will be loaded. See *Tables III* and *IV*. Any combination of the four coefficients can be loaded within a single LFIL command sequence.

Immediately following the filter control word, the filter coefficients are written. Each coefficient is written as a pair of data bytes, a data word. Because any combination of the four coefficients can be loaded within a single LFIL command sequence, the number of data words following the filter control word can vary in the range from zero to four.

In the case of the example module, the first byte of the filter control word, 00 hex, programs a derivative sampling coefficient of one. The second byte, x8 hex, indicates only the proportional gain coefficient will be loaded.

Immediately following the filter control word, the proportional gain coefficent is written. In this example, k_p is set to ten with the data word 000A hex. The other three filter coefficients remain at zero, their reset value.

Update Filter

The update filter command, UDF, transfers new filter coefficients from input buffers to working registers. Until UDF is executed, the new filter coefficients do not affect the transfer characteristic of the filter.

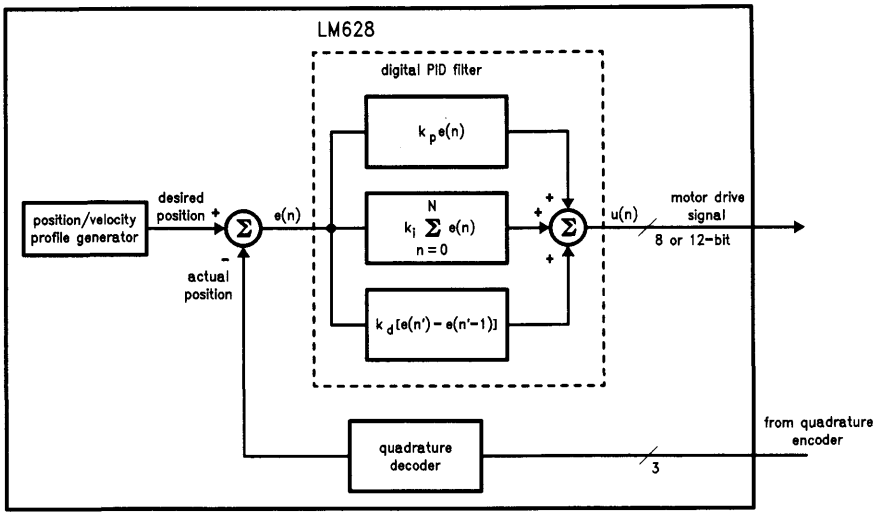

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FIGURE 5. LM628—Simplified Block Diagram Form

TABLE III. Filter Control Word Bit Allocation

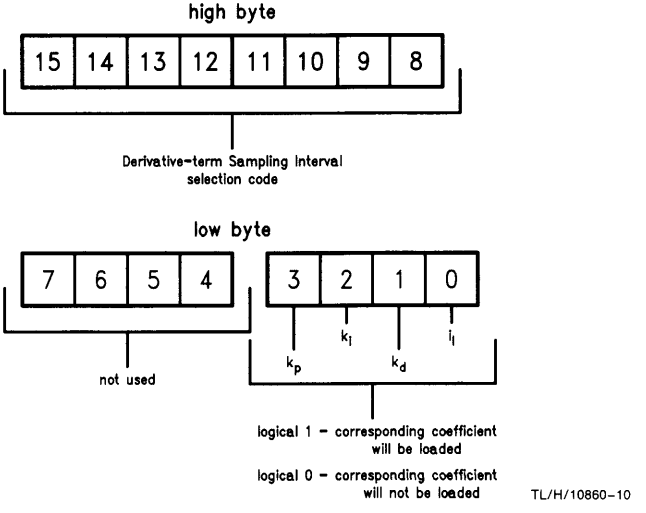

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TABLE IV. Derivative—Term Sampling Interval Selection Codes

Filter Control Word Bit Position								d_s	Selected Derivative-Term Sampling Interval—T_d
15	14	13	12	11	10	9	8		
0	0	0	0	0	0	0	0	1	T_s
0	0	0	0	0	0	0	1	2	$2T_s$
0	0	0	0	0	0	1	0	3	$3T_s$
0	0	0	0	0	0	1	1	4	$4T_s$
			•					•	•
			•					•	•
			•					•	•
1	1	1	1	1	1	1	1	256	$256T_s$

$T_s = (2048) \times \left(\frac{1}{f_{CLK}}\right)$ System Sample Period

$T_d = d_s \times T_s$ Derivative-term Sampling Interval

Port	Bytes	Command	Comments
c	1E	LFIL	This command initiates loading the filter coefficients input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the filter
d	x8	LB	control word. A 00 hex HB sets the derivative sampling interval to $2048/f_{CLK}$ by setting d_s to one. A x8 hex LB indicates only k_p will be loaded. The other filter parameters will remain at zero, their reset default value.
		Busy-bit Check Module	
d	00	HB	These two bytes set k_p
d	0A	LB	to ten.
		Busy-bit Check Module	
c	04	UDF	This command transfers new filter coefficients from input buffers to working registers. Until UDF is executed, coefficients loaded via the LFIL command do not affect the filter transfer characteristic.
		Busy-bit Check Module	

FIGURE 6. Filter Programming Module

Comments

After executing both the example initialization and example filter programming modules, the following observations are made. Filter gain is nonzero, but desired shaft position continues to track actual shaft position. Under these conditions, the motor drive signal remains at zero. The shaft should be stationary and "free wheeling". If there is significant drive amplifier offset, the shaft may rotate slowly, but with minimal torque capability.

Initially, k_p should be set below twenty, d_s should be set to one, and k_i, k_d, and i_l should remain at zero. These values will not provide optimum system performance, but they will be sufficient to test system functionality. See Tuning the PID Filter.

TRAJECTORY PROGRAMMING MODULE

Figure 7 details the example trajectory programming module.

Load Trajectory Parameters.

An LTRJ (Load TRaJectory) command sequence includes command LTRJ, a trajectory control word, and a variable number of data words.

The LTRJ command initiates loading trajectory parameters into input buffers.

The two data bytes, written immediately after LTRJ, comprise the trajectory control word. The first byte programs, with logical ones in respective bit positions, the trajectory mode (velocity or position), velocity mode direction, and stopping mode. See Stop Module. The second byte indicates, with logical ones in respective bit positions, which of the three trajectory parameters will be loaded. It also indicates whether the parameters are absolute or relative. See *Table V*. Any combination of the three parameters can be loaded within a single LTRJ command sequence.

Immediately following the trajectory control word, the trajectory parameters are written. Each parameter is written as a pair of data words (four data bytes). Because any combination of the three parameters can be loaded within a single LTRJ command sequence, the number of data words following the trajectory control word can vary in the range from zero to six.

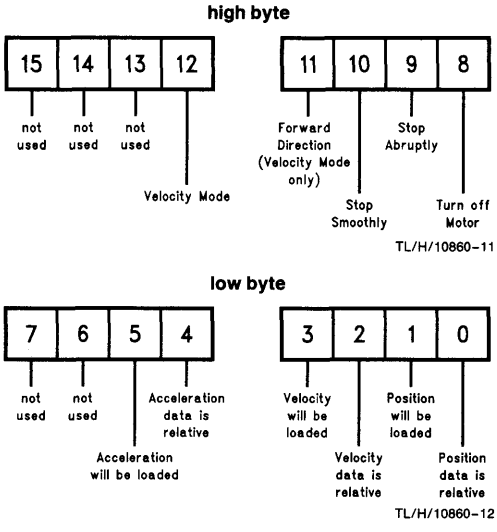
In the case of the example module, the first byte of the trajectory control word, 00 hex, programs the LM628 to operate in position mode. The second byte, 0A hex, indicates velocity and position will be loaded and both parameters are absolute. Four data words, two for each parameter loaded, follow the trajectory control word.

Start Motion Control

The start motion control command, STT (STarT), transfers new trajectory parameters from input buffers to working registers and begins execution of the new trajectory. Until STT is executed, the new trajectory parameters do not affect shaft motion.

Note: At this point no actual trajectory parameters are loaded. Calculation of trajectory parameters and execution of example moves is left for a later section.

Table V. Trajectory Control Word Bit Allocation



Port	Bytes	Command	Comments
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the
d	0A	LB	trajectory control word. A 0A hex LB indicates velocity and position will be loaded and both parameters are absolute.
		Busy-bit Check Module	
d	xx	HB	Velocity is loaded in two data
d	xx	LB	words. These two bytes are the high data word.
		Busy-bit Check Module	
d	xx	HB	velocity data word (low)
d	xx	LB	
		Busy-bit Check Module	
d	xx	HB	Position is loaded in two data
d	xx	LB	words. These two bytes are the high data word.
		Busy-bit Check Module	
d	xx	HB	position data word (low)
d	xx	LB	
		Busy-bit Check Module	
c	01	STT	STT must be issued to execute the desired trajectory.
		Busy-bit Check Module	

FIGURE 7. Trajectory Programming Module

STOP MODULE

This module demonstrates the programming flow required to stop shaft motion.

While the LM628 operates in position mode, normal stopping is always smooth and occurs automatically at the end of a specified trajectory (i.e. no stop module is required). Under exceptional conditions, however, a stop module can be used to affect a premature stop.

While the LM628 operates in velocity mode, stopping is always accomplished via a stop module.

The example stop module, shown in *Figure 8*, utilizes an LTRJ command sequence and an STT command.

Load Trajectory Parameters

Bits eight through ten of the trajectory control word select the stopping mode. See *Table V*.

In the case of the example module, the first byte of the trajectory control word, x1 hex, selects motor-off as the desired stopping mode. This mode stops shaft motion by setting the motor drive signal to zero (the appropriate offset-binary code to apply zero drive to the motor).

Setting bit nine of the trajectory control word selects stop abruptly as the desired stopping mode. This mode stops shaft motion (at maximum deceleration) by setting the target position equal to the current position.

Setting bit ten of the trajectory control word selects stop smoothly as the desired stopping mode. This mode stops shaft motion by decelerating at the current user-programmed acceleration rate.

Note: Bits eight through ten of the trajectory control word must be used exclusively; only one of them should be logic one at any time.

Start Motion Control

The start motion control command, STT, must be executed to stop shaft motion.

Comments

After shaft motion is stopped with either an "abrupt" or a "smooth" stop module, the control system will attempt to hold the shaft at its current position. If forced away from this desired resting position and released, the shaft will move back to the desired position. Unless new trajectory parameters are loaded, execution of another STT command will restart the specified move.

After shaft motion is stopped with a "'motor-off" stop module, desired shaft position tracks actual shaft position. Consequently, the motor drive signal remains at zero and the control system can not affect shaft position; the shaft should be stationary and free wheeling. If there is significant drive amplifier offset, the shaft may rotate slowly, but with minimal torque capability. Unless new trajectory parameters are loaded, execution of another STT command will restart the specified move.

Port	Bytes	Command	Comments
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	x1	HB	These two bytes are the
d	00	LB	trajectory control word. A x1 hex HB selects motor-off as the desired stopping mode. A 00 hex LB indicates no trajectory parameters will be loaded.
		Busy-bit Check Module	
c	01	STT	The start motion control command, STT, must be executed to stop shaft motion.
		Busy-bit Check Module	

FIGURE 8. Stop Module (Motor-Off)

II. PROGRAMS

This section focuses on the development of four brief LM628 programs.

LOOP PHASING PROGRAM

Following initial power-up, the correct polarity of the motor drive signal must be determined. If the polarity is incorrect (loop inversion), the drive signal will push the shaft away

from its desired position rather than towards it. This results in "motor runaway", a condition characterized by the motor running continuously at high speed.

The loop phasing program, detailed in *Figure 9*, contains both the example initialization and filter programming modules. It also contains an LTRJ command sequence and an STT command.

Note: Execution of this simple program is only required the *first* time a new system is used.

Load Trajectory Parameters

An LTRJ (Load TRaJectory) command sequence includes command LTRJ, a trajectory control word, and a variable number of data words.

In the case of the Loop Phasing Program, the first byte of the trajectory control word, 00 hex, programs the LM628 to operate in position mode. The second byte, 00 hex, indicates no trajectory parameters will be loaded (i.e. in this program, zero data words follow the trajectory control word). The three trajectory parameters will remain at zero, their reset value.

Start Motion Control

The start motion control command, STT (STarT), transfers new trajectory parameters from input buffers to working registers and begins execution of the new trajectory. Until STT is executed, the new trajectory parameters do not affect shaft motion.

Port	Bytes	Command	Comments
		Initialization Module	
		Filter Programming Module	
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the trajectory control word. A 00 hex LB indicates no trajectory parameters will be loaded.
d	00	LB	
		Busy-bit Check Module	
c	01	STT	STT must be issued to execute the desired trajectory.

FIGURE 9. Loop Phasing Program

Comments

Execution of command STT results in execution of the desired trajectory. With the acceleration set at zero, the profile generator generates a desired shaft position that is both constant and equal to the current absolute position. See *Figure 5*. Under these conditions, the control system will attempt to hold the shaft at its current absolute postion. The shaft will feel lightly "spring loaded". If forced (CAREFULLY) away from its desired position and released, the shaft will spring back to the desired position.

If the polarity of the motor drive signal is incorrect (loop inversion), motor runaway will occur immediately after execution of command STT, or after the shaft is forced (CAREFULLY) from its resting position.

Loop inversion can be corrected with one of three methods: interchanging the shaft position encoder signals (channel A and channel B), interchanging the motor power leads, or inverting the motor command signal before application to the motor drive amplifier. For LM629 based systems, loop inversion can be corrected by interchanging the motor power leads, interchanging the shaft position encoder signals, or logically inverting the PWM sign signal.

SIMPLE ABSOLUTE POSITION MOVE

The Simple Absolute Position Move Program, detailed in *Figure 13*, utilizes both the initialization and filter programming modules, as well as, an LTRJ command sequence and an STT command.

Factors that influenced the development of this program included the following: the program must demonstrate simple trajectory parameters calculations, the program must demonstrate the programming flow required to load and execute an absolute position move, and correct completion of the move must be verifiable through simple observation.

Move: The shaft will accelerate at 0.1 rev/sec^2 until it reaches a maximum velocity of 0.2 rev/sec, and then decelerate to a stop exactly two revolutions from the starting position. See *Figure 10*.

Note: Absolute position is position measured relative to zero (home). An absolute position move is a move that ends at a specified absolute position. For example, independent of the current absolute position of the shaft, if an absolute position of 30,000 counts is specified, upon completion of the move the absolute position of the shaft will be 30,000 counts (i.e. 30,000 counts relative to zero). The example program calls for a position move of two revolutions. Because the starting absolute position is 0 counts, the move is accomplished by specifying an absolute position of 8000 counts. See *Figure 13*.

The Quadrature Incremental Encoder

As a supplement to the trajectory parameters calculations, a brief discussion is provided here to differentiate between encoder ***lines*** and encoder ***counts***.

A quadrature incremental shaft encoder encodes shaft rotation as electrical pulses. *Figure 11* details the signals generated by a 3-channel quadrature incremental encoder. The LM628 decodes (or "counts") a quadrature incremental signal to determine the absolute position of the shaft.

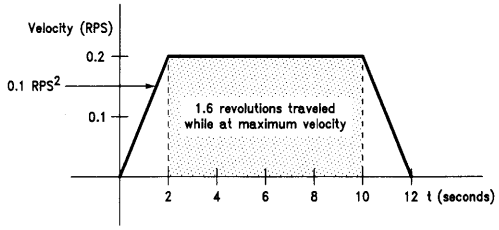


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FIGURE 10. Velocity Profile for Simple Absolute Position Move Program

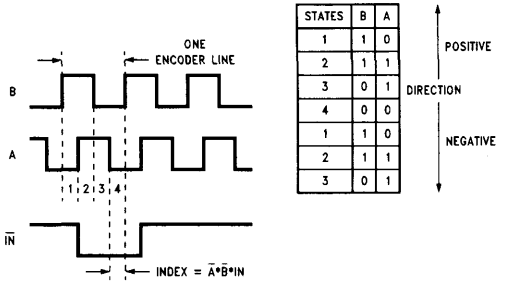

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FIGURE 11. 3-Channel Quadrature Encoder Signals

The resolution of a quadrature incremental encoder is usually specified as a number of ***lines***. This number indicates the number of cycles of the output signals for each complete shaft revolution. For example, an N-line encoder generates N cycles of its output signals during each complete shaft revolution.

By definition, two signals that are in quadrature are 90° out of phase. When considered together, channels A and B *(Figure 11)* traverse four distinct digital states during each full cycle of either channel. Each state transition represents one ***count*** of shaft motion. The leading channel indicates the direction of shaft rotation.

Each line, therefore, represents one cycle of the output signals, and each cycle represents four encoder counts.

$$\left(N\frac{\text{CYCLES}}{\text{REVOLUTION}}\right)\times\left(4\frac{\text{COUNTS}}{\text{CYCLE}}\right)=4N\frac{\text{COUNTS}}{\text{REVOLUTION}}$$

The reference system uses a one thousand line encoder.

$$\left(1000\frac{\text{CYCLES}}{\text{REVOLUTION}}\right)\times\left(4\frac{\text{COUNTS}}{\text{CYCLE}}\right)=4000\frac{\text{COUNTS}}{\text{REVOLUTION}}$$

Sample Period

Sampling of actual shaft position occurs at a fixed frequency, the reciprocal of which is the system sample period. The system sample period is the unit of time upon which shaft acceleration and velocity are based.

$$T_S = (2048)\times\left(\frac{1}{f_{CLOCK}}\right)\ \text{System Sample Period}$$

The reference system uses an 8 MHz clock. The sample period of the reference system follows directly from the definition.

$$T_S = (2048)\times\left(\frac{1}{8\times10^6\ \text{Hz}}\right) = 256\times10^{-6}\frac{\text{SECONDS}}{\text{SAMPLE}}$$

Trajectory Parameters Calculations

The shaft will accelerate at 0.1 rev/sec^2 until it reaches a maximum velocity of 0.2 rev/sec, and then decelerate to a stop exactly two revolutions from the starting position.

Trajectory parameters calculations for this move are detailed in *Figure 12*.

Comments

After completing the move, the control system will attempt to hold the shaft at its current absolute position. The shaft will feel lightly "spring loaded". If forced away from its desired resting position and released, the shaft will move back to the desired position.

$$A = \left(4000\frac{\text{COUNTS}}{\text{REVOLUTION}}\right)\times\left(256\times10^{-6}\frac{\text{SECONDS}}{\text{SAMPLE}}\right)^2\times\left(0.1\frac{\text{REVOLUTIONS}}{\text{SECOND}^2}\right) = 2.62\times10^{-5}\frac{\text{COUNTS}}{\text{SAMPLE}^2}$$

$$A = \left(2.62\times10^{-5}\frac{\text{COUNTS}}{\text{SAMPLE}^2}\right)\times(65{,}536) = 1.718\frac{\text{COUNTS}}{\text{SAMPLE}^2}\qquad\text{Acceleration Scaled}$$

$$A = 2\frac{\text{COUNTS}}{\text{SAMPLE}^2}\qquad\text{Acceleration Rounded}$$

$$A = 00\ 00\ 00\ 02\ \text{hex}\frac{\text{COUNTS}}{\text{SAMPLE}^2}$$

$$V = \left(4000\frac{\text{COUNTS}}{\text{REVOLUTION}}\right)\times\left(256\times10^{-6}\frac{\text{SECONDS}}{\text{SAMPLE}}\right)\times\left(0.2\frac{\text{REVOLUTIONS}}{\text{SECOND}}\right) = 0.2048\frac{\text{COUNTS}}{\text{SAMPLE}}$$

$$V = \left(0.2048\frac{\text{COUNTS}}{\text{SAMPLE}}\right)\times(65{,}536) = 13{,}421.77\frac{\text{COUNTS}}{\text{SAMPLE}}\qquad\text{Velocity Scaled}$$

$$V = 13{,}422\frac{\text{COUNTS}}{\text{SAMPLE}}\qquad\text{Velocity Rounded}$$

$$V = 00\ 00\ 34\ 6E\ \text{hex}\frac{\text{COUNTS}}{\text{SAMPLE}}$$

$$P = \left(4000\frac{\text{COUNTS}}{\text{REVOLUTION}}\right)\times(2.0\ \text{REVOLUTIONS}) = 8000\ \text{COUNTS}$$

$$P = 00\ 00\ 1F\ 40\ \text{hex COUNTS}$$

FIGURE 12. Calculations of Trajectory Parameters for Simple Absolute Position Move

Port	Bytes	Command	Comments
		Initialization Module	
		Filter Programming Module	
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers
		Busy-bit Check Module	
d	00	HB	These two bytes are the
d	2A	LB	trajectory control word. A 2A hex LB indicates acceleration, velocity, and position will be loaded and all three parameters are absolute.
		Busy-bit Check Module	
d	00	HB	Acceleration is loaded in two
d	00	LB	data words. These two bytes are the high data word. In this case, the acceleration is 0.1 rev/sec^2.
		Busy-bit Check Module	
d	00	HB	acceleration data word (low)
d	02	LB	
		Busy-bit Check Module	
d	00	HB	velocity is loaded in two data
d	00	LB	words. These two bytes are the high data word. In this case, the velocity is 0.2 rev/sec.
		Busy-bit Check Module	
d	34	HB	velocity data word (low)
d	6E	LB	
		Busy-bit Check Module	
d	00	HB	Position is loaded in two data
d	00	LB	words. These two bytes are the high data word. In this case, the position loaded is eight thousand counts. This results in a move of two revolutions in the forward direction.
		Busy-bit Check Module	
d	1F	HB	position data word (low)
d	40	LB	
		Busy-bit Check Module	
c	01	STT	STT must be issued to execute the desired trajectory.

FIGURE 13. Simple Absolute Position Move Program

SIMPLE RELATIVE POSITION MOVE

This program demonstrates the programming flow required to load and execute a relative position move. See *Figure 14.*

Move: Independent of the current resting position of the shaft, the shaft will complete thirty revolutions in the reverse direction. Total time to complete the move is fifteen seconds. Total time for acceleration and deceleration is five seconds.

Note: Target position is the final requested position. If the shaft is stationary, and motion has not been stopped with a "motor-off" stop module, the current absolute position of the shaft is the target position. If motion has been stopped with a "motor-off" stop module, or a position move has begun, the absolute position that corresponds to the endpoint of the current trajectory is the target position. Relative position is position measured relative to the current target position of the shaft. A relative position move is a move that ends the specified "relative" number of counts away from the current target position of the shaft. For example, if the current target position of the shaft is 10 counts, and a relative position of 30,000 counts is specified, upon completion of the move the absolute position of the shaft will be 30,010 counts (i.e. 30,000 counts relative to 10 counts).

Load Trajectory Parameters

The first byte of the trajectory control word, 00 hex, programs position mode operation. The second byte, 2B hex, indicates all three trajectory parameters will be loaded. It also indicates both acceleration and velocity will be absolute values while position will be a relative value.

Trajectory Parameters Calculations

Independent of the current resting position of the shaft, the shaft will complete thirty revolutions in the reverse direction. Total time to complete the move is fifteen seconds. Total time for acceleration and deceleration is five seconds.

The reference system utilizes a one thousand line encoder. The number of counts for each complete shaft revolution and the total counts for this position move are determined.

$$\left(1000\,\frac{\text{CYCLES}}{\text{REVOLUTION}}\right)\times\left(4\,\frac{\text{COUNTS}}{\text{CYCLE}}\right)=4000\,\frac{\text{COUNTS}}{\text{REVOLUTION}}$$

$$\left(4000\,\frac{\text{COUNTS}}{\text{REVOLUTION}}\right)\times(30\ \text{REVOLUTIONS})=120{,}000\ \text{COUNTS}$$

With respect to time, two-thirds of the move is made at maximum velocity and one-third is made at a velocity equal to one-half the maximum velocity.† Therefore, total counts traveled during acceleration and deceleration periods is one-fifth the total counts traveled. See *Figure 15.*

$$\frac{120{,}000\ \text{COUNTS}}{5}=24{,}000\ \text{COUNTS}\quad\text{total counts traveled during acceleration and deceleration}$$

$$\frac{24{,}000\ \text{COUNTS}}{2}=12{,}000\ \text{COUNTS}\quad\text{counts traveled during acceleration}$$

The reference system uses an 8 MHz clock. The sample period of the reference system is determined.

$$T_S=(2048)\times\left(\frac{1}{8\times10^6\text{Hz}}\right)=256\times10^{-6}\,\frac{\text{SECONDS}}{\text{SAMPLE}}$$

The number of samples during acceleration (and deceleration) is determined.

$$\frac{2.5\ \text{SECONDS}}{256\times10^{-6}\,\frac{\text{SECONDS}}{\text{SAMPLE}}}=9766\ \text{SAMPLES}\quad\text{number of samples during acceleration}$$

Using the number of counts traveled during acceleration and the number of samples during acceleration, acceleration is determined.

$$s=\frac{at^2}{2}\quad\text{distance traveled during time t at acceleration a}$$

$$a=\frac{2s}{t^2}=\frac{(2)\times(12{,}000\ \text{COUNTS})}{(9766\ \text{SAMPLES})^2}=0.000252\,\frac{\text{COUNTS}}{\text{SAMPLE}^2}$$

Total counts traveled while at maximum velocity is four-fifths the total counts traveled.

$$\frac{(4)\times(120{,}000\ \text{COUNTS})}{5}=96{,}000\ \text{COUNTS}$$

†Average velocity during acceleration and deceleration periods is one-half the maximum velocity.

Port	Bytes	Command	Comments
		Initialization Module	
		Filter Programming Module	
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the
d	2B	LB	trajectory control word. A 2B hex LB indicates all three parameters will be loaded and both acceleration and velocity will be absolute values while position will be a relative value.
		Busy-bit Check Module	
d	00	HB	Acceleration is loaded in two
d	00	LB	data words. These two bytes are the high data word. In this case, the acceleration is 17 counts/sample^2.
		Busy-bit Check Module	
d	00	HB	acceleration data word (low)
d	11	LB	
		Busy-bit Check Module	
d	00	HB	Velocity is loaded in two data
d	02	LB	words. These two bytes are the high data word. In this case, velocity is 161,087 counts/sample.
		Busy-bit Check Module	
d	75	HB	velocity data word (low)
d	3F	LB	
		Busy-bit Check Module	
d	FF	HB	Position is loaded in two data
d	FE	LB	words. These two bytes are the high data word. In this case, the position loaded is −120,000 counts. This results in a move of thirty revolutions in the reverse direction.
		Busy-bit Check Module	
d	2B	HB	position data word (low)
d	40	LB	
		Busy-bit Check Module	
c	01	STT	STT must be issued to execute the desired trajectory.

FIGURE 14. Simple Relative Position Move Program

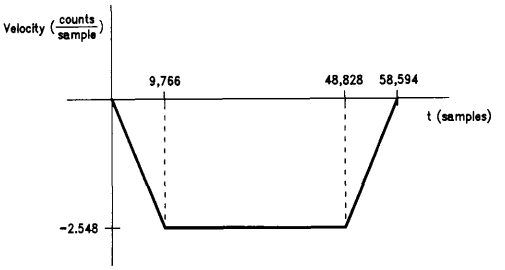

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FIGURE 15. Velocity Profile for Simple Relative Position Move Program

The number of samples while at maximum velocity is determined.

$$\frac{10 \text{ SECONDS}}{256 \times 10^{-6} \dfrac{\text{SECONDS}}{\text{SAMPLE}}} = 39{,}062 \text{ SAMPLES}$$ number of samples while at maximum velocity

Using the total counts traveled while at maximum velocity and the number of samples while at maximum velocity, velocity is determined.

$$\frac{96{,}000 \text{ COUNTS}}{39{,}062 \text{ SAMPLES}} = 2.458 \frac{\text{COUNTS}}{\text{SAMPLE}}$$

Both acceleration and velocity values are scaled.

$$\left(0.000252 \frac{\text{COUNTS}}{\text{SAMPLE}^2}\right) \times (65{,}536) = 16.515 \frac{\text{COUNTS}}{\text{SAMPLE}^2}$$

$$\left(2.458 \frac{\text{COUNTS}}{\text{SAMPLE}}\right) \times (65{,}536) = 161{,}087.488 \frac{\text{COUNTS}}{\text{SAMPLE}}$$

Acceleration and velocity are rounded to the nearest integer and all three trajectory parameters are converted to hexadecimal.

$$A = 17 = 00\ 00\ 00\ 11 \text{ hex} \frac{\text{COUNTS}}{\text{SAMPLE}^2}$$

$$V = 161{,}087 = 00\ 02\ 75\ 3F \text{ hex} \frac{\text{COUNTS}}{\text{SAMPLE}}$$

$$P = -120{,}000 = \text{FF FE 2B 40 hex COUNTS}$$

BASIC VELOCITY MODE MOVE WITH BREAKPOINTS

This program demonstrates basic velocity mode programming and the (typical) programming flow required to set both absolute and relative breakpoints. See *Figure 17.*

Move: The shaft will accelerate at 1.0 rev/sec^2 until it reaches a maximum velocity of 2.0 rev/sec. After completing twenty forward direction revolutions (including revolutions during acceleration), the shaft will accelerate at 1.0 rev/sec^2 until it reaches a maximum velocity of 4.0 rev/sec. After completing twenty forward direction revolutions (including revolutions during acceleration), the shaft will decelerate (at 1.0 rev/sec^2) to a stop. See *Figure 16.*

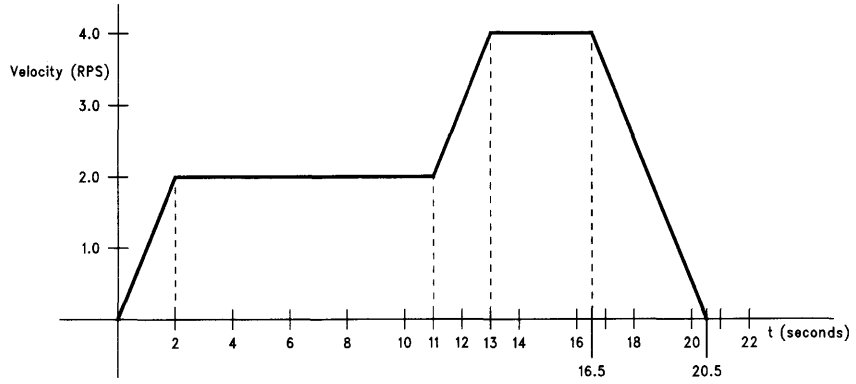

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FIGURE 16. Velocity Profile for Basic Velocity Mode with Breakpoints Program

Mask Interrupts

An MSKI command sequence allows the user to determine which interrupt conditions result in host interrupts; interrupting the host via the host interrupt output (pin 17). It contains an MSKI command and one data word.

The MSKI command initiates interrupt masking.

Immediately following the MSKI command, a single data word is written. The first byte is not used. Bits one through six of the second byte determine the masked/unmasked status of each interrupt. See *Table II*. Any zeros in this 6-bit field mask (disable) the corresponding interrupts while any ones unmask (enable) the corresponding interrupts.

In the case of the examlple program, the second byte of the MSKI data word, 40 hex, enables the breakpoint interrupt. All other interrupts are disabled (masked).

When interrupted, the host processor can read the Status Byte to determine which interrupt condition(s) occurred. See *Table I*.

Note: Command MSKI controls only the host interrupt process. Bits one through six of the Status Byte reflect actual conditions independent of the masked/unmasked status of individual interrupts. This feature allows interrupts to be serviced with a polling scheme.

Set Breakpoints (Absolute and Relative)

An SBPA command sequence enables the user to set breakpoints in terms of absolute shaft position. An SBPR command sequence enables setting breakpoints relative to the current target position. When a breakpoint position is reached, bit six of the status byte, the breakpoint interrupt flag, is set to logic high. If this interrupt is enabled (unmasked), the host will be interrupted via the host interrupt output (pin 17).

An SBPA (or SBPR) command initiates loading/setting a breakpoint. The two data words, written immediately following the SBPA (or SBPR) command, represent the breakpoint position.

The example program contains a relative breakpoint set at 80,000 counts relative to position zero (the current target position). This represents a move of twenty forward direction revolutions. When this position is reached, the LM628 interrupts the host processor, and the host executes a sequence of commands that increases the maximum velocity, resets the breakpoint interrupt flag, and loads an absolute breakpoint.

The example program contains an absolute breakpoint set at 160,000 counts. When this absolute position is reached, the LM628 interrupts the host processor, and the host executes a Smooth Stop Module.

Breakpoint positions for this example program are determined.

$$\left(4000\,\frac{\text{COUNTS}}{\text{REVOLUTION}}\right) \times (20\ \text{REVOLUTIONS})$$

$$= 80{,}000\ \text{COUNTS} \quad \begin{matrix}\text{relative}\\ \text{breakpoint}\end{matrix}$$

$$\left(4000\,\frac{\text{COUNTS}}{\text{REVOLUTION}}\right) \times (40\ \text{REVOLUTIONS})$$

$$= 160{,}000\ \text{COUNTS} \quad \begin{matrix}\text{absolute}\\ \text{breakpoint}\end{matrix}$$

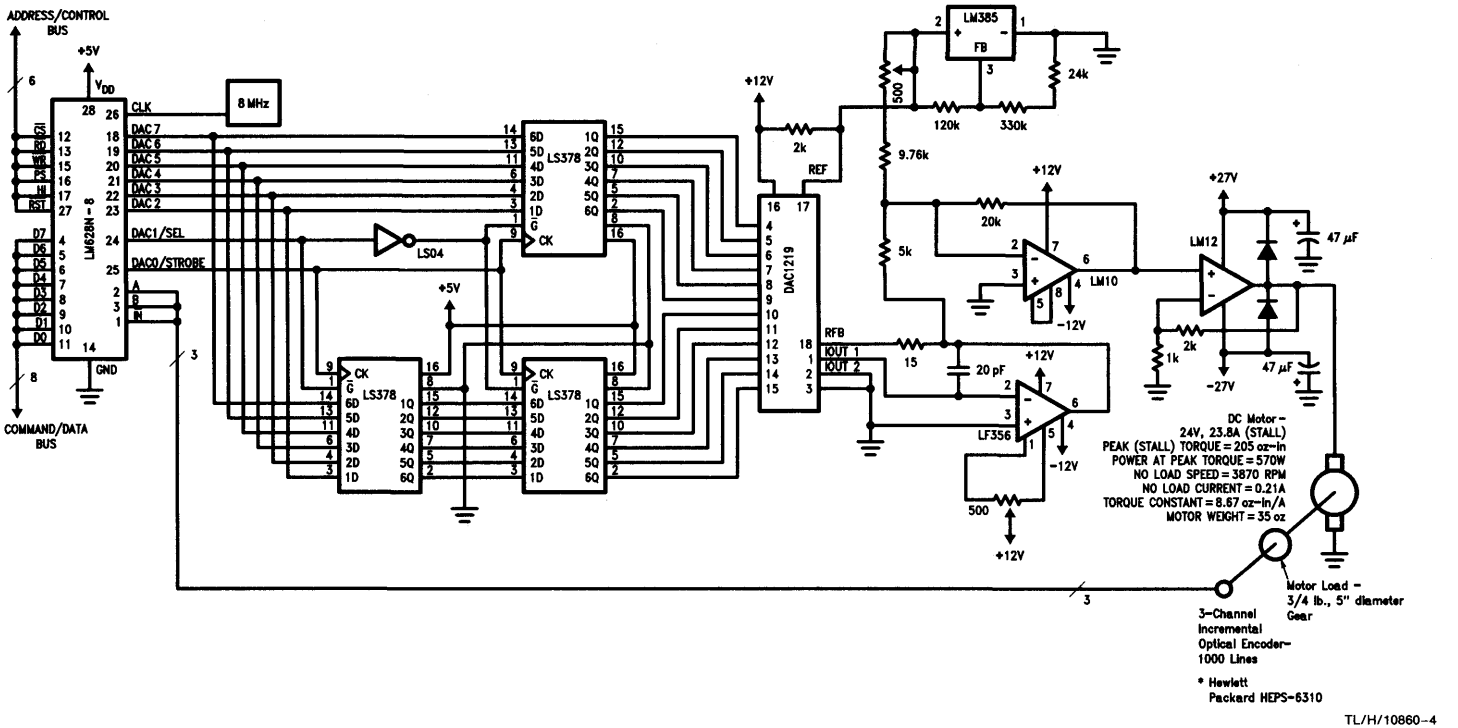
Load Trajectory Parameters

This example program contains two LTRJ command sequences. The trajectory control word of the first LTRJ command sequence, 1828 hex, programs forward direction velocity mode, and indicates an absolute acceleration and an absolute velocity will be loaded. The trajectory control word of the second LTRJ command sequence, 180C hex, programs forward direction velocity mode, and indicates a relative velocity will be loaded. See *Table V*.

Trajectory parameters calculations follow the same format as those detailed for the simple absolute position move. See *Figure 12*.

Port	Bytes	Command	Comments
		Initialization Module	
		Filter Programming Module	
c	1C	MSKI	Mask interrupts.
		Busy-bit Check Module	
d	xx	HB	don't care
d	40	LB	A 40 hex LB enables (unmasks) the breakpoint interrupt. All other interrupts are disabled (masked).
		Busy-bit Check Module	
c	21	SPBR	This command initiates loading a relative breakpoint.
		Busy-bit Check Module	
d	00	HB	A breakpoint is loaded in two
d	01	LB	data words. These two bytes are the high data word. In this case, the breakpoint is 80,000 counts relative to the current commanded target position (zero).
		Busy-bit Check Module	
d	38	HB	breakpoint data word (low)
d	80	LB	
		Busy-bit Check Module	
c	1F	LTRJ	Load trajectory.
		Busy-bit Check Module	
d	18	HB	These two bytes are the
d	28	LB	trajectory control word. A 18 hex HB programs forward direction velocity mode operation. A 28 hex LB indicates acceleration and velocity will be loaded and both values are absolute.
		Busy-bit Check Module	
d	00	HB	Acceleration is loaded in two
d	00	LB	data words. These two bytes are the high data word. In this case, the acceleration is 1.0 rev/sec^2.
		Busy-bit Check Module	
d	00	HB	acceleration data word (low)
d	11	LB	
		Busy-bit Check Module	
d	00	HB	Velocity is loaded in two data
d	02	LB	words. These two bytes are the high data word. In this case, velocity is 2.0 rev/s.
		Busy-bit Check Module	
d	0C	HB	velocity data word (low)
d	4A	LB	
		Busy-bit Check Module	
c	01	STT	Start motion control.
		Busy-bit Check Module	
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	18	HB	These two bytes are the
d	0C	LB	trajectory control word. A 18 hex HB programs forward direction velocity mode operation. A 0C hex LB indicates only velocity will be loaded and it will be a relative value.
		Busy-bit Check Module	
d	00	HB	Velocity is loaded in two data
d	02	LB	words. These two bytes are the high data word. In this case, velocity is 2.0 rev/s. Because this is a relative value, the current velocity will be increased by 2.0 rev/s. The resultant velocity will be 4.0 rev/s.
		Busy-bit Check Module	
d	0C	HB	velocity data word (low)
d	4A	LB	
		wait	This wait represents the host processor waiting for an LM628 breakpoint interrupt.
c	01	STT	Start motion control.
		Busy-bit Check Module	
c	1D	RSTI	Reset interrupts.
		Busy-bit Check Module	
d	xx	HB	don't care
d	00	LB	Zeros in bits one through six reset **all** interrupts.
		Busy-bit Check Module	
c	20	SPBA	This command initiates loading an absolute breakpoint.
		Busy-bit Check Module	
d	00	HB	A breakpoint is loaded in two
d	02	LB	data words. These two bytes are the high data word. In this case, the breakpoint is 160,000 counts absolute.
		Busy-bit Check Module	
d	71	HB	breakpoint data word (low)
d	00	LB	
		wait	This wait represents the host processor waiting for an LM628 breakpoint interrupt.
		"Smooth" Stop Module	

FIGURE 17. Basic Velocity Mode Move with Breakpoints Program



*Note: All resistor values in Ω

FIGURE 18. Reference System

III. TUNING THE PID FILTER

BACKGROUND

The transient response of a control system reveals important information about the "quality" of control, and because a step input is easy to generate and sufficiently drastic, the transient response of a control system is often characterized by the response to a step input, the system step response.

In turn, the step response of a control system can be characterized by three attributes: maximum overshoot, rise time, and settling time. These step response attributes are defined in what follows and detailed graphically in *Figure 19.*

1. The maximum overshoot, Mp, is the maximum peak value of the response curve measured from unity. The amount of maximum overshoot directly indicates the relative stability of the system.
2. The rise time, t_r, is the time required for the response to rise from ten to ninety percent of the final value.
3. The settling time, t_s, is the time required for the response to reach and stay within two percent of the final value.

A critically damped control system provides optimum performance. The step response of a critically damped control system exhibits the minimum possible rise time that maintains zero overshoot and zero ringing (damped oscillations). *Figure 20* illustrates the step response of a critically damped control system.

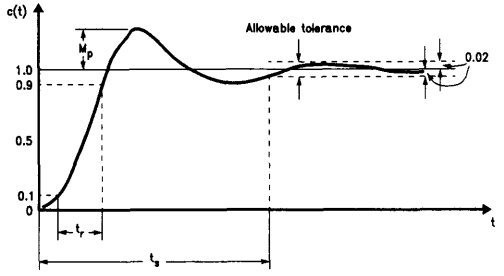


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FIGURE 19. Unit Step Response Curve Showing Transient Response Attributes

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FIGURE 20. Unit Step Response of a Critically Damped System

INTRODUCTION

The LM628 is a digital PID controller. The loop-compensation filter of a PID controller is usually tuned experimentally, especially if the system dynamics are not well known or defined.

The ultimate goal of tuning the PID filter is to critically damp the motor control system—provide optimum tracking and settling time.

As shown in *Figure 5*, the response of the PID filter is the sum of three terms, a proportional term, an integral term, and a derivative term. Five variables shape this response. These five variables include the three gain coefficients (k_p, k_i, and k_d), the integration limit coefficient (i_l), and the derivative sampling coefficient (d_s). *Tuning the filter equates to determining values for these variable coefficients, values that critically damp the control system.*

Filter coefficients are best determined with a two-step experimental approach. In the first step, the values of k_p, k_i, and k_d (along with i_l and d_s) are systematically varied until reasonably good response characteristics are obtained. Manual and visual methods are used to evaluate the effect of each coefficient on system behavior. In the second step, an oscilloscope trace of the system step response provides detailed information on system damping, and the filter coefficients, determined in step one, are modified to critically damp the system.

Note: In step one, adjustments to filter coefficient values are inherently coarse, while in step two, adjustments are inherently fine. Due to this coarse/fine nature, steps one and two complement each other, and the two-step approach is presented as the "best" tuning method. The PID filter can be tuned with either step one or step two alone.

STEP ONE—MANUAL VISUAL METHOD

Introduction

In the first step, the values of k_p, k_i, and k_d (along with i_l and d_s) are systematically varied until reasonably good response characteristics are obtained. Manual and visual methods are used to evaluate the effect of each coefficient on system behavior.

Note: The next four numbered sections are ordered steps to tuning the PID filter.

1. Prepare the System

The initialization section of the filter tuning program is executed to prepare the system for filter tuning. See *Figure 22.* This section initializes the system, presets the filter parameters (k_p, k_i, il = 0, k_d = 2, d_s = 1), and commands the control loop to hold the shaft at the current position.

After executing the initialization section of the filter tuning program, both desired and actual shaft positions equal zero; the shaft should be stationary. Any displacement of the shaft constitutes a position error, but with both k_p and k_i set to zero, the control loop can not correct this error.

2. Determine the Derivative Gain Coefficient

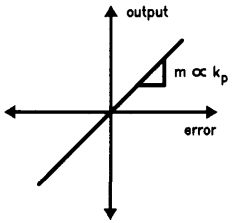
The filter derivative term provides damping to eliminate oscillation and minimize overshoot and ringing, stabilize the system. Damping is provided as a force proportional to the rate of change of position error, and the constant of proportionality is $k_d \times d_s$. See *Figure 21.*

Coefficients k_d and d_s are determined with an iterative process. Coefficient k_d is systematically increased until the shaft begins high frequency oscillations. Coefficient d_s is then increased by one. The entire process is repeated until d_s reaches a value appropriate for the system.

The system sample period sets the time interval between updates of position error. The derivative sampling interval is an integer multiple of the system sample period. See *Table IV.* It sets the time interval between successive position error samples used in the derivative term, and, therefore, directly affects system damping. The derivative sampling interval should be five to ten times smaller than the system mechanical time constant — this means many systems will require low d_s. In general, however, k_d and d_s should be set to give the largest $k_d \times d_s$ product that maintains acceptably low motor vibrations.

Note: Starting k_d at two and doubling it is a good method of increasing k_d. Manually turning the shaft reveals that with each increase of k_d, the resistance of the shaft to turning increases. The shaft feels increasingly sluggish and, because k_d provides a force proportional to the rate of change of position error, the faster the shaft is turned the more sluggish it feels. For the reference system, the final values of k_d and d_s are 4000 and 4 respectively.

Proportional Term



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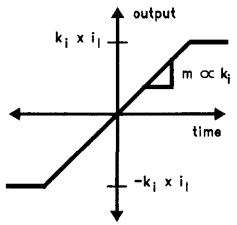
Integral Term



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Derivative Term

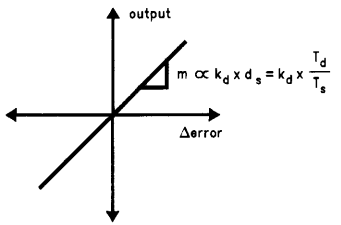

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FIGURE 21. Proportional, Integral, and Derivative (PID) Force Components

Port	Bytes	Command	Comments
c	00	RESET	See Initialization Module Text
		wait	The maximum time to complete RESET tasks is 1.5 ms.
c	06	PORT12	The RESET default size of the DAC port is eight bits. This command initializes the DAC port for a 12-bit DAC. It should not be issued in systems with an 8-bit DAC.
		Busy-bit Check Module	
c	1D	RSTI	This command resets **only** the interrupts indicated by *zeros in bits one* through six of the next data word. It also resets bit fifteen of the Signals Register and the host interrupt pin (pin 17).
		Busy-bit Check Module	
d	xx	HB	don't care
d	00	LB	Zeros in bits one through six indicate **all** interrupts will be reset.
		Busy-bit Check Module	
c	1C	MSKI	This command masks the interrupts indicated by zeros in bits one through six of the next data word.
		Busy-bit Check Module	
d	xx	HB	don't care
d	04	LB	A 04 hex LB enables (unmasks) the trajectory complete interrupt. All other interrupts are disabled (masked). See *Table II.*
		Busy-bit Check Module	
c	1E	LFIL	This command initiates loading the filter coefficients input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the filter
d	x2	LB	control word. A 00 hex HB sets the derivative sampling interval to $2048/f_{CLK}$ by setting d_s to one. A x2 hex LB indicates only k_d will be loaded. The other filter parameters will remain at zero, their reset default value.
		Busy-bit Check Module	
d	00	HB	These two bytes set k_d to
d	02	LB	two.
		Busy-bit Check Module	

FIGURE 22. Initialization Section— Filter Tuning Program

(Continued on Next Page)

Port	Bytes	Command	Comments
c	04	UDF	This command transfers new filter coefficients from input buffers to working registers. Until UDF is executed, coefficients loaded via the LFIL command do not affect the filter transfer characteristic.
		Busy-bit Check Module	
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the
d	00	LB	trajectory control word. A 00 hex LB indicates no trajectory parameters will be loaded.
		Busy-bit Check Module	
c	01	STT	STT must be issued to execute the desired trajectory.

FIGURE 22. Initialization Section—Filter Tuning Program (Continued)

3. Determine the Proportional Gain Coefficient

Inertial loading causes following (or tracking) error, position error associated with a moving shaft. External disturbances and torque loading cause displacement error, position error associated with a stationary shaft. The filter proportional term provides a restoring force to minimize these position errors. The restoring force is proportional to the position error and increases linearly as the position error increases. See *Figure 21.* The proportional gain coefficient, k_p, is the constant of proportionality.

Coefficient k_p is determined with an iterative process—the value of k_p is increased, and the system damping is evaluated. This is repeated until the system is critically damped.

System damping is evaluated manually. Manually turning the shaft reveals each increase of k_p increases the shaft "stiffness". The shaft feels spring loaded, and if forced away from its desired holding position and released, the shaft "springs" back. If k_p is too low, the system is over damped, and the shaft recovers too slowly. If k_p is too large, the system is under damped, and the shaft recovers too quickly. This causes overshoot, ringing, and possibly oscillation. The proportional gain coefficient, k_p, is increased to the largest value that does not cause excessive overshoot or ringing. At this point the system is critically damped, and therefore provides optimum tracking and settling time.

Note: Starting k_p at two and doubling it at each iteration is a good method of increasing k_p. The final value of k_p for the reference system is 40.

4. Determine the Integral Gain Coefficient

The filter proportional term minimizes the errors due to inertial and torque loading. The integral term, however, provides a corrective force that can eliminate following error while the shaft is spinning and the deflection effects of a static torque load while the shaft is stationary. This corrective force is proportional to the position error and increases linearly with time. See *Figure 21.* The integral gain coefficient, k_i, is the constant of proportionality.

High values of k_i provide quick torque compensation, but increase overshoot and ringing. In general, k_i should be set to the smallest value that provides the appropriate compromise between three system characteristics: overshoot, settling time, and time to cancel the effects of a static torque load. In systems without significant static torque loading, a k_i of zero may be appropriate.

The corrective force provided by the integral term increases linearly with time. The integration limit coefficient, i_l, acts as a clamping value on this force to prevent integral wind-up, a backlash effect. As noted in *Figure 21*, i_l limits the summation of error (over time), not the product of k_i and this summation. In many systems i_l can be set to its maximum value, 7FFF hex, without any adverse effects. The integral term has no effect if i_l is set to zero.

For the test system, the final values of k_i and i_l are 5 and 1000 respectively.

STEP TWO—STEP RESPONSE METHOD

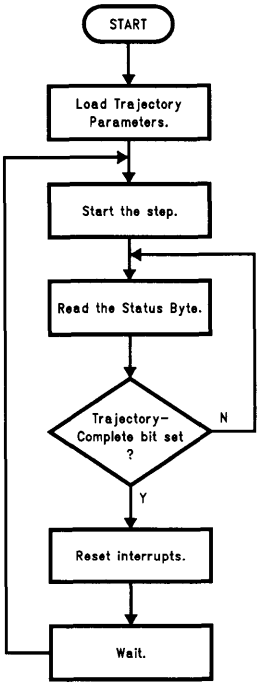
Introduction

The step response of a control system reveals important information about the "quality" of control—specifically, detailed information on system damping.

In the second step to tuning the PID filter, an oscilloscope trace of the control system step response is used to accurately evaluate system damping, and the filter coefficients, determined in step one, are fine tuned to critically damp the system.

Software Considerations

The step generation section of the filter tuning program provides the control loop with a repetitive small-signal step input. This is accomplished by repeatedly executing a small position move with high maximum velocity and high acceleration. See *Flow Diagram 3* and *Figure 23.*



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Flow Diagram 3. Step Generation Section of Filter Tuning Program

Port	Bytes	Command	Comments
c	1F	LTRJ	This command initiates loading the trajectory parameters input buffers.
		Busy-bit Check Module	
d	00	HB	These two bytes are the
d	2B	LB	trajectory control word. A 2B hex LB indicates acceleration, velocity, and position will be loaded and both acceleration and velocity are absolute while position is relative.
		Busy-bit Check Module	
d	00	HB	Acceleration is loaded in two
d	04	LB	data words. These two bytes are the high data word.
		Busy-bit Check Module	
d	93	HB	acceleration data word (low)
d	E0	LB	
		Busy-bit Check Module	
d	00	HB	Velocity is loaded in two data
d	07	LB	words. These two bytes are the high data word.
		Busy-bit Check Module	
d	A1	HB	velocity data word (low)
d	20	LB	
		Busy-bit Check Module	
d	00	HB	Position is loaded in two data
d	00	LB	words. These two bytes are the high data word.
		Busy-bit Check Module	
d	00	HB	position data word (low)
d	C8	LB	

Port	Bytes	Command	Comments
		Busy-bit Check Module	
c	01	STT	STT must be issued to execute the desired trajectory.
		Busy-bit Check Module	
c	xx	RDSTAT	This command reads the Status Byte. It is directly supported by LM628 hardware and can be executed at any time by pulling $\overline{CS}$, $\overline{PS}$, and $\overline{RD}$ logic low. Status information remains valid as long as $\overline{RD}$ is logic low.
		decision	If the Trajectory Complete interrupt bit is set, continue. Otherwise loop back to RDSTAT.
c	1D	RSTI	This command resets **only** the interrupts indicated by zeros in bits one through six of the next data word. It also resets bit fifteen of the Signals Register and the host interrupt pin (pin 17).
d	xx	HB	don't care
d	00	LB	Zeros in bits one through six indicate **all** interrupts will be reset.
		wait	This wait block inserts a delay between repetitions of the step input. The delay is application specific, but a good range of values for the delay is 5 ms to 5000 ms.
		loop	Loop back to STT.

FIGURE 23. Step Generation Section—Filter Tuning Program

Hardware Considerations

For a motor control system, an oscilloscope trace of the system step response is a graph of the real position of the shaft versus time after a small and instantaneous change in desired position.

For an LM628-based system, no extra hardware is needed to view the system step response. During a step, the voltage across the motor represents the system step response, and an oscilloscope is used to generate a graph of this response (voltage).

For an LM629-based system, extra hardware is needed to view the system step response. *Figure 24* illustrates a circuit for this purpose. During a step, the voltage output of this circuit represents the system step response, and an oscilloscope is used to generate a graph of this response.

The oscilloscope trigger signal, a rectangular pulse train, is taken from the host interrupt output pin (pin 17) of the LM628/LM629. This signal is generated by the combination of a trajectory complete interrupt and a reset interrupts (RSTI) command. See *Flow Diagram 3.*

Note: The circuit of *Figure 24* can be used to view the step response of an LM628-based system.

Observations

What follows are example oscilloscope traces of the step response of the reference system.

Note 1: All traces were generated using the circuit of *Figure 24.*

Note 2: All traces were generated using the following "step" trajectory parameters: relative position, 200 counts; absolute velocity, 500,000 counts/sample; acceleration, 300,000 counts/sample/sample. These values generated a good small-signal step input for the reference system; other systems will require different trajectory parameters. In general, step trajectory parameters consist of a small relative position, a high velocity, and a high acceleration.

The position parameter must be relative. Otherwise, a define home command (DFH) must be added to the main loop of the step generation section—filter tuning program. See *Flow Diagram 3.*

The circuit for viewing the system step response uses an 8-bit analog-to-digital converter. See *Figure 24.* To prevent converter overflow, the step position parameter must not be set higher than 200 counts.

Note 3: The circuit of *Figure 24* produces an "inverted" step response graph. The oscilloscope input was inverted to produce a positive-going (more familiar) step response graph.

Figure 25 represents the step response of an under damped control system; this response exhibits excessive overshoot and long settling time. The filter parameters used to generate this response were as follows: k_p, 35; k_i, 5; k_d, 600; d_s, 4; i_l, 1000. *Figure 25* indicates the need to increase k_d, the derivative gain coefficient.

Figure 26 represents the step response of an over damped control system; this response exhibits excessive rise time which indicates a sluggish system. The filter parameters used to generate this response were as follows: k_p, 35; k_i, 5; k_d, 10,000; d_s, 7; i_l, 1000. *Figure 26* indicates the need to decrease k_d and d_s.

Figure 27 represents the step response of a critically damped control system; this response exhibits virtually zero overshoot and short rise time. The filter parameters used to generate this response were as follows: k_p, 40; k_i, 5; k_d, 4000; d_s, 4; i_l, 1000.

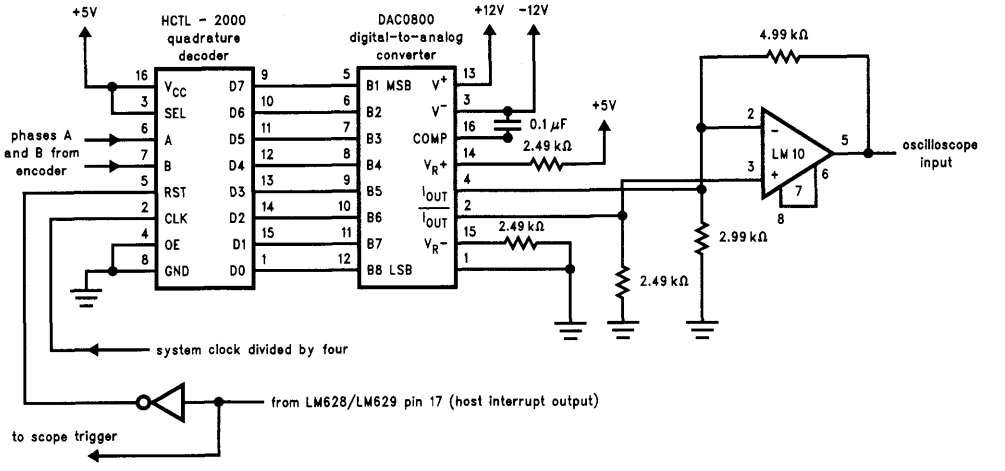

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FIGURE 24. Circuit for Viewing the System Step Response with an Oscilloscope

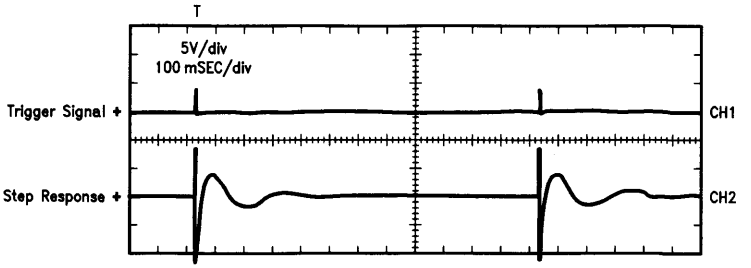

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FIGURE 25. The Step Response of an Under Damped Control System

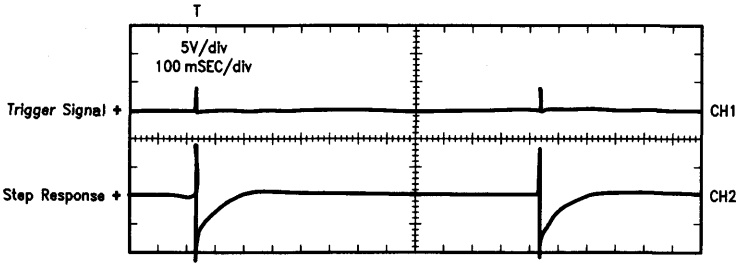

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FIGURE 26. The Step Response of an Over Damped Control System

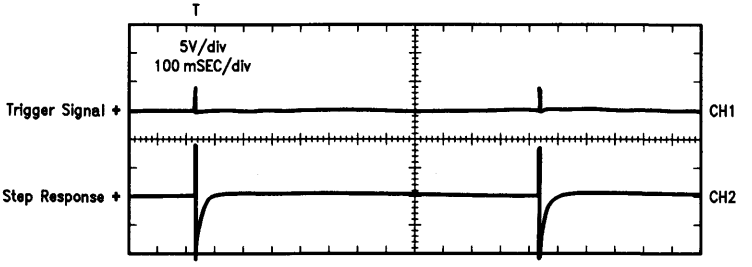

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FIGURE 27. The Step Response of a Critically Damped Control System

LM628/629 User Guide

National Semiconductor
Application Note 706

Table of Contents

List of Illustrations

1.0 INTRODUCTION

1.1 Application Note Objective

This application note is intended to explain and complement the information in the data sheet and also address the common user questions. While no initial familiarity with the LM628/629 is assumed, it will be useful to have the LM628/629 data sheet close by to consult for detailed descriptions of the user command set, timing diagrams, bit assignments, pin assignments, etc.

After the following brief description of the LM628/629, Section 2.0 gives a fairly full description of the device's operation, probably more than is necessary to get going with the device. This section ends with an outline of how to tune the control system by adjusting the PID filter coefficients.

Section 3 "User Command Set" discusses the use of the LM628/629 commands. For a detailed description of each command the user should refer to the data sheet.

Section 4 "Helpful User Ideas" starts with a short description of the actions necessary to get going, then proceeds to talk about some performance enhancements and follows on with a discussion of a couple of operating constraints of the device.

Section 5 "Theory" is a short foray into theory which relates the PID coefficients that would be calculated from a continuous domain control loop analysis to those of the discrete domain including the scaling factors inherent to the LM628/629. No attempt is made to discuss control system theory as such, readers should consult the ample references available, some suggestions are made at the end of this application note. Section 5 concludes with an example trajectory calculation, reviving those perhaps forgotten ideas about acceleration, velocity, distance and time.

Section 6 "Questions and Answers", is in question and answer format and is born out of and dedicated to the many interesting discussions with customers that have taken place.

1.2 Brief Description of LM628/629

LM628/629 is a microcontroller peripheral that incorporates in one device all the functions of a sample-data motion control system controller. Using the LM628/629 makes the potentially complex task of designing a fast and precise motion control system much easier. Additional features, such as trajectory profile generation, on the "fly" update of loop compensation and trajectory, and status reporting, are included. Both position and velocity motion control systems can be implemented with the LM628/629.

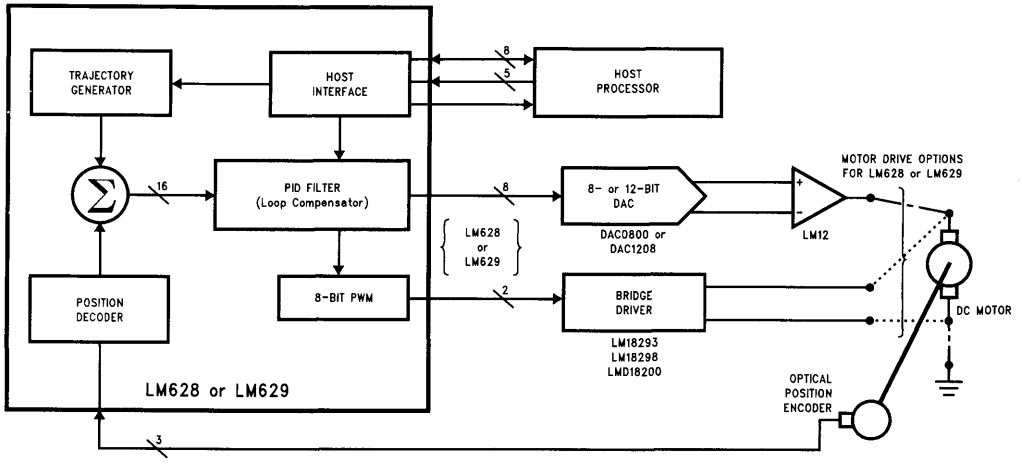

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FIGURE 1. LM628 and LM629 Typical System Block Diagram

LM628/629 is itself a purpose designed microcontroller that implements a position decoder, a summing junction, a digital PID loop compensation filter, and a trajectory profile generator, *Figure 1.* Output format is the only difference between LM628 and LM629. A parallel port is used to drive an 8- or 12-bit digital-to-analog converter from the LM628 while the LM629 provides a 7-bit plus sign PWM signal with sign and magnitude outputs. Interface to the host microcontroller is via an 8-bit bi-directional data port and six control lines which includes host interrupt and hardware reset. Maximum sampling rates of either 2.9 kHz or 3.9 kHz are available by choosing the LM6268/9 device options that have 6 MHz or 8 MHz maximum clock frequencies (device -6 or -8 suffixes).

In operation, to start a movement, a host microcontroller downloads acceleration, velocity and target position values to the LM628/629 trajectory generator. At each sample interval these values are used to calculate new demand or "set point" positions which are fed into the summing junction. Actual position of the motor is determined from the output signals of an optical incremental encoder. Decoded by the LM628/629's position decoder, actual position is fed to the other input of the summing junction and subtracted from the demand position to form the error signal input for the control loop compensator. The compensator is in the form of a "three term" PID filter (proportional, integral, derivative), this is implemented by a digital filter. The coefficients for the PID digital filter are most easily determined by tuning the control system to give the required response from the load in terms of accuracy, response time and overshoot. Having characterized a load these coefficient values are downloaded from the host before commencing a move. For a load that varies during a movement more coefficients can be downloaded and used to update the PID filter at the moment the load changes. All trajectory parameters except acceleration can also be updated while a movement is in progress.

2.0 DEVICE DESCRIPTION

2.1 Hardware Architecture

Four major functional blocks make up the LM628/629 in addition to the host and output interfaces. These are the Trajectory Profile Generator, Loop Compensating PID Filter, Summing Junction and Motor Position Decoder *(Figure 1).*

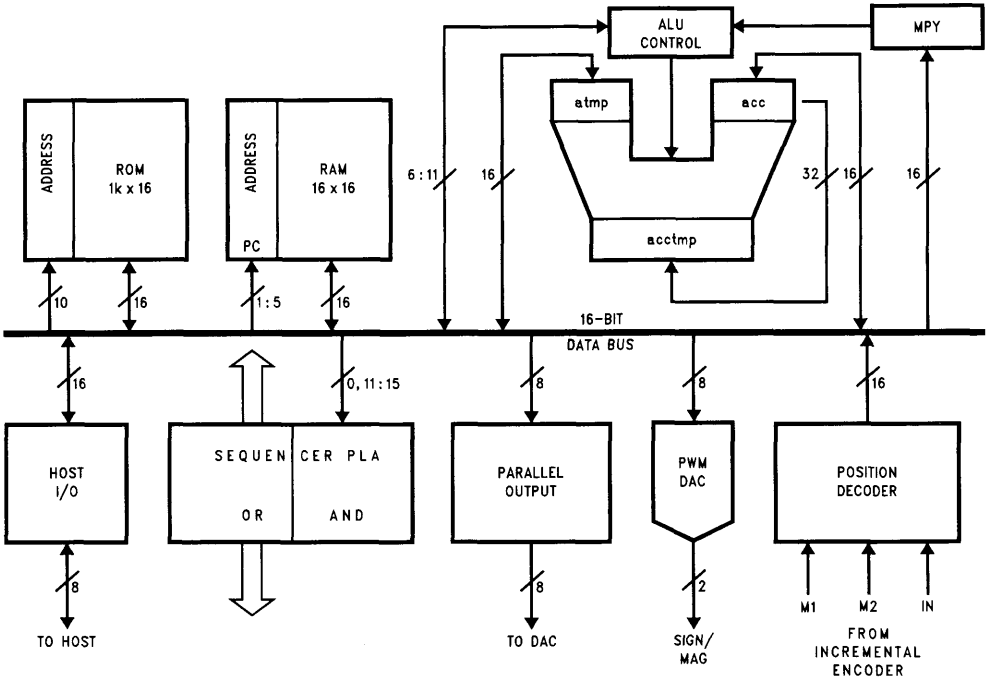

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FIGURE 2. Hardware Architecture of LM628/629

Details of how LM628/629 is implemented by a purpose designed microcontroller are shown in *Figure 2.* The control algorithm is stored in a 1k x 16-bit ROM and uses 16-bit wide instructions. A PLA decodes these instructions and provides data transfer timing signals for the single 16-bit data and instruction bus. User variable filter and trajectory profile parameters are stored as 32-bit double words in RAM. To provide sufficient dynamic range a 32-bit position register is used and for consistency. 32 bits are also used for velocity and acceleration values. A 32-bit ALU is used to support the 16 x 16-bit multiplications of the error and PID digital filter coefficients.

2.2 Motor Position Decoder

LM628/629 provides an interface for an optical position shaft encoder, decoding the two quadrature output signals to provide position and direction information, *Figure 3.* Optionally a third index position output signal can be used to capture position once per revolution. Each of the four states of the quadrature position signal are decoded by the LM628/629 giving a 4 times increase in position resolution over the number of encoder lines. An "N" line encoder will be decoded as "4N" position counts by LM628/629.

Position decoder block diagram, *Figure 4,* shows three lines coming from the shaft encoder, M1, M2 and Index. From these the decoder PLA determines if the motor has moved forward, backward or stayed still and then drives a 16-bit up-down counter that keeps track of actual motor position. Once per revolution when all three lines including the index line are simultaneously low, *Figure 3,* the current position count is captured in an index latch.

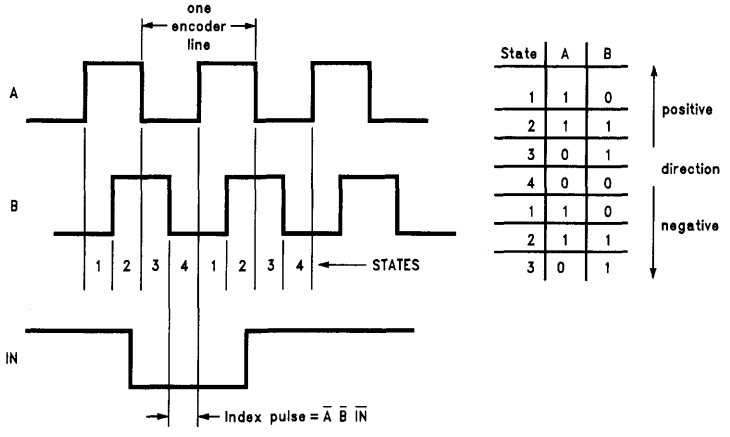

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FIGURE 3. Quadrature Encoder Output Signals and Direction Decode Table

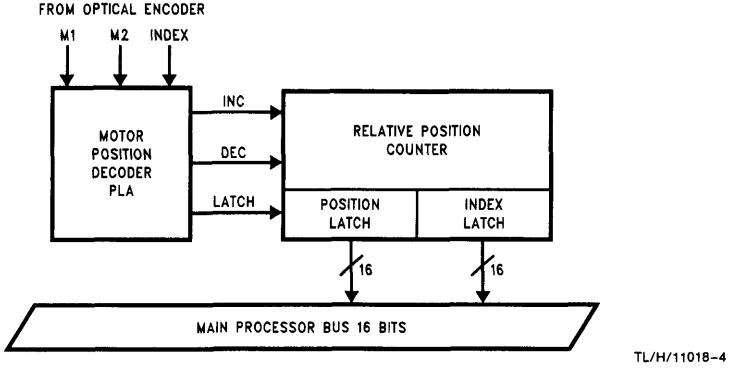

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FIGURE 4. LM628/629 Motor Position Decoder

The 16-bit up-down counter is used to capture the difference in position from one sample to the next. A position latch attached to the up-down counter is strobed at the same time in every sample period by a sync pulse that is generated in hardware. The position latch is read soon after the sync pulse and is added to the 32-bit position register in RAM that holds the actual current position. This is the value that is subtracted in the summing junction every sample interval from the new desired position calculated by the trajectory generator to form the error input to the PID filter.

Maximum encoder state capture rate is determined by the minimum number of clock cycles it takes to decode each encoder state, see *Figure 3,* this minimum number is 8 clock cycles, capture of the index pulse is also achieved during these 8 clock cycles. This gives a more than adequate 1 MHz maximum encoder state capture rate with the 8 MHz f_{CLK} devices (750 kHz for the 6 MHz f_{CLK} devices). For example, with the 1 MHz capture rate, a motor using a 500 line encoder will be moving at 30,000 rpm.

There is some limited signal conditioning at the decoder input to remove problems that would occur due to the asynchronous position encoder input being sampled on signal edges by the synchronous LM628/629. But there is no noise filtering as such on the encoder lines so it is important that they are kept clean and away from noise sources.

2.3 Trajectory Profile Generator

Desired position inputs to the summing junction, *Figure 1,* within the LM628/629 are provided by an internal independent trajectory profile generator. The trajectory profile generator takes information from the host and computes for each sample interval a new current desired position. The information required from the host is, operating mode, either position or velocity, target acceleration, target velocity and target position in position mode.

2.4 Definitions Relating to Profile Generation

The units of position and time, used by the LM628/629, are counts (4 × N encoder lines) and samples (sample intervals = $2048/f_{CLK}$) respectively. Velocity is therefore calculated in counts/sample and acceleration in counts/sample/sample.

Definitions of "target", "desired" and "actual" within the profile generation activity as they apply to velocity, acceleration and position are as follows. Final requested values are called "target", such as target position. The values computed by the profile generator each sample interval on the way to the target value are called "desired". Real values from the position encoder are called "actual".

For example, the current actual position of the motor will typically be a few counts away from the current desired position because a new value for desired position is calculated every sample interval during profile generation. The difference between the current desired position and current actual position relies on the ability of the control loop to keep the motor on track. In the extreme example of a locked rotor there could be a large difference between the current actual and desired positions.

Current desired velocity refers to a fixed velocity at any point on a on-going trajectory profile. While the profile demands acceleration, from zero to the target velocity, the velocity will incrementally increase at each sample interval.

Current actual velocity is determined by taking the difference in the actual position at the current and the previous sample intervals. At velocities of many counts per sample this is reasonably accurate, at low velocities, especially below one count per sample, it is very inaccurate.

2.5 Profile Generation

Trajectory profiles are plotted in terms of velocity versus time, *Figure 5,* and are velocity profiles by reason that a new desired position is calculated every sample interval. For constant velocity these desired position increments will be the same every sample interval, for acceleration and deceleration the desired position increments will respectively increase and decrease per sample interval. Target position is the integral of the velocity profile.

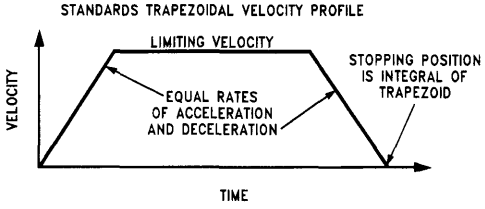

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FIGURE 5. Typical Trajectory Velocity Profile

When performing a move the LM628/629 uses the information as specified by the host and accelerates until the target velocity is reached. While doing this it takes note of the number of counts taken to reach the target velocity. This number of counts is subtracted from the target position to determine where deceleration should commence to ensure the motor stops at the target position. LM628/629 deceleration rates are equal to the acceleration rates. In some cases, depending on the relative target values of velocity, acceleration and position, the target velocity will not be reached and deceleration will commence immediately from acceleration.

2.6 Trajectory Resolution

The resolution the motor sees for position is one integral count. The algorithm used to calculate the trajectory adds the velocity to the current desired position once per sample period and produces the next desired position point. In order to allow very low velocities it is necessary to have velocities of fractional counts per sample. The LM628/629 in addition to the 32-bit position range keeps track of 16 bits of fractional position. The need for fractional velocity counts can be illustrated by the following example using a 500 line (2000 count) encoder and an 8 MHz clock LM628/629 giving a 256 μs sample interval. If the smallest resolution is 1 count per sample then the minimum velocity would be 2 revolutions per second or 120 rpm. (1/2000 revs/count $\times$ 1/256 μs counts/second). Many applications require velocities and steps in velocity less than this amount. This is provided by the fractional counts of acceleration and velocity.

2.7 Position, Velocity and Acceleration Resolution

Every sample cycle, while the profile demands acceleration, the acceleration register is added to the velocity register which in turn is added to the position register. When the demand for increasing acceleration stops, only velocity is added to the position register. Only integer values are output from the position register to the summing junction and so fractional position counts must accumulate over many sample intervals before an integer count is added and the position register changed. *Figure 6* shows the position, velocity and acceleration registers.

The position dynamic range is derived from the 32 bits of the integer position register, *Figure 6*. The MSB is used for the direction sign in the conventional manner, the next bit 30 is used to signify when a position overflow called "wraparound" has occurred. If the wraparound bit is set (or reset when going in a negative direction) while in operation the status byte bit 4 is set and optionally can be used to interrupt the host. The remaining 30 bits provide the available dynamic range of position in either the positive or negative direction ($\pm$1,073,741,824 counts).

Velocity has a resolution of $1/2^{16}$ counts/sample and acceleration has a resolution of $1/2^{16}$ counts/sample/sample as mentioned above. The dynamic range is 30 bits in both cases. The loss of one bit is due to velocity and acceleration being unsigned and another bit is used to detect wraparound. This leaves 14 bits or 16,383 integral counts and 16 bits for fractional counts.

2.8 Velocity Mode

LM628 supports a velocity mode where the motor is commanded to continue at a specified velocity, until it is told to

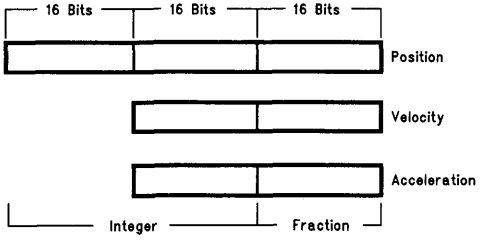

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FIGURE 6. Position, Velocity and Acceleration Registers

stop (LTRJ bits 9 or 10). The average velocity will be as specified but the instantaneous velocity will vary. Velocities of fractional counts per sample will exhibit the poorest instantaneous velocity. Velocity mode is a subset of position mode where the position is continually updated and moved ahead of the motor without a specified stop position. Care should be exercised in the case where a rotor becomes locked while in velocity mode as the profile generator will continue to advance the position. When the rotor becomes free high velocities will be attained to catch-up with the current desired position.

2.9 Motor Output Port

LM628 output port is configured to 8 bits after reset. The 8-bit output is updated once per sample interval and held until it is updated during the next sample interval. This allows use of a DAC without a latch. For 12-bit operation the PORT12 command should be issued immediately after reset. The output is multiplexed in two 6-bit words using pins 18 through 23. Pin 24 is low for the least significant word and high for the most significant. The rising edge of the active low strobe from pin 25 should be used to strobe the output into an external latch, see *Figure 7.* The DAC output is offset binary code, the zero codes are hex'80' for 8 bits and hex'800' for 12 bits.

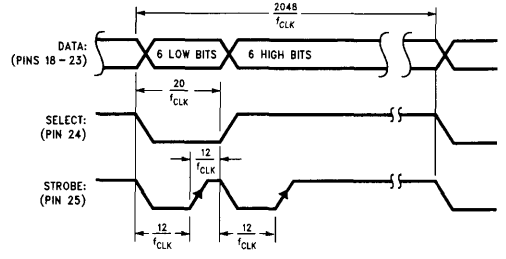

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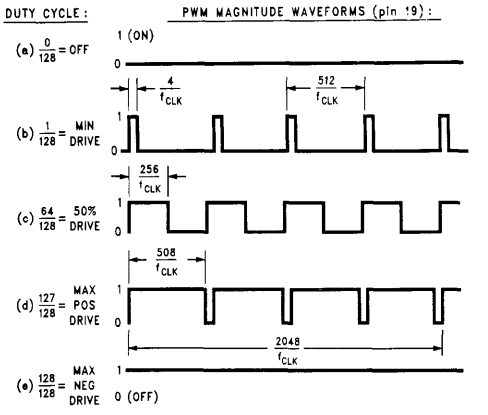
FIGURE 7. LM628 12-Bit DAC Output Multiplexed Timing

The choice of output resolution is dependant on the user's application. There is a fundamental trade-off between sampling rate and DAC output resolution, the LM628 8-bit output at a 256 μs sampling interval will most often provide as good results as a slower, e.g. microcontroller, implementation which has a 4 ms typical sampling interval and uses a 12-bit output. The LM628 also gives the choice of a 12-bit DAC output at a 256 μs sampling interval for high precision applications.

LM629 PWM sign and magnitude signals are output from pins 18 and 19 respectively. The sign output is used to control motor direction. The PWM magnitude output has a resolution of 8 bits from maximum negative drive to maximum positive drive. The magnitude output has an off condition, with the output at logic low, which is useful for turning a motor off when using a bridge motor drive circuit. The minimum duty cycle is 1/128 increasing to a maximum of 127/128 in the positive direction and a maximum of 128/128 in the negative direcition, i.e., a continuous output. There are four PWM periods in one LM629 sample interval. With an 8 MHz clock this increases the PWM output rate to 15.6 kHz from the LM629 maximum 3.9 kHz sample rate, see *Figure 8* for further timing information.



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Note: Sign output (pin 18) not shown.

FIGURE 8. LM629 PWM Output Signal Format

2.10 Host Interface

LM628/629 has three internal registers: status, high, and low bytes, *Figure 9,* which are used to communicate with the host microcontroller. These are controlled by the $\overline{RD}$, $\overline{WR}$, and $\overline{PS}$ lines and by use of the busy bit of the status byte. The status byte is read by bringing $\overline{RD}$ and $\overline{PS}$ low, bit 0 is the busy bit. Commands are written by bringing $\overline{WR}$ and $\overline{PS}$ low. When $\overline{PS}$ is high, $\overline{WR}$ brought low writes data into LM628/629 and similarly, $\overline{RD}$ is brought low to read data from LM628/629. Data transfer is a two-byte operation written in most to least significant byte order. The above description assumes that $\overline{CS}$ is low.

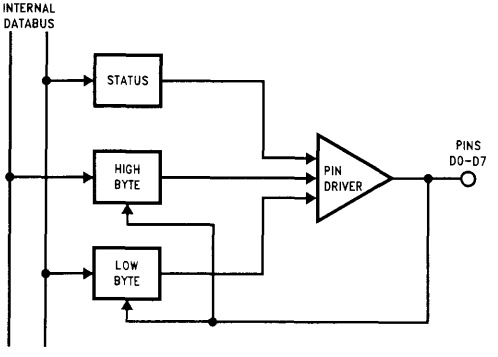

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FIGURE 9. Host Interface Internal I/O Registers

2.11 Hardware Busy Bit Operation

Before and between all command byte and data byte pair transfers, the busy bit must be read and checked to be at logic low. If the busy bit is set and commands are issued they will be ignored and if data is read it will be the current contents of the I/O buffer and not the expected data. The busy bit is set after the rising edge of the write signal for commands and the second rising edge of the respective read or write signal for two byte data transfers, *Figure 10.* The busy bit remains high for approximately 15 μs.

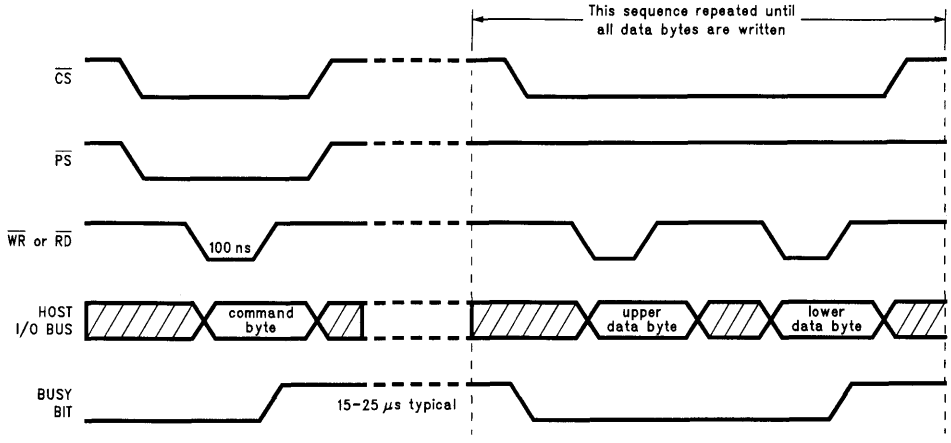

FIGURE 10. Busy Bit Operation during Command and Data Write Sequence

The busy bit reset to logic low indicates that high and low byte registers shown in *Figure 9* have been either loaded or read by the LM628/629 internal microcode. To service the command or data transfer this microcode which performs the trajectory and filter calculations is interrupted, except in critical areas, and the on-going calculation is suspended. The microcode was designed this way to achieve minimum latency when communicating with the host. However, if this communication becomes too frequent and on-going calculations are interrupted too often corruption will occur. In a 256 μs sample interval, the filter calculation takes 50 μs, outputting a sample 10 μs and trajectory calculation 90 μs. If the LM628 behaves in a manner that is unexpected the host communication rate should be checked in relation to these timings.

2.12 Filter Initial Values and Tuning

When connecting up a system for the first time there may be a possibility that the loop phasing is incorrect. As this may cause violent oscillation it is advisable to initially use a very low value of proportional gain, say $k_p = 1$ (with k_d, k_i and il all set to zero), which will provide a weak level of drive to the motor. (The Start command, STT, is sent to LM628/629 to close the control loop and energize the motor.) If the system does oscillate with this low value of k_p then the motor connections should be reversed.

Having determined that the loop phasing is correct k_p can be increased to a value of about 20 to see that the control system basically works. This value of k_p should hold the motor shaft reasonably stiffly, returning the motor to the set position, which will be zero until trajectory values have been input and a position move performed. If oscillation or unacceptable ringing occurs with a k_p value of 20 reduce this until it stops. Low values of acceleration and velocity can now be input, of around 100, and a position move commanded to say 1000 counts. All values suggested here are decimal. For details of loading trajectory and filter parameters see Section 3.0, reference (5) and the data sheet.

It is useful at this stage to try different values of acceleration and velocity to get a feel for the system limitations. These can be determined by using the reporting commands of desired and actual position and velocity, to see if the error between desired and actual positions of the motor are constant and not increasing without bound. See Section 3.6 and the data sheet for information about the reporting commands. Clearly it will be difficult to tune for best system response if the motor and its load cannot achieve the demanded values of acceleration and velocity. When correct operation is confirmed and limiting values understood, filter tuning can commence.

Due to the basic difficulty of accurately modeling a control system, with the added problem of variations that can occur in mechanical components over time and temperature, it is always necessary at some stage to perform tuning empirically. Determining the PID filter coefficients by tuning is the preferred method with LM628/629 because of the inherent flexibility in changing the filter coefficients provided by this programmable device.

Before tuning a control system the effect of each of the PID filter coefficients should be understood. The following is a very brief review, for a detailed understanding reference (2) should be consulted. The proportional coefficient, k_p, provides adjustment of the control system loop proportional gain, as this is increased the output steady state error is reduced. The error between the required and actual position is effectively divided by the loop gain. However there is a natural limitation on how far k_p can be increased on its own to reduce output position error because a reduction in phase margin is also a consequence of increasing k_p. This is first encountered as ringing about the final position in response to a step change input and then instability in the form of oscillation as the phase margin becomes zero. To improve stability, k_d, the derivative coefficient, provides a damping effect by providing a term proportional to velocity in antiphase to the ringing, or viewed in another way, adds some leading phase shift into the loop and increases the phase margin.

In the tuning process the coefficients k_p and k_d are iteratively increased to their optimum values constrained by the system constants and are trade-offs between response time, stability and final position error. When k_p and k_d have been determined the integral coefficient, k_i, can be introduced to remove steady state errors at the load. The steady state

errors removed are the velocity lag that occurs with a constant velocity output and the position error due to a constant static torque. A value of integration limit, il, has to be input with k_i, otherwise k_i will have no effect. The integral coefficient k_i adds another variable to the system to allow further optimization, very high values of k_i will decrease the phase margin and hence stability, see Section 5 and reference (2) for more details. Reference (5) gives more details of PID filter tuning and how to load filter parameters.

Figure 11 illustrates how a relatively slow response with overshoot can be compensated by adjustment of the PID filter coefficients to give a faster critically damped response.

3.0 USER COMMAND SET

3.1 Overview

The following types of User Commands are available:

Initialization
Filter control commands
Trajectory control commands
Interrupt control commands
Data reporting commands

User commands are single bytes and have a varying number of accompanying data bytes ranging from zero to fourteen depending upon the command. Both filter and trajectory control commands use a double buffered scheme to input data. These commands load primary registers with multiple words of data which are only transferred into secondary working registers when the host issues a respective single byte user command. This allows data to be input before its actual use which can eliminate any potential communication bottlenecks and allow synchronized operation of multiple axes.

3.2 Host-LM628/629 Communication—The Busy Bit

Communication flow between the LM628/629 and its host is controlled by using a busy bit, bit 0, in the Status Byte. The busy bit must be checked to be at logic 0 by the host before commands and data are issued or data is read. This includes between data byte pairs for commands with multiple words of data.

3.3 Loading the Trapezoidal Velocity Profile Generator

To initiate a motor move, trajectory generator values have to be input to the LM628/629 using the Load Trajectory Parameters, LTRJ, command. The command is followed by a trajectory control word which details the information to be loaded in subsequent data words. Table I gives the bit allocations, a bit is set to logic 1 to give the function shown.

TABLE I. Trajectory Control Word Bit Allocations

Bit Position	Function
Bit 15	Not Used
Bit 14	Not Used
Bit 13	Not Used
Bit 12	Forward Direction (Velocity Mode Only)
Bit 11	Velocity Mode
Bit 10	Stop Smoothly (Decelerate as Programmed)
Bit 9	Stop Abruptly (Maximum Deceleration)
Bit 8	Turn Off Motor (Output Zero Drive)
Bit 7	Not Used
Bit 6	Not Used
Bit 5	Acceleration Will Be Loaded
Bit 4	Acceleration Data Is Relative
Bit 3	Velocity Will Be Loaded
Bit 2	Velocity Data Is Relative
Bit 1	Position Will Be Loaded
Bit 0	Position Data Is Relative

Bits 0 to 5 determine whether any, all or none of the position, velocity or acceleration values are loaded and whether they are absolute values or values relative to those previously loaded. All trajectory values are 32-bit values, position values are both positive and negative. Velocity and acceleration are 16-bit integers with 16-bit fractions whose absolute value is always positive. When entering relative values ensure that the absolute value remains positive. The manual stop commands bits 8, 9 and 10 are intended to allow an unprogrammed stop in position mode, while a position move is in progress, perhaps by the demand of some external event, and to provide a method to stop in velocity mode. They do not specify how the motor will stop in position mode at the end of a normal position move. In position mode a programmed move will automatically stop with a deceleration rate equal to the acceleration rate at the target position. Setting a stop bit along with other trajectory parameters at the beginning of a move will result in no movement! Bits 8, 9 and 10 should only be set one at a time, bit 8 turns the motor off by outputting zero drive to the motor, bit 9 stops the motor at maximum deceleration by setting the target position equal to the current position and bit 10 stops the motor using the current user-programmed acceleration value. Bit 11 is set for operating in velocity mode and bit 12 is set for forward direction in velocity mode.

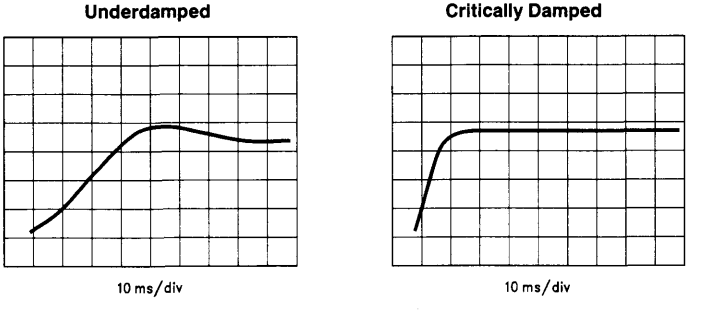

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FIGURE 11. Position vs Time for 100 Count Step Input

Following immediately after the trajectory control word should be two 16-bit data words for each parameter specified to be loaded. These should be in the descending order of the trajectory control word bits, that is acceleration, velocity and position. They are written to the LM628/629 as two pairs of data bytes in most to least significant byte order. The busy bit should be checked between the command byte and the data byte pair forming the trajectory control word and the individual data byte pairs of the data. The Start command, STT, transfers the loaded trajectory data into the working registers of the double buffered scheme to initiate movement of the motor. This buffering allows any parameter, except acceleration, to be updated while the motor is moving by loading data with the LTRJ command and to be later executed by using the STT command.

New values of acceleration can be loaded with LTRJ while the motor is moving, but cannot be executed by the STT command until the trajectory has completed or the drive to the motor is turned off by using bit 8 of the trajectory control word. If acceleration has been changed and STT is issued while the drive to the motor is still present, a command error interrupt will be generated and the command ignored. Separate pairs of LTRJ and STT commands should be issued to first turn the motor off and then update acceleration. System operation when changing acceleration while the motor is moving, but with the drive removed, is discussed in Section 4.5.1.

3.4 Loading PID Filter Coefficients

PID filter coefficients are loaded using the Load Filter Parameters, LFIL, command and are the proportional coefficient k_p, derivative coefficient k_d and integral coefficient k_i. Associated with k_i, an integration limit, il, has to be loaded. This constrains the magnitude of the integration term of the PID filter to the il value, see Section 4.4.2. Associated with the derivative coefficient, a derivative sample rate can be chosen from $2048/f_{CLK}$ to $(2048 \times 256)/f_{CLK}$ in steps of $2048/f_{CLK}$, see Section 4.4.1.

The first pair of data bytes following the LFIL command byte form the filter control word. The most significant byte sets the derivative sample rate, the fastest rate, $2048/f_{CLK}$, being hex'00' the slowest rate $(2048 \times 256)/f_{CLK}$ being hex'FF'. The lower four bits of the least significant byte tell the LM628/629 which of the coefficients is going to be loaded, bit 3 is k_p, bit 2 is k_i, bit 1 is k_d and bit 0 is il. Each filter coefficient and the integration limit can range in value from hex'0000' to '7FFF', positive only. If all coefficient values are loaded then ten bytes of data, including the filter control word, will follow the LFIL command. Again the busy bit has to be checked between the command byte and filter control word and between data byte pairs. Use of new filter coefficient values by the LM628/629 is initiated by issuing the single byte Update Filter command, UDF.

When controlled movement of the motor has been achieved, by programming the filter and trajectory, attention turns to incorporating the LM628/629 into a system. Interrupt Control Commands and Data Reporting Commands enable the host microcontroller to keep track of LM628/629 activity.

3.5 Interrupt Control Commands

There are five commands that can be used to interrupt the host microcontroller when a predefined condition occurs and two commands that control interrupt operation. When the LM628/629 is programmed to interrupt its host, the event which caused this interrupt can be determined from bits 1 to 6 of the Status Byte (additionally bit 0 is the busy bit and bit 7 indicates that the motor is off). All the Interrupt Control commands are executable during motion.

The Mask Interrupts command, MSKI, is used to tell LM628/629 which of bits 1 to 6 will interrupt the host through use of interrupt mask data associated with the command. The data is in the form of a data byte pair, bits 1–6 of the least significant byte being set to logic 1 when an interrupt source is enabled. The Reset Interrupts command, $\overline{RSTI}$, resets interrupt bits in the Status Byte by sending a data byte pair, the least significant byte having logic 0 in bit positions 1 to 6 if they are to be reset.

Executing the Set Index Position command, SIP, causes bit 3 of the status byte to be set when the absolute position of the next index pulse is recorded in the index register. This can be read with the command, Read Index Position, RDIP.

Executing either Load Position Error for Interrupt, LPEI, or Load Position Error for Stopping, LPES, commands, sets bit 5 of the Status Byte when a position error exceeding a specified limit occurs. An excessive position error can indicate a serious system problem and these two commands give the option when this occurs of either interrupting the host or stopping the motor and interrupting the host. The excessive position is specified following each command by a data byte pair in most to least significant byte order.

Executing either Set Break Point Absolute, SBPA, or Set Break Point Relative, SBPR, commands, sets bit 6 of the status byte when either the specified, absolute or relative, breakpoint respectively is reached. The data for SBPA can be the full position range (hex'C0000000' to '3FFFFFFF') and is sent in two data byte pairs in most to least significant byte order. The data for the Set Breakpoint Relative command is also of two data byte pairs, but its value should be such that when added to the target position it remains within the absolute position range. These commands can be used to signal the moment to update the on-going trajectory or filter coefficients. This is achieved by transferring data from the primary registers, previously loaded using LTRJ or LFIL, to working registers, using the STT or UDF commands.

Interrupt bits 1, 2 and 4 of the Status Byte are not set by executing interrupt commands but by events occurring during LM628/629 operation as follows. Bit 1 is the command error interrupt, bit 2 is the trajectory complete interrupt and bit 4 is the wraparound interrupt. These bits are also masked and reset by the MSKI and $\overline{RSTI}$ commands respectively. The Status Byte still indicates the condition of interrupt bits 1–6 when they are masked from interrupting the host, allowing them to be incorporated in a polling scheme.

3.6 Data Reporting Commands

Read Status Byte, RDSTAT, supported by a hardware register accessed via $\overline{CS}$, $\overline{RD}$ and $\overline{PS}$ control, is the most frequently used method of determining LM628/629 status. This is primarily to read the busy bit 0 while communicating commands and data as described in Section 3.2.

There are seven other user commands which can read data from LM628/629 data registers.

The Read Signals Register command, RDSIGS, returns a 16-bit data word to the host. The least-significant byte repeats the RDSTAT byte except for bit 0 which indicates that a SIP command has been executed but that an index pulse has not occurred. The most significant byte has 6 bits that indicate set-up conditions (bits 8, 9, 11, 12, 13 and 14). The other two bits of the RDSIGS data word indicate that the trajectory generator has completed its function, bit 10, and that the host interrupt output (Pin 17) has been set to logic 1, bit 15. Full details of the bit assignments of this command can be found in the data sheet.

The Read Index Position, RDIP, command reads the position recorded in the 32 bits of the index register in four data bytes. This command, with the SIP command, can be used to acquire a home position or successive values. These could be used, for example, for gross error checking.

Both on-going 32-bit position inputs to the summing junction can be read. Read desired position, RDDP, reads the current desired position the demand or "set point input" from the trajectory generator and Read Real Position, RDRP, reads the current actual position of the motor.

Read Desired Velocity, RDDV, reads the current desired velocity used to calculate the desired position profile by the trajectory generator. It is a 32-bit value containing integer and fractional velocity information. Read Real Velocity, RDRV, reads the instantaneous actual velocity and is a 16-bit integer value.

Read Integration-Term Summation Value, RDSUM, reads the accumulated value of the integration term. This is a 16-bit value ranging from zero to the current, il, integration limit value.

3.7 Software Example

The following example shows the flow of microcontroller commands needed to get the LM628/629 to control a simple motor move. As it is non-specific to any microcontroller pseudo commands $\overline{WR}$,XXXXH and RD,XXXXH with hex immediate data will be used to indicate read and write operations respectively by the host to and from the LM628/629. Decisions use IF..THEN..ELSE. BUSY is a user routine to check the busy bit in the Status Byte, WAIT is a user routine to wait 1.5 ms after hardware reset.

```
LABEL     MNEMONIC        :REMARK
Initialization:
          WAIT            :Routine to wait 1.5 ms after reset.
          RDSTAT          :Check correct RESET operation by reading the
                          :Status Byte. This should be either hex'84' or 'C4'
          IF Status byte not equal hex'84' or 'C4' THEN repeat
          hardware RESET
                          :Make decision concerning validity of RESET
```

Optionally the Reset can be further checked for correct operation as follows. It is useful to include this to reset all interrupt bits in the Status Byte before further action:

```
          MSKI            :Mask interrupts
          BUSY            :Check busy bit 0 routine
          WR,0000H        :Host writes two zero bytes of data to
                          :LM628/629. This mask disables all interrupts.
          BUSY            :Check busy bit
          RSTI            :Reset Interrupts command
          BUSY            :Check busy bit
          WR,0000H        :Host writes two zero bytes of data to LM628/629
          RDSTAT          :Status byte should read either hex'80' or 'C0'
          IF Status byte not equal hex'80' or 'C0' THEN repeat
          hardware RESET
                          :
          IF Status Byte equal to hex'C0' THEN continue ELSE PORT
                          :
          BUSY            :Check busy bit
          RSTI            :Reset Interrupts
          BUSY            :Check busy bit
          WR,0000H        :Reset all interrupt bits
Set Output Port Size for a 12-bit DAC.
PORT      BUSY            :Check busy bit
          PORT12          :Sets LM628 output port to 12-bits
                           (Only for systems with 12-bit DAC)
```

```
Load Filter Parameters
        BUSY            :Check busy bit
        LFIL            :Load Filter Parameters command
        BUSY            :Check busy bit
        WR,0008H        :Filter Control Word
                        :    Bits 8 to 15 (MSB) set the derivative
                        :sample rate.
                        :    Bit 3    Loading kp data
                        :    Bit 2    Loading ki data
                        :    Bit 1    Loading kd data
                        :    Bit 0    Loading il data
                        :Choose to load kp only at maximum
                        :derivative sample rate then Filter Control
                        :Word = 0008H
        BUSY            :Check busy bit
        WR,0032H        :Choose kp = 50, load data byte pair MS
                        :byte first
Update Filter
        BUSY            :Check busy bit
        UDF             :
Load Trajectory Parameters
        BUSY            :Check busy bit
        LTRJ            :Load trajectory parameters command.
        BUSY            :Check busy bit
        WR,002AH        :Load trajectory control word:
                        :    See Table I
                        :Choose Position mode, and load absolute
                        :acceleration, velocity and position. Then
                        :trajectory control word = 002AH. This means
                        :6 pairs of data bytes should follow.
        BUSY            :Check busy bit
        WR,XXXXH        :Load Acceleration integer word MS byte first
        BUSY            :Check busy bit
        WR,XXXXH        :Load Acceleration fractional word MS byte first
        BUSY            :Check busy bit
        WR,XXXXH        :Load Velocity integer word MS byte first
        BUSY            :Check busy bit
        WR,XXXXH        :Load Velocity fractional word MS byte first
        BUSY            :Check busy bit
        WR,XXXXH        :Load Position MS byte pair first
        BUSY            :Check busy bit
        WR,XXXXH        :Load position LS byte pair
Start Motion
        BUSY            :Check busy bit
        STT             :Start command
Check for Trajectory complete.
        RDSTAT          :Check Status Byte bit 2 for trajectory
                        :complete
Busy bit check routine
BUSY    RDSTAT          :Read status byte
        If bit 0 is set THEN BUSY ELSE RETURN
        END
```

*Consult reference (5) for more information on programming the LM628/629.

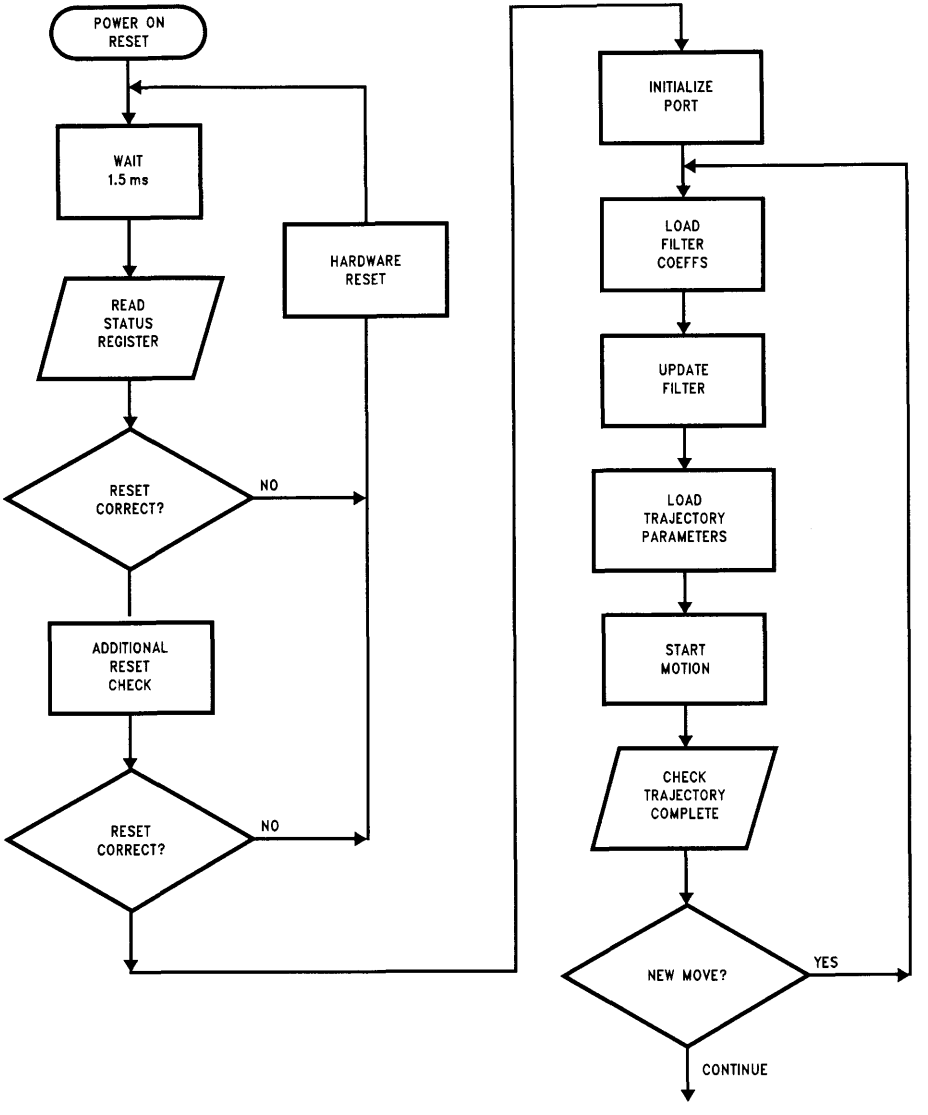

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FIGURE 12. Basic Software Flow

4.0 HELPFUL USER IDEAS

4.1 Getting Started

This section outlines the actions that are necessary to implement a simple motion control system using LM628/629. More details on how LM628/629 works and the use of the User Command Set are given in the sections "2.0 DEVICE DESCRIPTION" and "3.0 USER COMMAND SET".

4.2 Hardware

The following hardware connections need to be made:

4.2.1 Host Microcontroller Interface

Interface to the host microcontroller is via an 8-bit command/data port which is controlled by four lines. These are the conventional chip select $\overline{CS}$, read $\overline{RD}$, write $\overline{WR}$ and a line called Port Select $\overline{PS}$, see *Figure 13.* $\overline{PS}$ is used to select user Command or Data transfer between the LM628/629 and the host. In the special case of the Status Byte (RDSTAT) bringing $\overline{PS}$, $\overline{CS}$ and $\overline{RD}$ low together allows access to this hardware register at any time. An optional interrupt line, HI, from the LM628/629 to the host can be used. A microcontroller output line is necessary to control the LM628/629 hardware reset action.

4.2.2 Position Encoder Interface

The two optical incremental position encoder outputs feed into the LM628/629 quadrature decoder TTL inputs A and B. The leading phase of the quadrature encoder output defines the forward direction of the motor and should be connected to input A. Optionally an index pulse may be used from the position encoder. This is connected to the $\overline{IN}$ input, which should be tied high if not used, see *Figure 13.*

4.2.3 Output Interface

LM628 has a parallel output of either 8 or 12 bits, the latter is output as two multiplexed 6-bit words. *Figure 14* illustrates how a motor might be driven using a LM12 power linear amplifier from the output of 8-bit DAC0800.

LM629 has a sign and magnitude PWM output, *Figure 13,* of 7-bit resolution plus sign. *Figure 15* shows how the LM629 sign and magnitude outputs can be used to control the outputs of an LM18293 quad half-H driver. The half-H drivers are used in pairs, by using 100 mΩ current sharing resistors, and form a full-H bridge driver of 2A output. The sign bit is used to steer the PWM LM629 magnitude output to either side of the H-bridge lower output transistors while holding the upper transistors on the opposite side of the H-bridge continuously on.

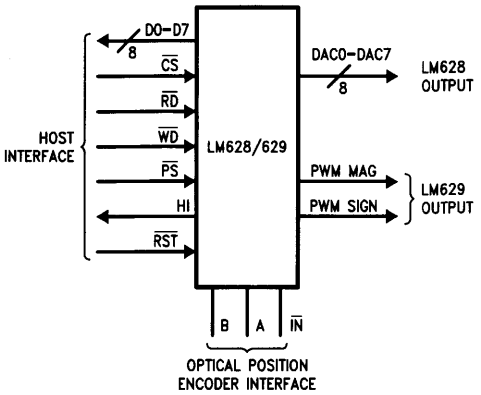

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FIGURE 13. LM628 and LM629 Host, Output and Position Encoder Interfaces

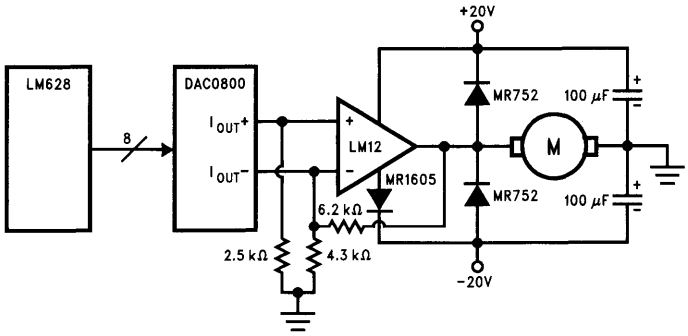

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FIGURE 14. LM628 Example of Linear Motor Drive Using LM12

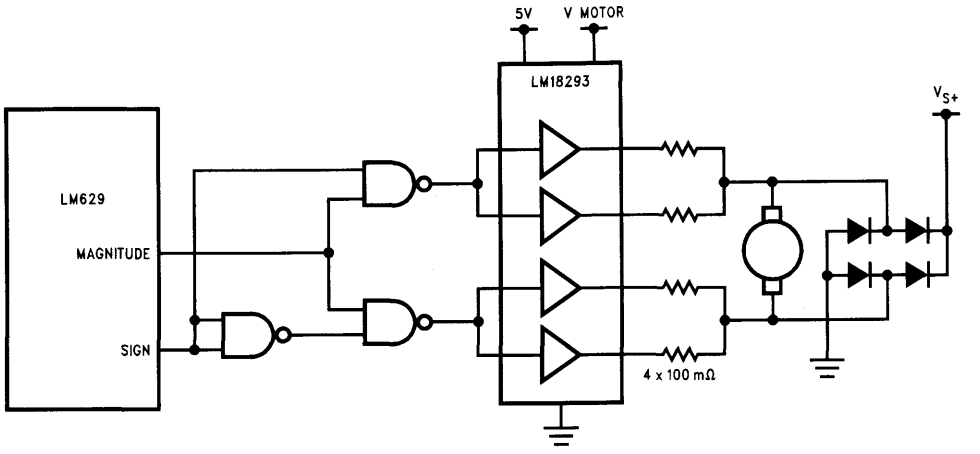

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FIGURE 15. LM629 H-Bridge Motor Drive Example Using LM18293

4.3 Software

Making LM628/629 perform a motion control function requires that the host microcontroller, after initializing LM628/629, loads coefficients for the PID filter and then loads trajectory information. The interrupt and data reporting commands can then be used by the host to keep track of LM628/629 actions. For detailed descriptions see the LM628/629 data sheet and Section 3.

4.4 Initialization

There is only one initialization operation that must be performed; a check that hardware reset has operated correctly. If required, the size of the LM628 output port should be configured. Other operations which might be part of user's system initialization are discussed under Interrupt and Data Reporting commands, Sections 3.5 and 3.6.

4.4.1 Hardware RESET Check

The hardware reset is activated by a logic low pulse at pin 27, $\overline{RST}$, from the host of greater than 8 clock cycles. To ensure that this reset has operated correctly the Status Byte should be checked immediately after the reset pin goes high, it should read hex'00'. If the reset is successful this will change to hex'84' or 'C4' within 1.5 ms. If not, the hardware reset and check should be repeated. A further check can be used to make certain that a reset has been successful by using the Reset Interrupts command, RSTI. Before sending the RSTI, issue the Mask Interrupts command, MSKI, and mask data that disables all interrupts, this mask is sent as two bytes of data equaling hex'0000'. Then issue the RSTI command plus mask data that resets all interrupts, this equals hex'0000' and is again sent as two bytes. Do not forget to check the busy bit between the command byte and data byte pairs. When the chip has reset properly the status byte will change from hex'84' or 'C4' to hex'80' or 'C0'.

4.4.2 Initializing LM628 Output Port

Reset sets the LM628 output port size to 8 bits. If a 12-bit DAC is being used, then the output port size is set by the use of the PORT12 command.

4.4.3 Interrupt Commands

Optionally the commands which cause the LM628/629 to take action on a predefined condition (e.g., SIP, LPEI, LPES, SBPA and SBPR) can be included in the initialization, these are discussed under Interrupt Commands.

4.5 Performance Refinements

4.5.1 Derivative Sample Rate

The derivative sample interval is controllable to improve the stability of low velocity, high inertia loads. At low speeds, when fractional counts for velocity are used, the integer position counts, desired and actual, only change after several sample intervals of the LM628/629 ($2048/f_{CLK}$). This means that for sample intervals between integer count changes the error voltage will not change for successive samples. As the derivative term, k_d, multiplies the difference betweeen the previous and current error values, if the derivative sample interval is the same as the sample interval, several consecutive sample intervals will have zero derivative term and hence no damping contribution. Lengthening the derivative sample interval ensures a more constant derivate term and hence improved stability. Derivative sample interval is loaded with the filter coefficient values as the most significant byte of the LFIL control word everytime the command is used, the host therefore needs to store the current value for re-loading at times of filter coefficient change.

4.5.2 Integral Windup

Along with the integral filter coefficient, k_i, an integration limit, il, has to be input into LM628/629 which allows the user to set the maximum value of the integration term of equation (3), Section 5.2.2. This term is then able to accumulate up to the value of the integration limit and any further increase due to error of the same sign is ignored. Setting the integration limit enables the user to prevent an effect called "Integral Windup". For example, if an LM628/629 attempts to accelerate a motor at a faster rate than it can achieve, a very large integral term will result. When the LM628/629 tries to stop the motor at the target position the large accumulated integral term will dominate the filter and cause the motor to badly overshoot, and thus integral windup has occurred.

4.5.3 Profiles Other Than Trapezoidal

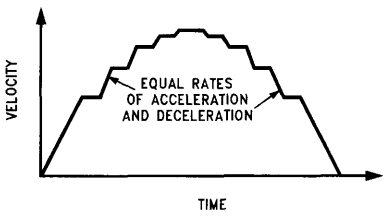

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FIGURE 16. Generating a Non-Trapezoidal Profile

If it is required to have a velocity profile other than trapezoidal, this can be accomplished by breaking the profile into small pieces each of which is part of a small trapezoid. A piecewise linear approximation to the required profile can then be achieved by changing the maximum velocity before the trapezoid has had time to complete, see *Figure 16.*

4.5.4 Synchronizing Axes

For controlling tightly coupled coordinated motion between multiple-axes, synchronization is required. The best possible synchronization that can be achieved between multiple LM628/629 is within one sample interval, ($2048/f_{CLK}$, 256 μs for an 8 MHz clock, 341 μs for a 6 MHz clock). This is achieved by using the pipeline feature of the LM628/629 where all controlled axes are loaded individually with trajectory values using the LTRJ command and then simultaneously given the start command STT. PID filter coefficients can be updated in a similar manner using LFIL and UDF commands.

4.6 Operating Constraints

4.6.1 Updating Acceleration on the Fly

Whereas velocity and target position can be updated while the motor is moving, on the "fly", the algorithm described in Section 2.5 prevents this for acceleration. To change acceleration while the motor is moving in mid-trajectory the motor off command has to be issued by setting LTRJ command bit 8. Then the new acceleration can be loaded, again using the

LTRJ command. When the start command STT is issued the motor will be energized and the trajectory generator will start generating a new profile from the actual position when the STT command was issued. In doing this the trajectory generator will assume that the motor starts from a stationary position in the normal way. If the motor has sufficient inertia and is still moving when the STT command is issued then the control loop will attempt to bring the motor on to the new profile, possibly with a large error value being input to the PID filter and a consequential saturated output until the motor velocity matches the profile. This is a classic case of overload in a feedback system. It will operate in an open loop manner until the error input gets within controllable bounds and then the feedback loop will close. Performance in this situation is unpredictable and application specific. LM628/629 was not intentionally designed to operate in this way.

4.6.2 Command Update Rate

If an LM628/629 is updated too frequently by the host it will not keep up with the commands given. The LM628/629 aborts the current trajectory calculation when it receives a new STT command, resulting in the output staying at the value of the previous sample. For this reason it is recommended that trajectory is not updated at a greater rate than once every 10 ms.

5.0 THEORY

5.1 PID Filter

5.1.1 PID Filter in the Continuous Domain

The LM628/629 uses a PID filter as the loop compensator, the expression for the PID filter in the continuous domain is:

$$H(s) = K_p + K_i/s + K_d s \quad (1)$$

Where K_p = proportional coefficient
K_i = integral coefficient
K_d = derivative coefficient

5.1.2 PID Filter Bode Plots

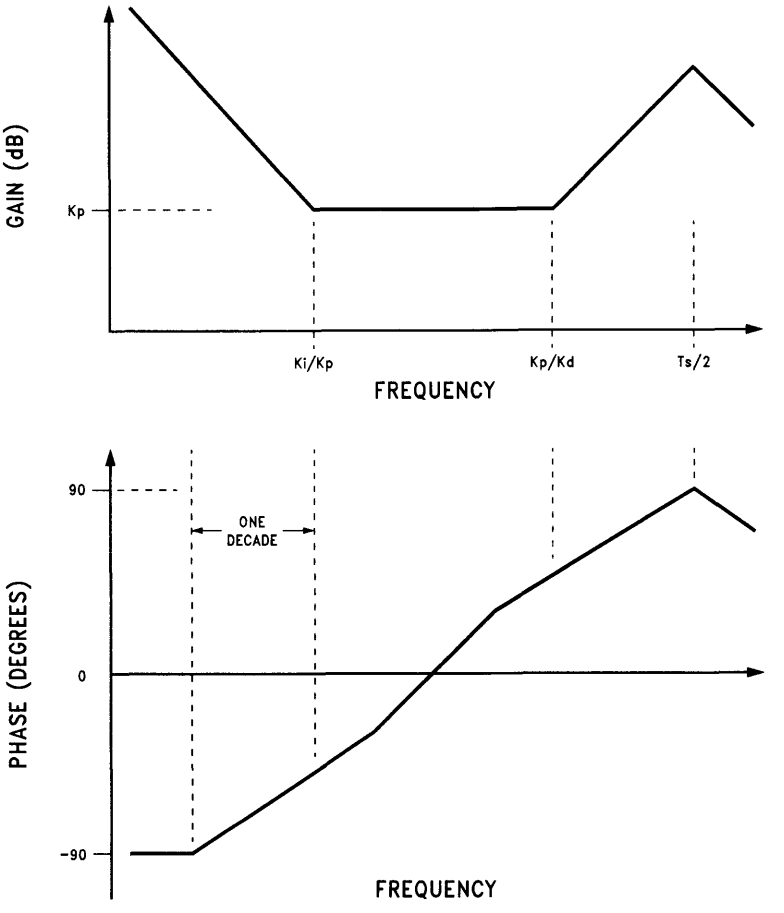

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FIGURE 17. Bode Plots of PID Transfer Function

The Bode plots for this function (shown in *Figure 17*) show the effect of the individual terms of equation (1). The proportional term, K_p provides adjustment of proportional gain. The derivative term K_d increases the system bandwidth but more importantly adds leading phase shift to the control loop at high frequencies. This improves stability by counteracting the lagging phase shift introduced by other control loop components such as the motor. The integral term, K_i, provides a high DC gain which reduces static errors, but introduces a lagging phase shift at low frequencies. The relative magnitudes of K_d, K_i and loop proportional gain have to be adjusted to achieve optimum performance without introducing instability.

5.2 PID Filter Coefficient Scaling Factors for LM628/629

While the easiest way to determine the PID filter coefficient k_p, k_d, and k_i values is to use tuning as described in Section 2.11, some users may want to use a more theoretical approach to at least find initial starting values before fine tuning. As very often this analysis is performed in the continuous (s) domain and transformed into the discrete digital domain for implementation, the relationship between the continuous domain coefficients and the values input into LM628/629 is of interest.

5.2.1 PID Filter Difference Equation

In the discrete domain, equation (1) becomes the difference equation:

$$u(n) = K_p e(n) + K_i T \sum_{n=0}^{N} e(n) + K_d / T_s [e(n) - e(n-1)] \qquad (2)$$

Where:

T is the sample interval $2048/f_{CLK}$

T_s is the derivative sample interval ($2048/f_{CLK} \times (1..255)$

5.2.2 Difference Equation with LM628/629 Coefficients

In terms of LM628/629 coefficients, (2) becomes:

$$u(n) = k_p e(n) + k_i \sum_{n=0}^{N} e(n) + k_d [e(n') - e(n'-0)] \qquad (3)$$

Where:

k_p, k_i and k_d are the discrete-time LM628/629 coefficients

e(n) is the position error at sample time n

n′ indicates sampling at the derivative sampling rate.

The error signal e(n) [or e(n′)] is a 16-bit number from the output of the summing junction and is the input to the PID filter. The 15-bit filter coefficients are respectively multiplied by the 16-bit error terms as shown in equation (3) to produce 32-bit products.

5.2.3 LM628/629 PID Filter Output

The proportional coefficient k_p is multiplied by the error signal directly. The error signal is continually summed at the sample rate to previously accumulated errors to form the integral signal and is maintained to 24 bits. To achieve a more usable range from this term, only the most significant 16 bits are used and multiplied by the integral coefficient, k_i. The absolute value of this product is compared with the integration limit, il, and the smallest value, appropriately signed, is used. To form the derivative signal, the previous error is subtracted from the current error over the derivative sampling interval. This is multiplied by the derivative coefficient k_d and the product contributes every sample interval to the output independently of the user chosen derivative sample interval.

The least significant 16 bits of the 32-bit products from the three terms are added together to produce the resulting u(n) of equation (3) each sample interval. From the PID filter 16-bit result, either the most significant 8 or 12 bits are output, depending on the output word size being used. A consequence of this and the use of the 16 MSB's of the integral signal is a scaling of the filter coefficients in relation to the continuous domain coefficients.

5.2.4 Scaling for k_p and k_d

Figure 18 gives details of the multiplication and output for k_p and k_d. Taking the output from the MS byte of the LS 16 bits of the 32-bit result register causes an effective 8-bit right-shift or division of 256 associated with k_p and k_d as follows:

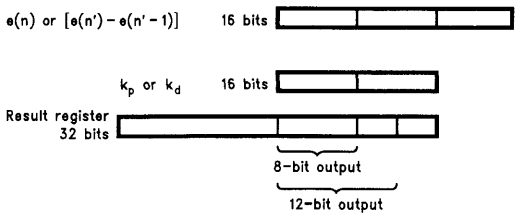

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FIGURE 18. Scaling of k_p and k_d

Result $= k_p \times e(n)/256 = K_p \times e(n)$.'. k_p
$= 256 \times K_p$.

Similarly for k_d:

Result $= (k_d \times [e(n') - e(n'-1)])/256$
$= K_d/T_s \times e(n)$.'. $k_d = 256 \times K_d/T_s$

Where T_s is the derivative sampling rate.

5.2.5 Scaling for k_i

Figure 19 shows the multiplication and output for the integral term k_i. The use of a 24-bit register for the error terms summation gives further scaling:

Result $= k_i/256 \times > e(n)/256$
$= K_i \times T$.'. $k_i = 65536\ K_i \times T$.

Where T is the sampling interval $2048/f_{CLK}$.

For a 12-bit output the factors are:

$k_p = 16 \times K_p$, $k_d = 16 \times K_d/T_s$ and $k_i = 4096\ K_i \times T$.

If the 32-bit result register overflows into the most significant 16-bits as a result of a calculation, then all the lower bits are set high to give a predictable saturated output.

5.3 An Example of a Trajectory Calculation

Problem: Determine the trajectory parameters for a motor move of 500 revolutions in 1 minute with 15 seconds of acceleration and deceleration respectively. Assume the optical incremental encoder used has 500 lines.

The LM628/629 quadrature decoder gives four counts for each encoder line giving 2000 counts per revolution in this example. The total number of counts for this position move is $2000 \times 500 = 1{,}000{,}000$ counts.

By definition, average velocity during the acceleration and deceleration periods, from and to zero, is half the maximum velocity. In this example, half the total time to make the move (30 seconds) is taken by acceleration and deceleration. Thus in terms of time, half the move is made at maximum velocity and half the move at an average velocity of half this maximum. Therefore, the combined distance traveled during acceleration and deceleration is half that during

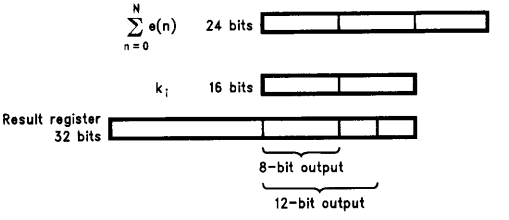

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FIGURE 19. Scaling for k_i

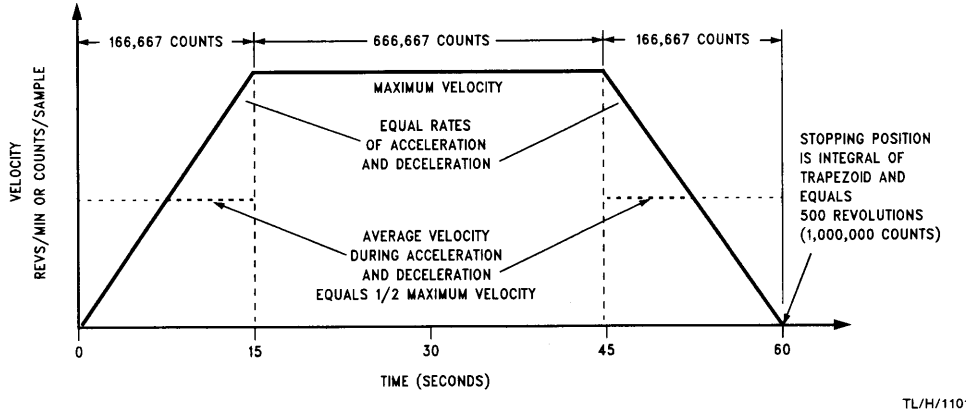

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FIGURE 20. Trajectory Calculation Example Profile

maximum velocity or 1/3 of the total, or 333,333 counts. Acceleration and deceleration takes 166,667 counts respectively.

The time interval used by the LM628/629 is the sample interval which is 256 μs for a f_{CLK} of 8 MHz.

The number of sample periods in 15 seconds = 15s/256 μs = 58,600 samples

Remembering that distance s = $at^2/2$ is traveled due to acceleration 'a' and time 't'.

Therefore acceleration a = $2S/t^2$

$= 2 \times 166{,}667/58{,}600$

$= 97.1 \times 10^{-6}$ counts/sample^2

Acceleration and velocity values are entered into LM628/629 as a 32-bit integer double-word but represents a 16-bit integer plus 16-bit fractional value. To achieve this acceleration and velocity decimal values are scaled by 65536 and any remaining fractions discarded. This value is then converted to hex to enter into LM628 in four bytes.

Scaled acceleration a = $97.1 \times 10^{-6} \times 65536$

= 6.36 decimal = 00000006 hex.

The maximum velocity can be calculated in two ways, either by the distance in counts traveled at maximum velocity divided by the number of samples or by the acceleration multiplied by the number of samples over acceleration duration, as follows:

Velocity = $666{,}667/117{,}200 = 97.1 \times 10^{-6} \times 58{,}600$

= 5.69 counts/sample

Scaled by 65536 becomes 372,899.8 decimal = 0005B0A3 hex.

Inputting these values for acceleration and velocity with the target position of 1,000,000 decimal, 000F4240 hex will achieve the desired velocity profile.

6.0 QUESTIONS AND ANSWERS

6.1 The Two Most Popular Questions

6.1.1 Why doesn't the motor move, I've loaded filter parameters, trajectory parameters and issued Update Filter, UDF, and Start, STT, commands?

Answer: The most like cause is that a stop bit (one of bits 8, 9 or 10 of the trajectory control word) has been set in error, supposedly to cause a stop in position mode. This is unnecessary, in position mode the trajectory stops automatically at the target position, see Section 3.3.

6.1.2 Can acceleration be changed on the fly?

Answer: No, not directly and a command error interrupt will be generated when STT is issued if acceleration has been changed. Acceleration can be changed if the motor is turned off first using bit 8 of the Load Trajectory Parameter, LTRJ, trajectory control word, see Section 4.6.1.

6.2.More on Acceleration Change

6.2.1 What happens at restart if acceleration is changed with the motor drive off and the motor is still moving?

Answer: The trajectory generation starting position is the actual position when the STT command is issued, but assumes that the motor is stationary. If the motor is moving the control loop will attempt to bring the motor back onto an accelerating profile, producing a large error value and less than predictable results. The LM628/629 was not designed with the intention to allow acceleration changes with moving motors.

6.2.2 Is there any way to change acceleration?

Answer: Acceleration change can be simulated by making many small changes of maximum velocity. For instance if a small velocity change is loaded, using LTRJ and STT commands, issuing these repeatedly at predetermined time intervals will cause the maximum velocity to increment producing a piecewise linear acceleration profile. The actual acceleration between velocity increments remains the same.

6.3 More on Stop Commands

6.3.1 What happens if the on-going trajectory is stopped by setting LTRJ control word bits 9 or 10, stop abruptly or stop smoothly, and then restarted by issuing Start, STT?

Answer: While stopped the motor position will be held by the control loop at the position determined as a result of issuing the stop command. Issuing STT will cause the motor to restart the trajectory toward the original target position with normal controlled acceleration.

6.3.2 What happens if the on-going trajectory is stopped by setting LTRJ control word bit 8, motor-off?

Answer: The LM628's DAC output is set to mid-scale, this puts zero volts on the motor which will still have a dynamic braking effect due to the commutation diodes. The LM629's PWM output sets the magnitude output to zero with a similar effect. If the motor freewheels or is moved the desired and actual positions will be the same. This can be verified using the RDDP and RDRP commands. When Start, STT, is issued the loop will be closed again and the motor will move toward the original trajectory from the actual current position.

6.3.3 If the motor is off, how can the control loop be closed and the motor energized?

Answer: Simply by issuing the Start, STT command. If any previous trajectory has completed then the motor will be held in the current position. If a trajectory was in progress when the motor-off command was issued then the motor will restart and move to the target position in position mode, or resume movement in velocity mode.

6.4 More on Define Home

6.4.1 What happens if the Define Home command, DFH, is issued while a current trajectory is in progress?

Answer: The position where the DFH command is issued is reset to zero, but the motor still stops at the original position commanded, i.e., the position where DFH is issued is substracted from the original target position.

6.4.2 Does issuing Define Home, DFH, zero both the trajectory and position register.

Answer: Yes, use Read Real Position, RDRP, and Read Desired Position, RDDP to verify.

6.5 More on Velocity

6.5.1 Why is a command error interrupt generated when inputting negative values of relative velocity?

Answer: Because the negative relative velocity would cause a negative absolute velocity which is not allowed. Negative absolute values of velocity imply movement in the negative direction which can be achieved by inputting a negative po-

sition value or in velocity mode by not setting bit 12. Similarly negative values of acceleration imply deceleration which occurs automatically at the acceleration rate when the LM628/629 stops the motor in position mode or if making a transition from a higher to a lower value of velocity.

6.5.2 What happens in velocity (or position) mode when the position range is exceeded?

Answer: The position range extends from maximum negative position hex'C0000000' to maximum positive position hex'3FFFFFFF' using a 32-bit double word. Bit 31 is the direction bit, logic 0 indicates forward direction, bit 30 is the wraparound bit used to control position over-range in velocity (or position) mode.

When the position increases past hex'3FFFFFFF' the wraparound bit 30 is set, which also sets the wraparound bit in the Status byte bit 4. This can be polled by the host or optionally used to interrupt the host as defined by the MSKI commands. Essentially the host has to manage wraparound by noting its occurrence and resetting the Status byte wraparound bit using the RSTI command. When the wraparound bit 30 is set in the position register so is the direction bit. This means one count past maximum positive position hex'3FFFFFFF' moves the position register onto the maximum negative position hex'C0000000'. Continued increase in positive direction causes the position register to count up to zero and back to positive values of position and on toward another wraparound.

Similarly when traveling in a negative direction, using two's complement arithmetic, position counts range from hex'FFFFFFF' (−1 decimal) to the maximum negative position of hex'C0000000'. One more negative count causes the position register to change to hex'3FFFFFFF', the maximum positive position. This time the wraparound bit 30 is reset, causing the wraparound bit 4 of the status byte to be set. Also the direction bit 31 is reset to zero. Further counts in the negative direction cause the position register to count down to zero as would be expected. With management there is no reason why absolute position should be lost, even when changing between velocity and position modes.

6.6 More on Use of Commands

6.6.1 If filter parameter and trajectory commands are pipelined for synchronization of axes, can the Update Filter, UDF, and Start, STT, commands be issued consecutively?

Answer: Yes.

6.6.2 Can commands be issued between another command and its data?

Answer: No.

6.6.3 What is the response time of the set breakpoint commands, SBPA and SBPR?

Answer: There is an uncertainty of one sample interval in the setting of the breakpoint bit 6 in the Status Byte in response to these commands.

6.6.4 What happens when the Set Index Position, SIP, command is issued?

Answer: On the next occurrence of all three inputs from the position encoder being low the corresponding position is loaded into the index register. This can be read with the Read Index Position command, RDIP. Bit 0 of the Read Signals register, shows when an SIP command has been issued but the index position has not yet been acquired. RDSIGS command accesses the Read Signals Register.

6.6.5 What happens if the motor is not able to keep up with the specified trajectory acceleration and velocity values?

Answer: A large, saturated, position error will be generated, and the control loop will be non-linear. The acceleration and velocity values should be set within the capability of the motor. Read Desired and Real Position commands, RDDP and RDRP can be used to determine the size of the error. The Load Position Error commands, for either host Interrupt or motor Stopping, LPEI and LPES, can be used to monitor the error size for controlled action where safety is a factor.

6.6.6 When is the command error bit 1 in the Status Byte set?

Answer:

a) When an acceleration change is attempted when the motor is moving and the drive on.

b) When loading a relative velocity would cause a negative absolute velocity.

c) Incorrect reading and writing operations generally.

6.6.7 What does the trajectory complete bit 2 in the Status Byte indicate?

Answer: That the trajectory loaded by LTRJ and initiated by STT has completed. The motor may or may not be at this position. Bit 2 is also set when the motor stop commands are executed and completed.

6.6.8 What do the specified minimum and maximum values of velocity mean in reality?

Answer: Assume a 500 line encoder = 1/2000 revs/count is used.

The maximum LM628/629 velocity is 16383 counts/sample and for a 8 MHz clock the LM628/629 sample rate is 3.9k samples/second, multiplying these values gives 32k revs/second or 1.92M rpm.

The maximum encoder rate is 1M counts/second multiplied by 1/2000 revs/count gives 500 revs/second or 30k rpm. The encoder capture rate therefore sets the maximum velocity limit.

The minimum LM628/629 velocity is 1/65536 counts/sample (one fractional count), multiplying this value by the sample rate and encoder revs/count gives 30×10^{-6} revs/second or 1.8×10^{-3} rpm.

The LM628 provides no limitation to practical values of velocity.

6.6.9 How long will it take to get to position wraparound in velocity mode traveling at 5000 rpm with a 500 line encoder?

Answer: 107 minutes.

7.0 REFERENCES AND FURTHER READING

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