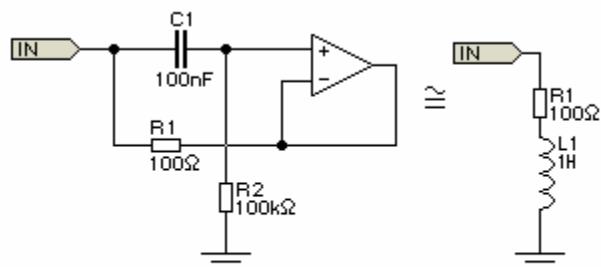


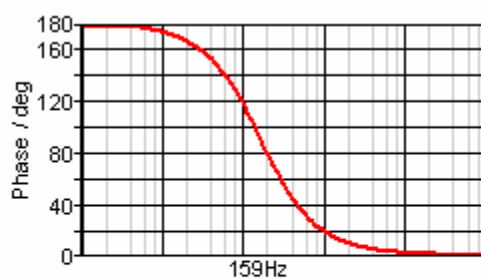
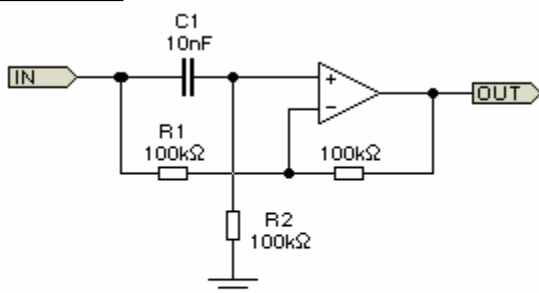
These are some of the basic concepts of active filters taken from Rod Elliot's website. For full articles and explanations, see the "Elliot Sound Products" link from the home page. This is just an overview for quick reference.

Simulated Inductor



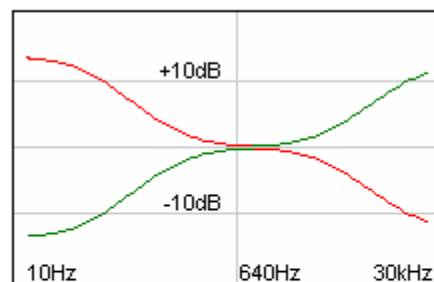
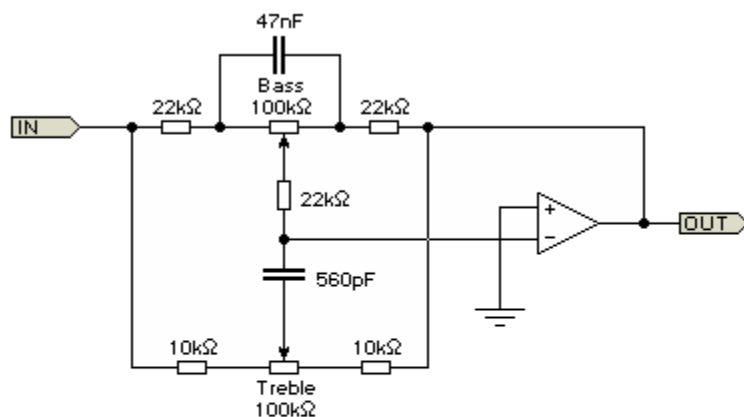
$$L = C1 * R1 * (R2 - R1)$$

Phase Shifter



$$F_{\text{Phase Shift}} = 1 / (2 * \pi * R2 * C1)$$

Simple Tone Control

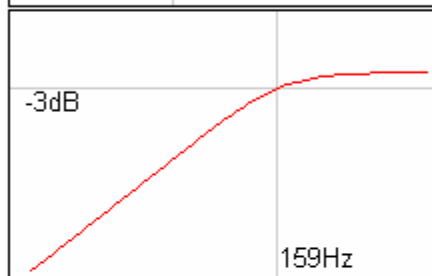
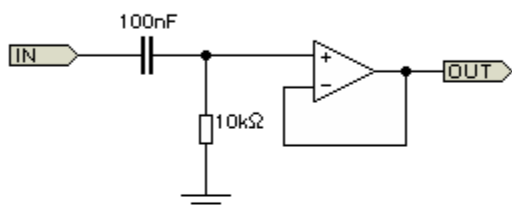
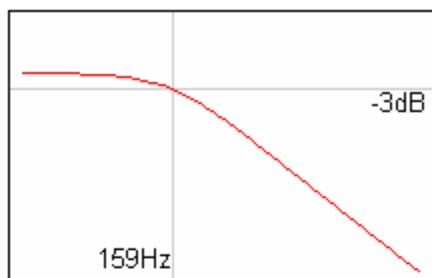
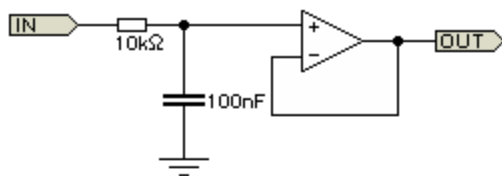


$F_{\text{Bass}_0} = 1 / (2 * \pi * C * R_v) \dots$ where C is the cap across the pot, and R_v is the pot value

$F_{\text{Bass}_{\pm 3\text{dB}}} = 1 / (2 * \pi * C * R_s) \dots$ where C is the cap, and R_s is the series resistance to the pot

$F_{\text{Treble}} = 1 / (2 * \pi * C * R_b) \dots$ where C is the treble cap (560pF above) and R_b is the bass feed resistor from the pot wiper. (Not accurate for treble due to bass interaction)

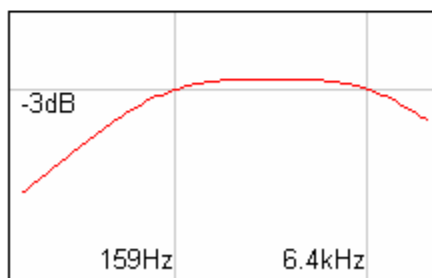
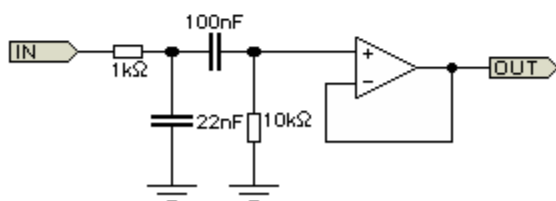
First Order Filter



$R_c = 1 / (2 * \pi * F * C) \dots$ where R_c is capacitive reactance

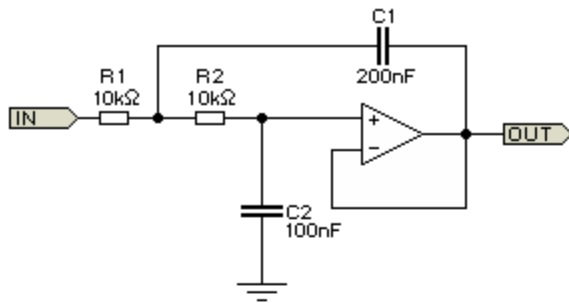
$$F_{-3dB} = 1 / (2 \pi R C)$$

$$F_{-3dB} = 1 / (2 \pi * 10k * 100nF) = 159 \text{ Hz}$$



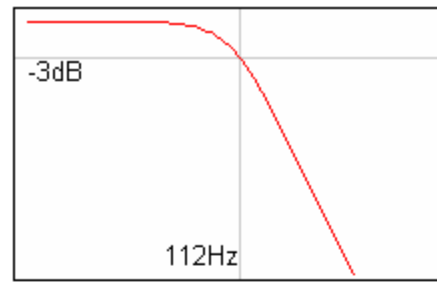
Cascaded (Second filter loads the first so separate filters would be more accurate)

Second Order Filter

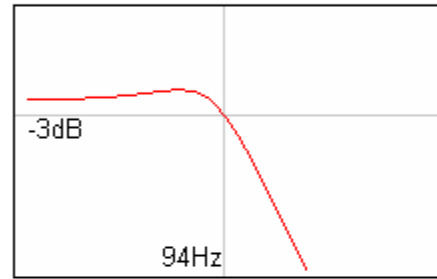
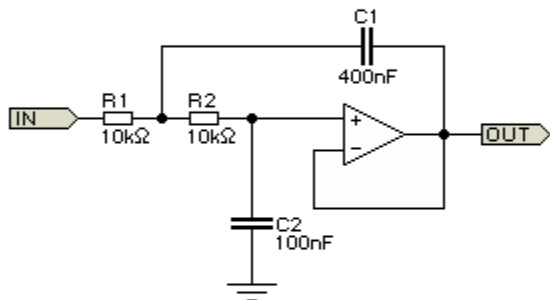


$$C1 = 4 / d^2 * C2 = 2 * C2 \dots \text{ where } d = 1 / Q$$

$$C2 = 0.707 / (2 * \pi * F * R)$$

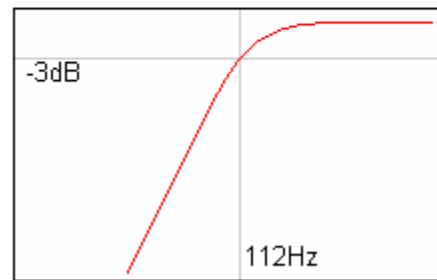
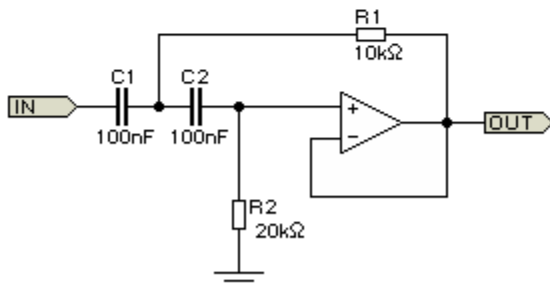


Butterworth (Q=.707)



Chebyshev (Q=1)

Formulae do not apply to Chebyshev!



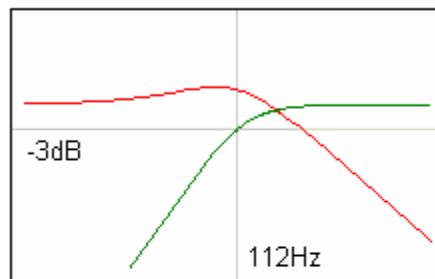
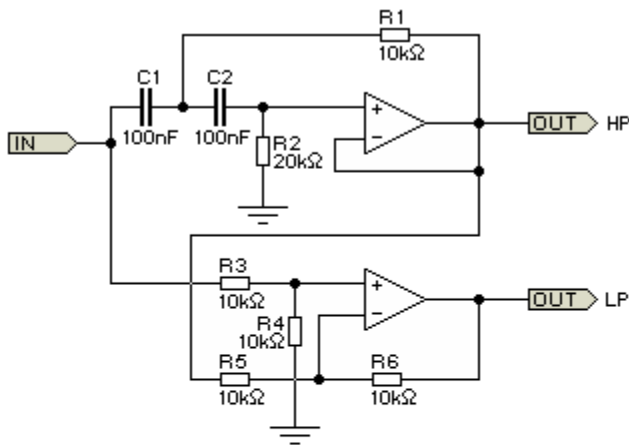
Butterworth (Q=.707)

Reversed Butterworth for High-Pass: Frequency determined by R1 and C1

$$R1 = 4 / d^2 * R2 = 2 * R2 \dots \text{ where } d = 1 / Q$$

$$C = 0.707 / (2 * \pi * F * R)$$

Subtracting Technique

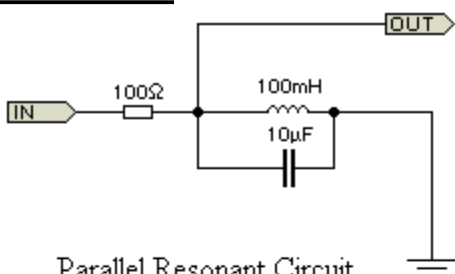


Subtracting Electronic Crossover

12dB/octave High-Pass subtracted from the full input by a differencing op-amp.

- -6dB Hi rolloff
- -12dB Lo rolloff
- Flat Response
- Phase Coherent

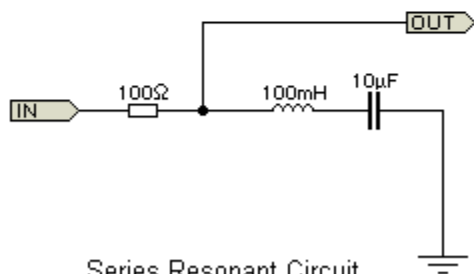
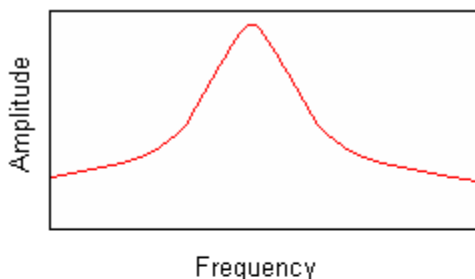
Resonance



Parallel Resonant Circuit

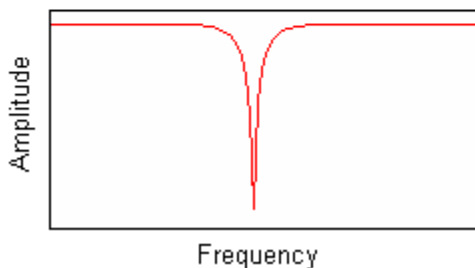
$$f_0 = 1 / (2 * \pi * \sqrt{LC})$$

Increase Q by increasing R_{in}



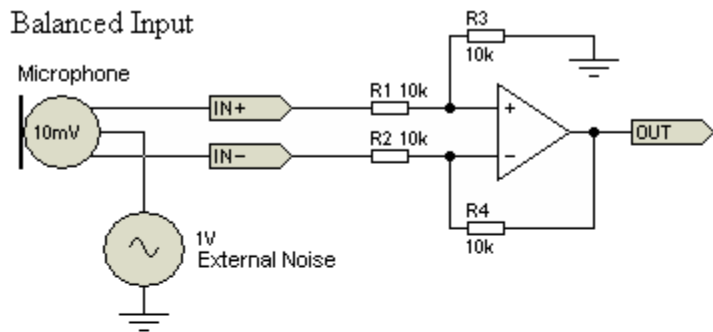
Series Resonant Circuit

Reduce Q by increasing R_{in}



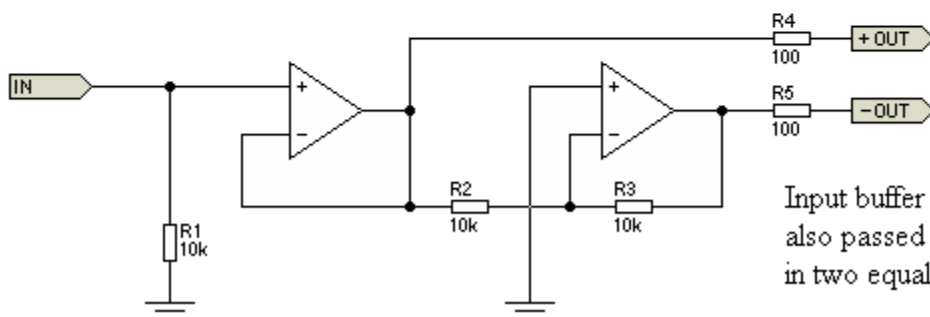
Common-Mode Rejection (Balanced Audio)

Balanced Input



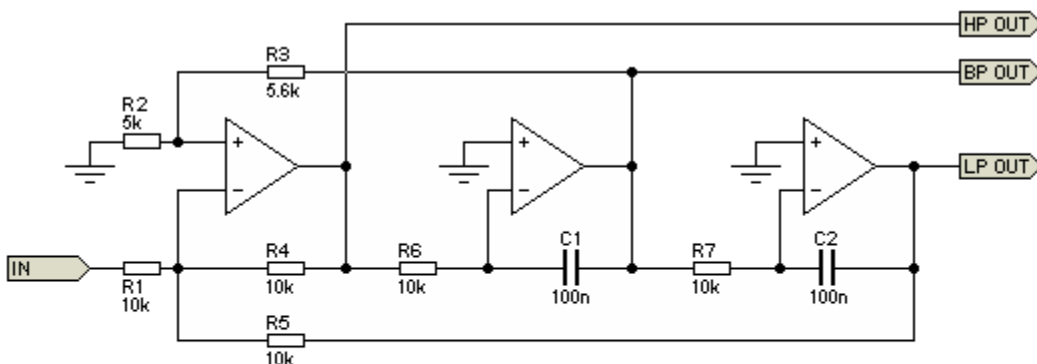
Common-Mode Rejection
 Opposite voltages are differenced, adding the absolute voltages together and cancelling what is common (noise).

Balanced Output



Input buffer is passed to the + Output and also passed to an inverting buffer, resulting in two equal but opposite signals.

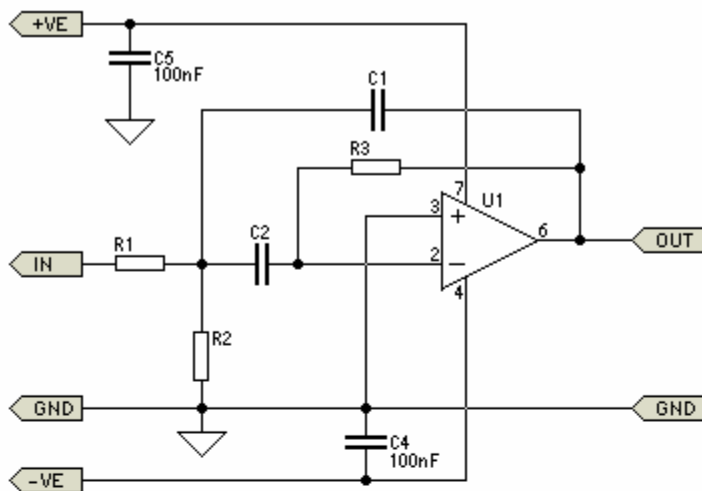
Advanced EQ



State Variable Filter

R3 sets filter Q: $R3 = (3 - d / d) * R2$ Where d = damping (1 / Q)
 Frequency is changed by varying R6 and R7, or C1 and C2.
 Bandpass output is in phase with input. Lowpass is +90° out of phase. Highpass is -90° out of phase.

Multiple Feedback Bandpass Filter (Graphic EQ)



1/3 octave interval - 3rd root of 2 - 1.26

For the 100 to 200 Hz octave, freq's are:

100*1.26, 100*1.26*1.26, 100*1.26*1.26...

= 100Hz, 126Hz, 158.7Hz and 200Hz.

bandwidth = 1/Q

Select capacitance first.

f (min) (Hz)	f(max) (Hz)	Capacitance (nF)
20	80	330
80	300	82
300	1,200	22
1200	4,800	5.6
4,800	20k	1.5

Input resistance $R1 = Q / (G * 2 * \pi * f * C)$

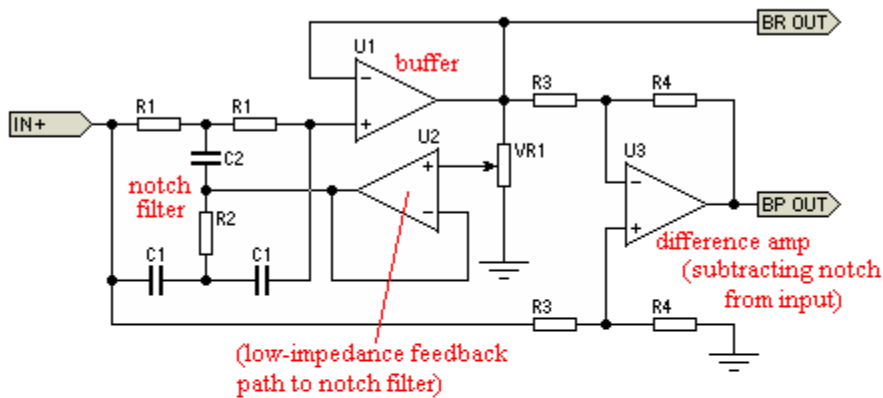
Attenuator resistance $R2 = Q / ((2 * Q^2 - G) * 2 * \pi * f * C)$

Feedback resistance $R3 = Q / (\pi * f * C)$

Passband Gain $G = 1 / ((R1 / R3) * 2)$

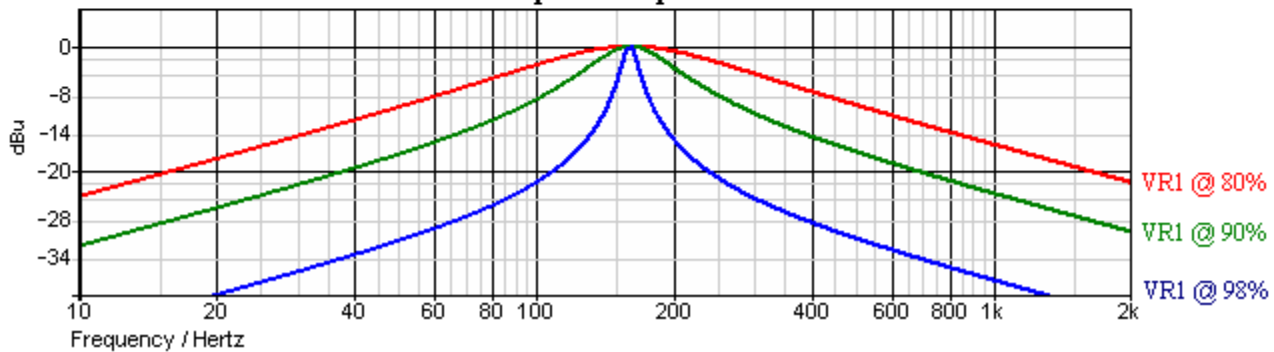
Centre Frequency $f = (1 / (2 * \pi * C)) * \sqrt{((R1 + R2) / (R1 * R2 * R3))}$

Constant Gain, Variable Q



$$R2 = R1 / 2 \text{ and } C2 = C1 * 2$$

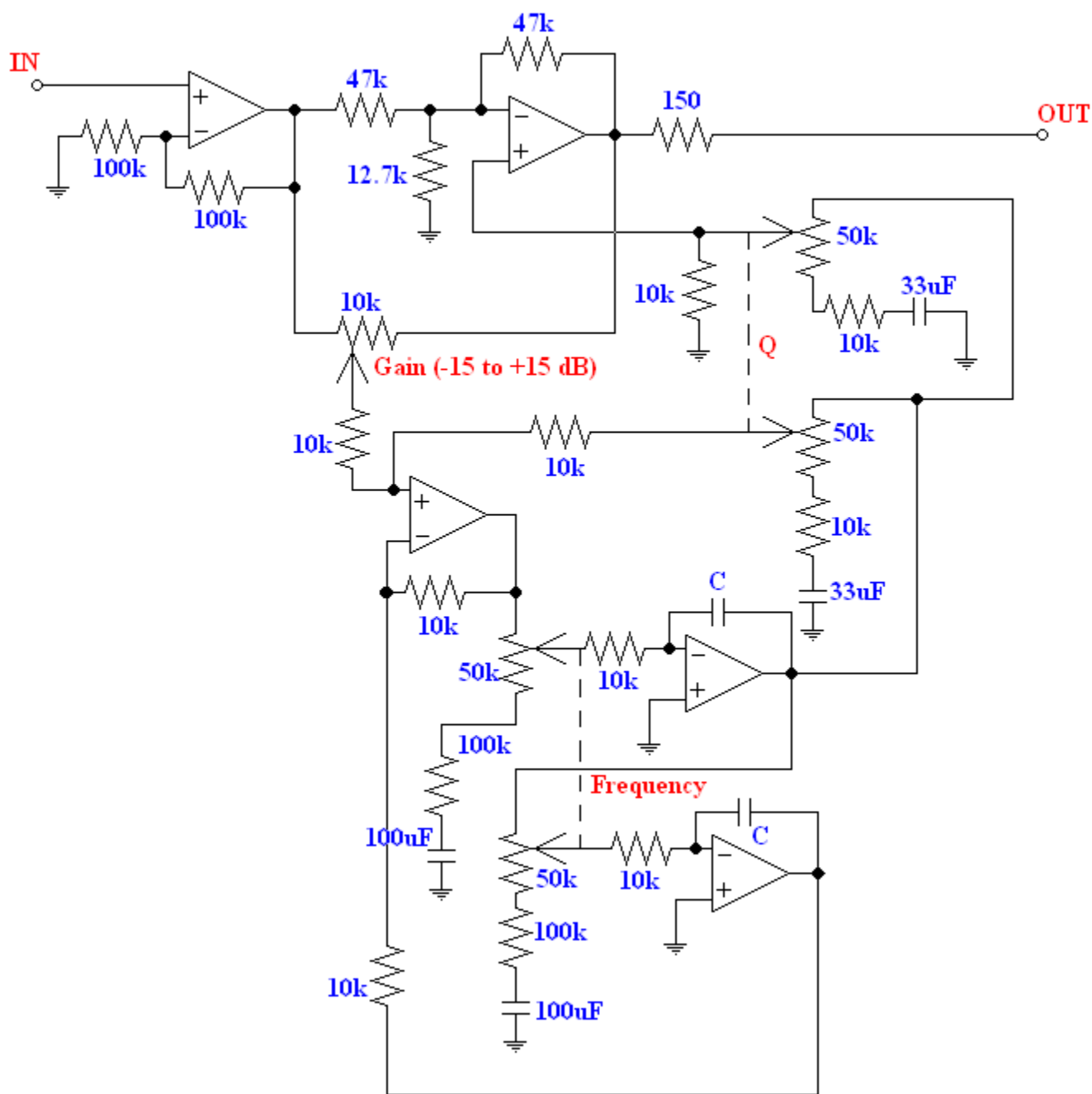
Bandpass Response



Fully Parametric EQ

This schematic is not part of the Elliot Sound Products website, but I think it is the most important filter network ever invented. This is a fully parametric EQ with characteristics similar to those found on a high-end mixing desk. All three parameters can be adjusted virtually independently of each other. At the extremes of the frequency sweep, Q adjustment has a slight effect on gain. Besides that, it is a very good parametric EQ.

$C = 27\text{nF}$, $f = 90 \text{ to } 587 \text{ Hz}$
 $C = 4.2\text{nF}$, $f = 581 \text{ to } 3.5\text{k Hz}$



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