

# Active filter has separate band and frequency controls

by John Jenkins  
Montgomery, Ala.

The bandwidth and center frequency of an active band-pass filter can be controlled independently by two separate resistors. Moreover, the filter's gain remains at unity over its full tuning range. Filter Q range is 2 to 200, while center frequency is 1 to 10 kilohertz.

The circuit shown in (a) has these properties, but it requires a variable inductor, which is usually difficult to tune, can be large, and cannot provide good temperature stability. The transfer function for this LC filter is:

$$e_o/e_i = (s/R_1C_1)/(s^2 + s/R_1C_1 + 1/LC_1)$$

Replacing the inductor with an active RC network, as illustrated in (b), yields a temperature-stable circuit. If all the components are ideal and  $R_2C_2 = R_3C_3$ , the equivalent inductance can be expressed as:

$$L_{eq} = R_2C_2R_f \text{ henries}$$

and the 3-decibel bandwidth as:

$$BW = 1/(2\pi R_1C_1) \text{ hertz}$$

and the center frequency as:

$$f_o = 1/[2\pi(R_fC_1R_2C_2)^{1/2}] \text{ Hz}$$

A wide range of component values can be used in the circuit, which is easy to design, once the desired filter specifications are established. As an example, a filter will be designed with a 5-Hz bandwidth, a center frequency of 1 kHz, and a maximum output voltage of 1 volt peak-to-peak. A few important operational amplifier specifications must also be known. Typically, input resistance ( $R_i$ ) is greater than 40 kilohms, output resis-

tance ( $R_o$ ) is less than 200 ohms, voltage gain ( $G_v$ ) is more than 10,000, and output voltage swing ( $V_{os}$ ) exceeds 20 v pk-pk.

To solve the design equations, let:

$$K_1 = (R_fC_1R_2C_2)^{1/2} = 1/(2\pi f_o) = 1.59 \times 10^{-4}$$

$$K_2 = R_1C_1 = 1/(2\pi BW) = 3.18 \times 10^{-2}$$

$$K_3 = (R_fC_1/R_2C_2)^{1/2} = [(V_{os2}/e_{omax})^2 - 1]^{1/2} = 19.98$$

then the filter's time constants can be computed:

$$R_1C_1 = K_2 = 3.18 \times 10^{-2}$$

$$R_2C_2 = K_1/K_3 = 7.96 \times 10^{-6}$$

$$R_fC_1 = K_1K_3 = 3.18 \times 10^{-3}$$

$$R_f/R_1 = K_1K_3/K_2 = 0.1$$

For most applications, a few simplified guidelines can be followed to choose component values: resistor  $R_1$  should be less than 400 kilohms, resistor  $R_2$  should lie between  $R_{i2}$  (about 40 kilohms) and 1 kilohm, the load resistance should be greater than 1 kilohm, and factor  $(1 - R_3C_3/R_2C_2)$  should range between 0 and resistance ratio  $(R_f/R_1) \times 10^{-2}$ .

This last constraint requires that time constant  $R_2C_2$  track  $R_3C_3$  within +0% and -0.1%. Therefore, these resistors and capacitors must have closely matched temperature coefficients and operating temperatures. Metal-film resistors and NPO-type capacitors that are mounted close together can be used. (The  $R_2C_2$  and  $R_3C_3$  time constants can be aligned by first opening the filter's input to obtain maximum Q, then increasing  $R_3$  until oscillation occurs, and then decreasing  $R_3$  until oscillation just stops.)

A set of typical component values is noted in (b). As indicated, resistor  $R_1$  tunes filter bandwidth, while resistor  $R_f$  adjusts center frequency. □

**Active circuit ousts variable inductor.** Bandpass filter (a) offers independent center frequency and bandwidth adjustments. Hard-to-tune variable inductor can be replaced by active circuit (b) that provides an equivalent inductance and better temperature stability. Fully active filter is easy to design and will operate over a broad range of component values. General-purpose amplifiers can be used.

