

Ideal rectifier uses equal-value resistors

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Operational amplifiers can be combined with diodes and resistors to perform nearly ideal rectification, satisfying $e_o = |e_i|$. The diodes are situated within the feedback loop, so that the diode forward voltage drop is reduced at the output by the feedback factor. Figure 1a shows a commonly used full-wave rectifying circuit which gives a positive output, e_o , for bipolar input at e_i . This circuit has the following disadvantages:

- Output e_o due to plus input at e_i is obtained by bucking out the plus current from R_5 with the negative (rectified) current through R_3 . The tolerance of this difference voltage can be three times resistor tolerance, since it is obtained by subtraction.
- Non-zero input impedance. If a summing junction is required at the input node, another operational amplifier is required.
- Increased drive requirements. The input at e_i drives two amplifiers in parallel.
- Unequal resistor values. R_3 is half of R_5 .

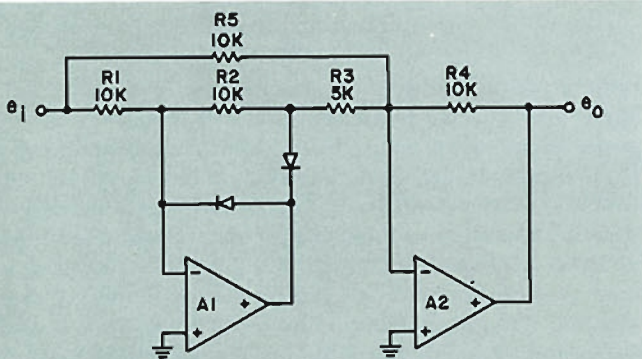


FIGURE 1a.

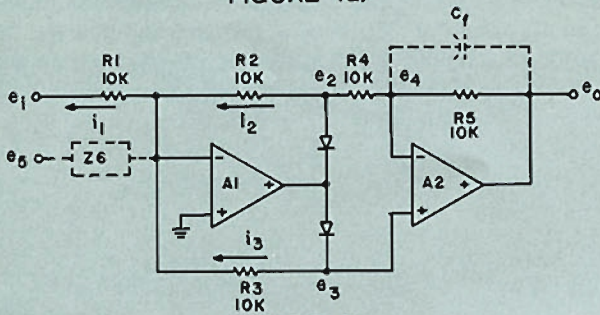


FIGURE 1b.

An improved 'ideal' full-wave rectifier (b) is achieved by modifying a standard circuit (a).

Figure 1b shows an "ideal" rectifier configuration which has the following advantages:

- All resistors are of the same (arbitrary) value.
- Output voltage tolerance is an additive function of resistor tolerance. Equal-value resistors are easy to select for high accuracy.
- Zero input impedance. The single summing junction at n allows extra isolated inputs to be connected, as shown dotted for e_5 and Z_6 .

It may be necessary to connect a small capacitor, C_f , in parallel with R_5 in order to prevent high-frequency oscillations. Rectified voltages e_2 and e_3 are unequal in this circuit.

It turns out that the equal-resistor version is a special case and that, in general, the resistors can be unequal as long as they satisfy Eq. 3 below, which is derived in the following manner. The voltage gain for plus input is:

$$G(+)=e_o/e_i=(R_2/R_1)(R_5/R_4). \quad (1)$$

This is the gain of two tandem-connected inverting operational amplifiers.

For minus input there are two feedback paths to the summing junction of A1, one from each amplifier out (Figure 1b). Mathematically this is expressed as:

$$i_1=i_2+i_3$$

or

$$e_i/R_1=e_o/(R_2+R_4+R_5)+e_3/R_3;$$

since:

$$e_3=e_4=e_o(R_2+R_4)/(R_2+R_4+R_5),$$

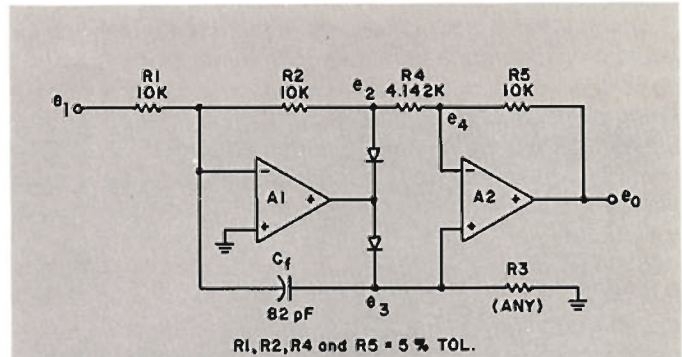
then:

$$\begin{aligned} 1/G(-) &= e_i/e_o \\ &= R_1[1/(R_2+R_4+R_5) \\ &\quad + (R_2+R_4)/R_3 \\ &\quad \times (R_2+R_4+R_5)]. \end{aligned} \quad (2)$$

This is equated with $1/G(+)=[(R_1/R_2)(R_4/R_5)]$ to ensure equal output for plus and minus inputs. The resulting identity is solved for R_2/R_3 :

$$R_2/R_3=(R_4/R_5)+[(1-R_2/R_4)/(1+R_2/R_4)]. \quad (3)$$

Inspection of Eq. 3 shows that if $R_2=R_4$ the second term drops out and $R_3=R_5$. Furthermore, for unity gain, $R_2=R_3$ and $R_2=R_3=R_4=R_5$; the result is the circuit shown in Figure 1b. If current gain is required from A1, $R_2/R_4 > 1$ and Eq. 3 is used to calculate R_3 after R_2 , R_4 , and R_5 have been selected. If the calculated value of R_3 is negative, R_5 is reduced and R_3 is recalculated.



R_1, R_2, R_4 and $R_5 = 5\% \text{ TOL.}$

FIGURE 2. Degenerate form of ideal rectifier uses only four precision resistors.

A new circuit results if R_3 is allowed to go to infinity and the noninverting input of A2 is returned to ground through a resistor of arbitrary value (Figure 2). This is an ideal rectifier circuit that requires only three precision resistors (four, if R_1 is counted in). If a further constraint that three of these resistors must be equal is imposed, the resistor ratios are:

$$R_1=R_2=R_5=R;$$

$$R_4=(2^{1/2}-1)R;$$

$$|G|=2^{1/2}+1.$$

(continued on next page)

In general:

$$\begin{aligned}R_2 &> R_4; \\ R_4/R_5 &= (R_2/R_4 - 1) / (R_2/R_4 + 1); \\ |G| &= (R_2/R_1) (R_5/R_4) \\ &= (R_2 + R_4 + R_5) / R_1.\end{aligned}$$

The gain is fixed at $1 + 2\frac{1}{2}$ for both plus and minus inputs. One difficulty with the circuit of Figure 2 is that the forward path for negative inputs consists of the full open-loop gain of A1 and A2 in tandem. A value for C_f of 82pF was sufficient to stabilize an operating breadboard made with low-cost commercial units.

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