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Single op amp achieves doublehysteresis-transfer characteristic

Herminio Martínez, Encarna García, and Juan Gámiz, Technical University of Catalonia, Barcelona, Spain

In process-control applications requiring discontinuous controllers, the most elementary choice is a two-position-mode or on/off controller. A typical example of such a controller is a space heater. If the temperature drops below a setpoint, the heater turns on, and, if the temperature rises above the setpoint, it turns off. In the analog domain, the basis for the ba-



Figure 1 One straightforward way of obtaining a double-hysteresis-transfer characteristic uses three op amps with voltage references and zener diodes.



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sic implementation of a two-position controller is an analog comparator or an open-loop operational amplifier. However, to avoid false switching, the typical implementation uses the wellknown Schmitt trigger.

A logical extension of the two-position control mode is to provide several-rather than two-intermediate settings of the controller's output. You can use this discontinuous-control mode to reduce the cycling behavior, overshoot, or undershoot inherent in the two-position mode. In fact, however, it is usually speedier to use some other mode when the two-position mode is unsatisfactory. The most common example is the three-position controller. Figure 1 shows one simple way to implement this controller. In this configuration, the Schmitt triggers around the operational amplifiers, A1 and A2, which implement the negative and positive hysteresis, respectively. You can replace A_1 and A_2 with analog comparators, such as an LM311 or similar. Figure 2 shows the I/O-transfer characteristic of the circuit in Figure 1:

$$V_{\rm M} = V_{\rm REF} \frac{R_1 + R_2}{R_2},$$

designideas

$$V_{\rm H} = V_{\rm M} + \left(V_{\rm Z} + V_{\rm Y}\right) \frac{R_1}{R_2}$$

and

$$V_{L} = V_{M} - (V_{Z} + V_{Y}) \frac{R_{1}}{R_{2}}.$$

 V_z and V_y are, respectively, the breakdown and the forward voltages of the four zener diodes.

Figure 3 shows a more efficient way to implement a three-position controller. The circuit's basis is a single operational amplifier, and it needs no reference voltages. The input and output diodes determine the upper high-voltage and lower low-voltage switchingthreshold levels and the hysteresis of the comparator. Putting $V_{\mbox{\tiny IN}}(t)$ in the middle band eliminates the input diodes from the circuit, and the circuit is essentially a voltage follower with positive feedback. The output voltage follows $V_{4}(t)$, but the positive feedback establishing $V_{A}(t)$ sets this voltage at some fraction of the output voltage. So, two constraints define the output level in this circuit state: $V_{OUT}(t) = V_A(t)$, and

$$V_{A}(t) = V_{OUT}(t) \frac{R_{1}}{R_{1} + R_{2}}.$$

The only condition satisfying these two constraints is that V_{OUT} and V_A =0V; so, the output remains at 0V when the input diodes are reverse-biased. A 0V output state continues until input voltage increases with positive or negative values. Then, one of the two input zener diodes conducts, driving the amplifier output positive or negative at an input voltage of $\pm V_H$. In this condition, when absolute input voltage decreases, the amplifier output again goes to 0V at an input voltage of $\pm V_L$. Thus, the design equations for V_H and V_L are $V_H = V_{Z1} + V_\gamma$, and **Figure 4** shows the I/O-transfer

Figure 4 shows the I/O-transfer characteristic of the circuit with the values in **Figure 3**, where D_{1A} and D_{1B}

$$V_{L} = (V_{Z1} + V_{Y1}) - (V_{Z2} + V_{Y2}) \frac{R_{1}}{R_{1} + R_{2}}$$

are 6.8V 1N4099 zener diodes and D_{2A} and D_{2B} are 3V 1N5225 zener diodes. Figure 5 shows the output voltage when you apply a triangular waveform at the circuit's input.EDN



Figure 3 This circuit achieves dual hysteresis using only one op amp.



Figure 4 This oscilloscope trace shows the transfer characteristic of the circuit in Figure 3.



Figure 5 This oscilloscope trace shows the response of the circuit in Figure 3 to a triangular input waveform.