

## Two op amp instrumentation amplifier circuit

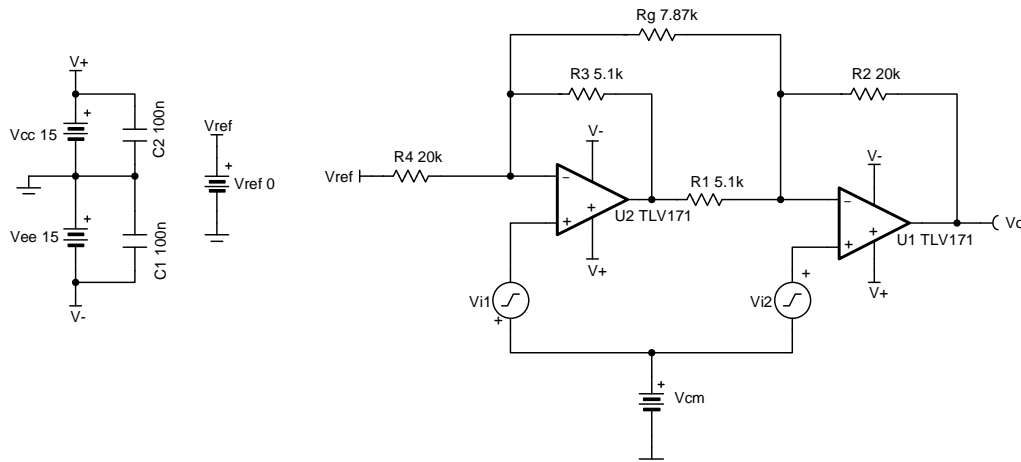
### Design Goals

Input $V_{IDiff}(V_{i2} - V_{i1})$		Output		Supply		
$V_{IDiff\_Min}$	$V_{IDiff\_Max}$	$V_{oMin}$	$V_{oMax}$	$V_{cc}$	$V_{ee}$	$V_{ref}$
+/-1V	+/-2V	-10V	+10V	15V	-15V	0V

$V_{cm}$	Gain Range
+/-10V	5V/V to 10V/V

### Design Description

This design amplifies the difference between  $V_{i1}$  and  $V_{i2}$  and outputs a single ended signal while rejecting the common-mode voltage. Linear operation of an instrumentation amplifier depends upon the linear operation of its primary building block: op amps. An op amp operates linearly when the input and output signals are within the device's input common-mode and output-swing ranges, respectively. The supply voltages used to power the op amps define these ranges.



### Design Notes

1.  $R_g$  sets the gain of the circuit.
2. High-value resistors can degrade the phase margin of the circuit and introduce additional noise in the circuit.
3. The ratio of  $R_4$  and  $R_3$  set the minimum gain when  $R_g$  is removed.
4. Ratios of  $R_2/R_1$  and  $R_4/R_3$  must be matched to avoid degrading the instrumentation amplifier's DC CMRR and ensuring the  $V_{ref}$  gain is 1V/V.
5. Linear operation is contingent upon the input common-mode and the output swing ranges of the discrete op amps used. The linear output swing ranges are specified under the  $A_{o1}$  test conditions in the op amps datasheets.

## Design Steps

1. Transfer function of this circuit.

$$V_o = V_{iDiff} \times G + V_{ref} = (V_{i2} - V_{i1}) \times G + V_{ref}$$

when  $V_{ref} = 0$ , the transfer function simplifies to the following equation:

$$V_o = (V_{i2} - V_{i1}) \times G$$

where  $G$  is the gain of the instrumentation amplifier and  $G = 1 + \frac{R_4}{R_3} + \frac{2R_2}{R_g}$

2. Select  $R_4$  and  $R_3$  to set the minimum gain.

$$G_{min} = 1 + \frac{R_4}{R_3} = 5 \frac{V}{V}$$

Choose  $R_4 = 20k\Omega$

$$G_{min} = 1 + \frac{20k\Omega}{R_3} = 5 \frac{V}{V}$$

$$R_3 = \frac{R_4}{5-1} = \frac{20k\Omega}{4} = 5k\Omega \rightarrow R_3 = 5.1k\Omega \text{ (Standard Value)}$$

3. Select  $R_1$  and  $R_2$ . Ensure that  $R_1/R_2$  and  $R_3/R_4$  ratios are matched to set the gain applied to the reference voltage at  $1V/V$ .

$$\frac{V_{o-ref}}{V_{ref}} = \left(-\frac{R_3}{R_4}\right) \times \left(-\frac{R_2}{R_1}\right) = \frac{R_3 \times R_2}{R_4 \times R_1} = 1 \frac{V}{V}$$

$$\frac{R_2}{R_1} = \frac{R_4}{R_3} \rightarrow R_1 = R_3 = 5.1k\Omega \text{ and } R_2 = R_4 = 20k\Omega \text{ (Standard Value)}$$

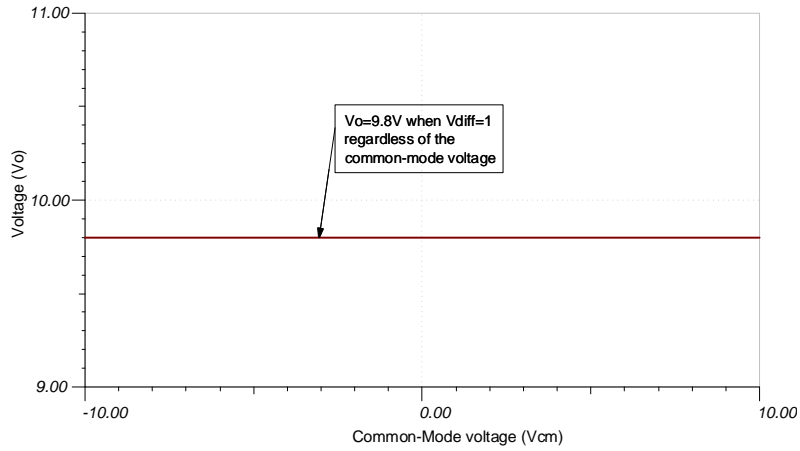
4. Select  $R_g$  to meet the desired maximum gain  $G = 10V/V$ .

$$G = 1 + \frac{R_4}{R_3} + \frac{2R_2}{R_g} = 1 + \frac{20k\Omega}{5.1k\Omega} + \frac{2 \times 20k\Omega}{R_g} = 10 \frac{V}{V}$$

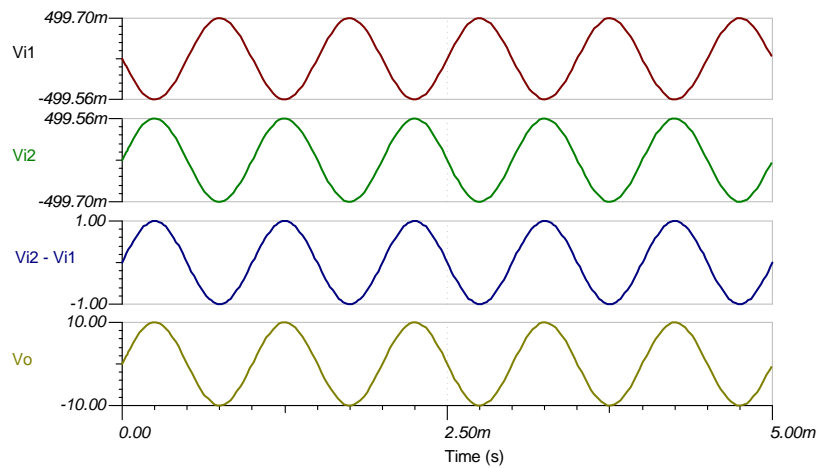
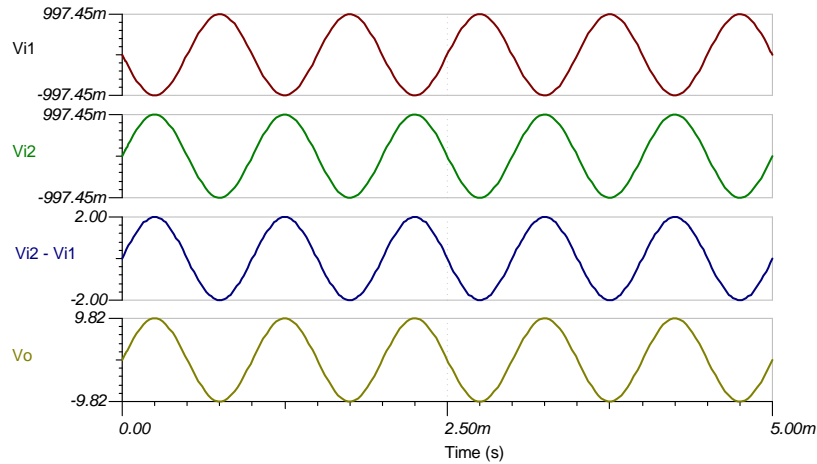
$$R_g = 8k\Omega \rightarrow R_g = 7.87k\Omega \text{ (Standard Value)}$$

**Design Simulations**

**DC Simulation Results**



**Transient Simulation Results**



**References:**

1. [Analog Engineer's Circuit Cookbooks](#)
2. SPICE Simulation File [SBOMAU7](#)
3. [TI Precision Labs](#)
4. [V<sub>CM</sub> vs. V<sub>OUT</sub> plots for instrumentation amplifiers with two op amps](#)
5. [Common-mode Range Calculator for Instrumentation Amplifiers](#)

**Design Featured Op Amp**

TLV171	
V <sub>ss</sub>	4.5V to 36V
V <sub>inCM</sub>	(V <sub>ee</sub> -0.1V) to (V <sub>cc</sub> -2V)
V <sub>out</sub>	Rail-to-rail
V <sub>os</sub>	0.25mV
I <sub>q</sub>	475μA
I <sub>b</sub>	8pA
UGBW	3MHz
SR	1.5V/μs
#Channels	1,2,4
<a href="http://www.ti.com/product/tlv171">www.ti.com/product/tlv171</a>	

**Design Alternate Op Amp**

OPA172	
V <sub>ss</sub>	4.5V to 36V
V <sub>inCM</sub>	(V <sub>ee</sub> -0.1V) to (V <sub>cc</sub> -2V)
V <sub>out</sub>	Rail-to-rail
V <sub>os</sub>	0.2mV
I <sub>q</sub>	1.6mA
I <sub>b</sub>	8pA
UGBW	10MHz
SR	10V/μs
#Channels	1,2,4
<a href="http://www.ti.com/product/opa172">www.ti.com/product/opa172</a>	

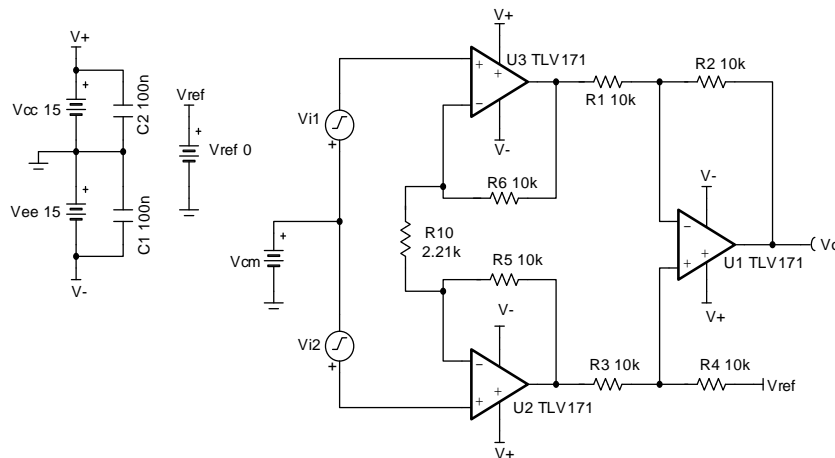
## Three op amp instrumentation amplifier circuit

### Design Goals

Input $V_{i\text{diff}}$ ( $V_{i2} - V_{i1}$ )		Common-mode Voltage	Output		Supply		
$V_{i\text{diff Min}}$	$V_{i\text{diff Max}}$	$V_{\text{cm}}$	$V_{o\text{Min}}$	$V_{o\text{Max}}$	$V_{\text{cc}}$	$V_{\text{ee}}$	$V_{\text{ref}}$
-0.5V	+0.5V	$\pm 7\text{V}$	-5V	+5V	+15V	-15V	0V

### Design Description

This design uses 3 op amps to build a discrete instrumentation amplifier. The circuit converts a differential signal to a single-ended output signal. Linear operation of an instrumentation amplifier depends upon linear operation of its building block: op amps. An op amp operates linearly when the input and output signals are within the device's input common-mode and output swing ranges, respectively. The supply voltages used to power the op amps define these ranges.



### Design Notes

1. Use precision resistors to achieve high DC CMRR performance
2.  $R_{10}$  sets the gain of the circuit.
3. Add an isolation resistor to the output stage to drive large capacitive loads.
4. High-value resistors can degrade the phase margin of the circuit and introduce additional noise in the circuit.
5. Linear operation is contingent upon the input common-mode and the output swing ranges of the discrete op amps used. The linear output swing ranges are specified under the  $A_{o1}$  test conditions in the op amps datasheets.

## Design Steps

1. Transfer function of this circuit:

$$V_o = (V_{i2} - V_{i1}) \times G + V_{ref}$$

When  $V_{ref} = 0$ , the transfer function simplifies to the following equation:

$$V_o = (V_{i2} - V_{i1}) \times G$$

$$\text{where } G = \frac{R_4}{R_3} \times \left( 1 + \frac{2 \times R_5}{R_{10}} \right)$$

2. Select the feedback loop resistors  $R_5$  and  $R_6$ :

Choose  $R_5 = R_6 = 10 \text{ k}\Omega$  (Standard Value)

3. Select  $R_1, R_2, R_3, R_4$ . To set the  $V_{ref}$  gain at  $1V/V$  and avoid degrading the instrumentation amplifier's CMRR, ratios of  $R_4/R_3$  and  $R_2/R_1$  must be equal.

Choose  $R_1 = R_2 = R_3 = R_4 = 10 \text{ k}\Omega$  (Standard Value)

4. Calculate  $R_{10}$  to meet the desired gain:

$$G = \frac{R_4}{R_3} \times \left( 1 + \frac{2 \times R_5}{R_{10}} \right) = 10 \frac{V}{V} \quad ( \quad )$$

$$R_4 = R_3 = 10 \text{ k}\Omega$$

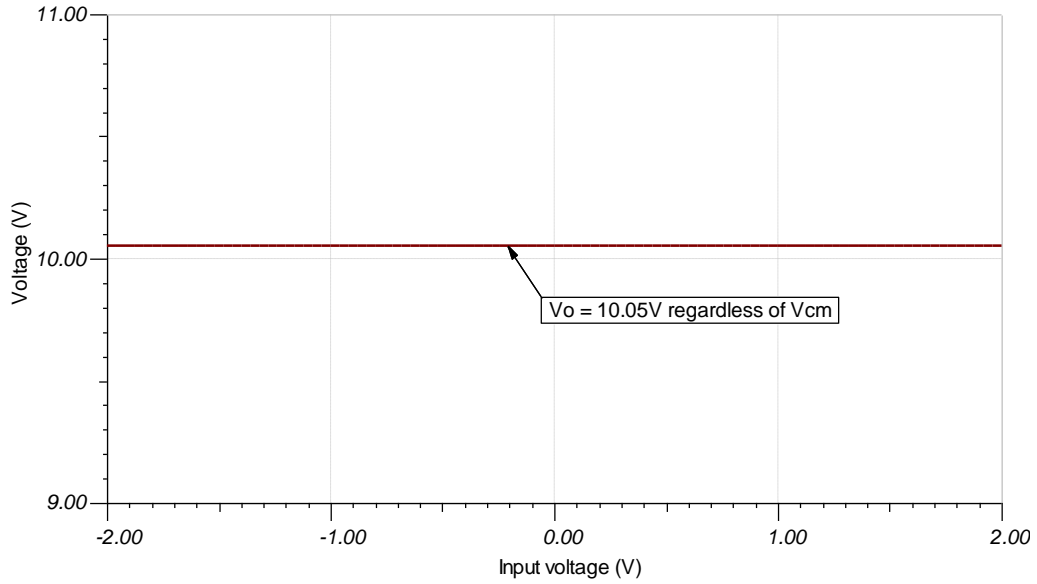
$$\rightarrow G = 1 + \frac{2 \times 10 \text{ k}\Omega}{R_{10}} = 10 \frac{V}{V} \rightarrow 1 + \frac{20 \text{ k}\Omega}{R_{10}} = 10 \frac{V}{V}$$

$$\frac{20 \text{ k}\Omega}{R_{10}} = 9 \frac{V}{V} \rightarrow R_{10} = \frac{20 \text{ k}\Omega}{9} = 2222.2 \Omega \rightarrow R_{10} = 2.21 \text{ k}\Omega \quad (\text{Standard Value}) \quad (1)$$

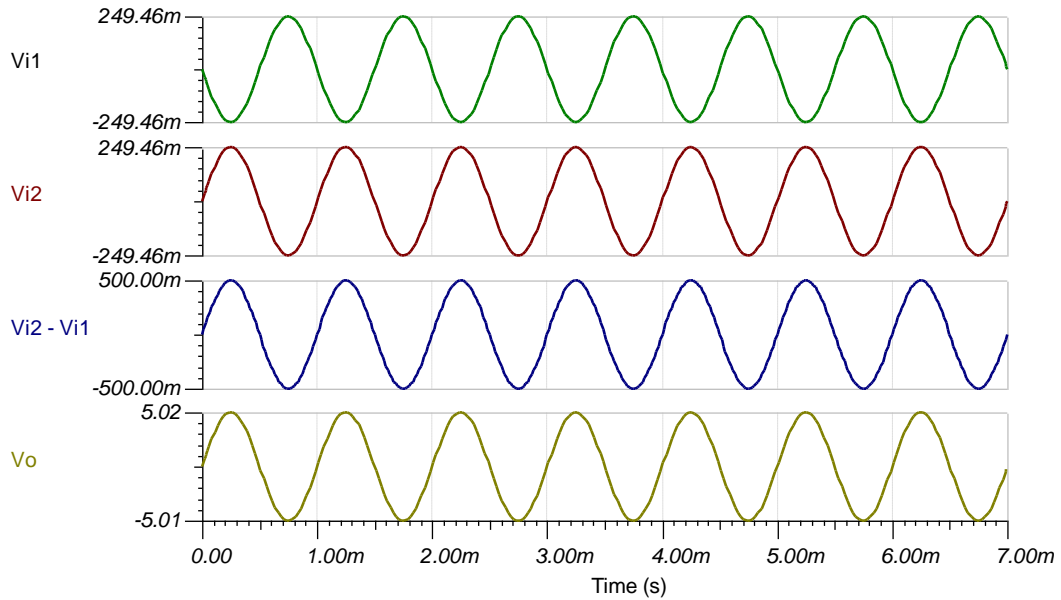
5. To check the common-mode voltage range, download and install the program from reference [5]. Edit the INA\_Data.txt file in the installation directory by adding the code for a 3 op amp INA whose internal amplifiers have the common-mode range, output swing, and supply voltage range as defined by the amplifier of choice (TLV172 in this case). There is no  $V_{be}$  shift in this design and the gain of the output stage difference amplifier is  $1 V/V$ . The default supply voltage and reference voltages are  $\pm 15 \text{ V}$  and  $0 \text{ V}$ , respectively. Run the program and set the gain and reference voltage accordingly. The resulting  $V_{CM}$  vs.  $V_{OUT}$  plot approximates the linear operating region of the discrete INA.

**Design Simulations**

**DC Simulation Results**



**Transient Simulation Results**



**References:**

1. [Analog Engineer's Circuit Cookbooks](#)
2. SPICE Simulation File [SBOMAU8](#)
3. [TI Precision Labs](#)
4. [Instrumentation Amplifier  \$V\_{CM}\$  vs.  \$V\_{OUT}\$  Plots](#)
5. [Common-mode Range Calculator for Instrumentation Amplifiers](#)

**Design Featured Op Amp**

TLV171	
$V_{SS}$	4.5V to 36V
$V_{inCM}$	$(V-) - 0.1V < V_{in} < (V+) - 2V$
$V_{out}$	Rail-to-rail
$V_{os}$	0.25mV
$I_q$	475 $\mu$ A
$I_b$	8pA
UGBW	3MHz
SR	1.5V/ $\mu$ s
#Channels	1,2,4
<a href="http://www.ti.com/product/tlv171">www.ti.com/product/tlv171</a>	

**Design Alternate Op Amp**

	OPA172	OPA192
$V_{SS}$	4.5V to 36V	4.5V to 36V
$V_{inCM}$	$(V-) - 0.1V < V_{in} < (V+) - 2V$	$V_{ee} - 0.1V$ to $V_{cc} + 0.1V$
$V_{out}$	Rail-to-rail	Rail-to-rail
$V_{os}$	0.2mV	$\pm 5\mu$ V
$I_q$	1.6mA	1mA/Ch
$I_b$	8pA	5pA
UGBW	10MHz	10MHz
SR	10V/ $\mu$ s	20V/ $\mu$ s
#Channels	1,2,4	1, 2, 4
	<a href="http://www.ti.com/product/opa172">www.ti.com/product/opa172</a>	<a href="http://www.ti.com/product/opa192">www.ti.com/product/opa192</a>